

S-39-26 (Pace Bridge Road) Bridge Replacement over Tributary to South Saluda River

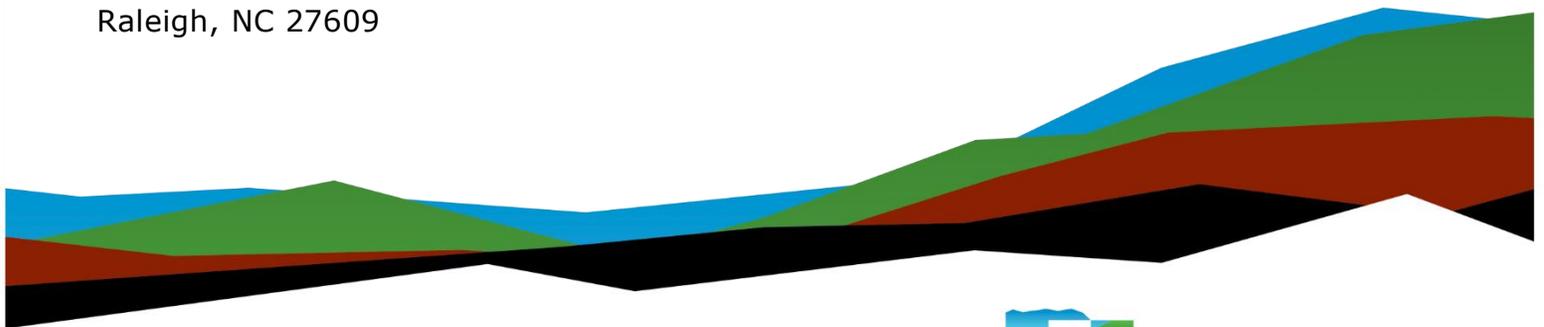
Pickens County, SC

Geotechnical Subsurface Data Report

October 30, 2024 | SCDOT Project ID: P043138
Terracon Project No.: 8623P180 Revision 1

Prepared for:

HNTB Corporation
343 E. Six Forks Road, Suite 200
Raleigh, NC 27609



Nationwide
[Terracon.com](https://www.terracon.com)

- Facilities
- Environmental
- Geotechnical
- Materials



72 Pointe Circle
Greenville, SC 29615
P (864) 292-2901
Terracon.com

October 30, 2024

HNTB Corporation
343 E. Forks Road, Suite 200
Raleigh, NC 27609

Attn: Mr. Spencer Franklin, PE, Senior Vice President
P: 919-546-8997

Re: Geotechnical Subsurface Data Report
S-39-26 Bridge Replacement over Tributary to South Saluda River
Pickens County, South Carolina
SCDOT Project ID.: P043138
Terracon Project No.: 8623P180 Revision 1

Dear Mr. Franklin:

Terracon Consultants Inc. (Terracon) has completed the exploration, testing and limited engineering analysis services (contained in the geotechnical baseline report) for the above referenced project. The services were conducted in general accordance with our Supplement Number 004 to Task Order Number 001, dated July 19, 2024.

Introduction

HNTB Corporation (HNTB) has contracted Terracon to perform subsurface exploration, laboratory testing and limited preliminary engineering recommendations for the replacement of the S-39-26 bridge over Tributary to South Saluda River in Pickens County, South Carolina. This will be a complete bridge replacement within the project existing alignment. This GSDR was prepared in general accordance with the 2022 SCDOT Geotechnical Design Manual (GDM) and Preconstruction Design Memorandum (PCDM) 11 - Supplemental Design Criteria for Low Volume Bridge Replacement Projects.

Project Description

The project site is located at the S-39-26 (Pace Bridge Road) crossing over Tributary to South Saluda River in Pickens County, South Carolina. Site location and exploration plans are presented in Appendix A of this report. Based on the conceptual plans by HNTB dated 9/3/2024, the replacement bridge will be constructed on the same alignment as the current

bridge. The current plan indicates the new bridge will be a 70-ft long single span bridge constructed with a prestressed concrete cored slab.

Geotechnical Testing

The geotechnical exploration for this project was performed between August 14 and August 20, 2024. The results of our fieldwork and our associated laboratory testing are included in Appendices A and B.

Field Exploration

Our field exploration consisted of the following:

- Two (2) Standard Penetration Test (SPT) Borings (S-39-26-1 and S-39-26-2)
- Two (2) offset borings near S-39-26-1 and S-39-26-2 for bulk sample collection

The tests were performed at the approximate locations as approved by SCDOT. A description of our testing methods and graphical logs outlining the soil conditions at each test location are presented in Appendix A. The test locations were established in the field by Terracon and surveyed by Thomas & Hutton after completion. Station and offset are based on the plans provided at the time the tests were performed.

Laboratory Testing

The following laboratory tests were performed on the soil samples collected at the site.

- Twenty-two (22) Natural Moisture Content Tests
- Six (6) Atterberg Limits Tests
- Seven (7) Fines Content Tests
- Four (4) Grain Size Tests with Hydrometer
- One (1) Remolded, Consolidated-Undrained (CU) Triaxial Compression Test with Pore Pressure Readings
- One (1) Standard Proctor Test
- One (1) Corrosivity Suite (pH, chloride content, sulfate content, and resistivity tests)
- Four (4) Compressive Strength of Rock Cores

The general scope of the laboratory testing frequency was determined by the SCDOT. The laboratory testing assignment was performed by our engineers. The laboratory procedures and results of the laboratory tests are presented in Appendix B.

Geotechnical Subsurface Data Report

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
October 30, 2024 | Terracon Project No. 8623P180 R1 | SCDOT Project ID: P043138



Closure

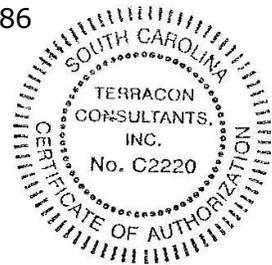
We appreciate the opportunity to be of service to you on this project. If you have any questions concerning this report or we may be of further service, please contact us.

Sincerely,
Terracon Consultants, Inc.

A handwritten signature in black ink that reads "Maggie McKenney".

Maggie McKenney, EIT
Senior Staff Engineer

Jonathan Ard, PE
Manager Regional Services
SC Registration No. 30886



Appendix A

Field Exploration

- Exhibit A-1 – Site Location Map
- Exhibit A-2 – Exploration Plans (2 Pages)
- Exhibit A-3 – Summary of Boring Data
- Exhibit A-4 – GeoScoping Form (2 Pages)
- Exhibit A-5 – Field Exploration Description (2 Pages)
- Exhibit A-6 – Soil/Rock Description Terms (2 Pages)
- Exhibit A-7 – Soil/Rock Symbols
- Exhibit A-8 – Boring Logs (4 Pages)
- Exhibit A-9 – Rock Core Photograph Logs

Note: All exhibits are one page unless noted above

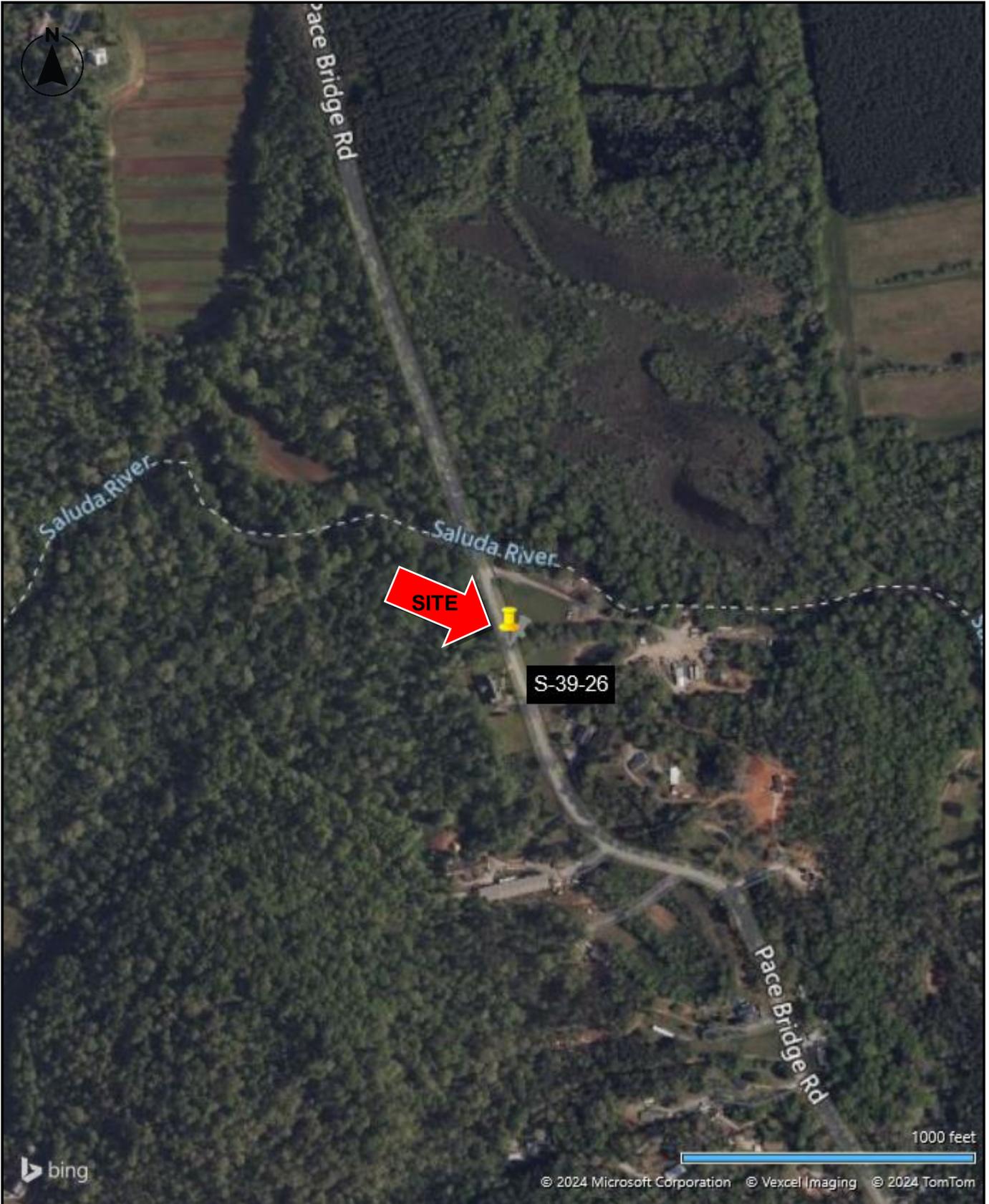


DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

AERIAL PHOTOGRAPHY PROVIDED BY MICROSOFT BING MAPS

Project Number	8623P180
Scale	AS SHOWN
Client	HNTB
Date	9/20/2024



72 Pointe Cir
Greenville, South Carolina 29615

SITE LOCATION	
S-39-26 BRO Tributary to South Saluda River	
Pace Bridge Road	
Pickens County, SC	

Exhibit
A-1

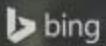


SPT Boring Location

S-39-26-2

S-39-26-1

50 feet



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DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

AERIAL PHOTOGRAPHY PROVIDED BY MICROSOFT BING MAPS

Project Number	8623P180
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Date	9/20/2024



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Greenville, South Carolina 29615

EXPLORATION PLAN
S-39-26 BRO Tributary to South Saluda River Pace Bridge Road Pickens County, SC

Exhibit
A-2



DIAGRAM IS FOR GENERAL LOCATION ONLY, AND IS NOT INTENDED FOR CONSTRUCTION PURPOSES

PRELIMINARY SITE PLAN PROVIDED BY HNTB

Project Number	8623P180
Scale	AS SHOWN
Client	HNTB
Date	9/20/2024



72 Pointe Cir
Greenville, South Carolina 29615

EXPLORATION PLAN

S-39-26 BRO Tributary to South Saluda River
Pace Bridge Road
Pickens County, SC

Exhibit

A-2

Summary of Boring Data – Exhibit A-3

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
Terracon Project No. 8623P180 | SCDOT Project ID: P043138



Summary of Boring Data

Boring No.	Ground Elevation (ft)	Test Depth (ft)	Northing (ft)	Easting (ft)	Latitude (°)	Longitude (°)	Station (ft) ¹	Offset (ft) ¹
S-39-26-1	916.72	69.5	1159885.36	1529783.68	35.011245°	-82.570163°	27+69	4 R
S-39-26-2	916.49	70.5	1159935.94	1529757.18	35.011383°	-82.570254°	28+26	5 L

1. Plans were provided by HNTB after the field exploration and survey. Station and offset values are estimated based on overlay in Google Earth™.
2. A composite bulk sample was collected about 7.5 feet west of S-39-26-1 and about 11 feet east of S-39-26-2.
3. Station and offset are based on the plans provided at the time the tests were performed.

GeoScoping Form

PROJECT INFORMATION			
Project ID:	P043138	Date of Trip:	8/14/2024
County:	Pickens	Location:	Marietta
Rd/ Route:	S-39-26	Local Name:	Pace Bridge Road
Attendees:	M. McKenney		

EXISTING BRIDGE INFORMATION			
Bridge Length:	45 ft	Bridge Width:	28 ft
Superstructure Type:	Concrete framing and decking	Substructure Type:	Timber and Steel H-Piles
Begin Bridge Sta ¹ :	27+64	End Bridge Sta ¹ :	28+34
Begin Bridge Embankment Sta ¹ :	26+64	End Bridge Embankment Sta ¹ :	29+34
Structure Number:	05605	Posted Weight Limit:	11 tons
Crossing:	Tributary to Saluda River	Skew:	N/A
Latitude:	35.011314°	Longitude:	-82.570205°
Existing Fill Height:	approximately 8 ft	Approx Existing Slope Angle:	2H:1V

1. Begin & End Bridge Embankment 100 ft down Sta. or up Sta., respectively. Sta. estimated from overlay of bridge plan provided by HNTB.

EXISTING ROADWAY EMBANKMENT INFORMATION			
Begin Project Sta:	27+10	Begin Bridge Embankment Sta:	26+64
Accessibility Issues:	None Observed		
Ground Cover:	Asphalt pavement and grass shoulder		
Existing Fill Height:	8 feet, sloping	Approx Existing Slope Angle:	2H:1V
Local Development:	developed - residential		
Topography:	graded slope to tributary		
Traffic Control Necessary:	No		
Surface Soils:	clayey sand	Muck:	No
Exposed Rock in Stream Bed:	No	Exposed Rock in banks:	No
Wetlands on Site:	Yes	Wetland Adjacent:	Yes
Depth FG to Water:	10 feet	Water Depth:	0.5 to 1 ft
Depth to Existing Ground:	approximately 11 feet at center of bridge		
Scour Condition at EB:	Critical	Scour Condition at IB:	Critical
End Bridge Embankment Sta:	29+34	End Project Sta:	29+60
Accessibility Issues:	None Observed		
Ground Cover:	Asphalt pavement and grass shoulder		
Existing Fill Height:	8 feet, sloping	Approx Existing Slope Angle:	2H:1V
Local Development:	developed - residential		
Topography:	graded slope to tributary		
Traffic Control Necessary:	No		
Surface Soils:	sandy silt	Muck:	No
Exposed Rock in Stream Bed:	No	Exposed Rock in banks:	No
Wetlands on Site:	Yes	Wetland Adjacent:	Yes
Depth FG to Water:	10 feet	Water Depth:	0.5 to 1 ft
Depth to Existing Ground:	approximately 11 feet at center of bridge		
Scour Condition at EB:	Critical	Scour Condition at IB:	Critical

GeoScoping Form

UTILITIES INFORMATION	
Attached:	N/A
Above Ground:	Overhead power was observed on the west side of the road
Underground:	N/A

Comments:

Field Exploration Description

Overview

The testing locations were proposed to and approved by SCDOT and located in the field by Terracon using measurements from existing structures shown on the provided drawings. The borings were surveyed by Thomas and Hutton, LLC after testing and drilling was complete. The locations as shown in the Exploration Plan are shown to the scale indicated.

A field log of each test location was prepared by our engineer. The final boring logs included with this report represent the engineer's description of the encountered conditions modified as necessary based on laboratory test results of the individual samples.

Soil Test Borings (STB)

All boring and sampling operations were conducted in general accordance with the following procedures:

- SCDOT Geotechnical Design Manual 2022
- Preconstruction Design Memorandum (PCDM) 11 - Supplemental Design Criteria for Low Volume Bridge Replacement Projects
- ASTM D5783, "Standard Guide for Use of Direct Rotary Drilling with Water-Based Drilling Fluid for Geo-environmental Exploration"
- ASTM D6151, "Standard Practice for Using Hollow-Stem Augers for Geotechnical Exploration and Soil Sampling"
- ASTM D1586 "Test Method for Penetration Test and Split-Barrel Sampling of Soils"
- ASTM D4220 "Standard Practices for Preserving and Transporting Soil"
- ASTM D2113 "Standard Practice for Rock Core Drilling and Sampling of Rock for Site Exploration"
- ASTM D5079 "Standard Practices for Preserving and Transporting Rock Core Samples"

Each soil test boring was advanced using rotary wash drilling techniques. The initial sampling program is summarized in the following table:

Test ID	Total Depth	Interval of Continuous Sampling
S-39-26-1	69.5 feet with 10 feet rock coring	0 to 10 feet
S-39-26-2	70.5 feet with 10 feet rock coring	0 to 10 feet
S-39-26-1/2 Offset	5 feet	Bulk Sample

1. Bulk sample was obtained with 2 ¼-inch Hollow Stem Auger (HSA).

Soil samples were obtained with a standard 1.4-inch I.D., 2-inch O.D., split-barrel sampler, also known as a standard split-spoon. The sampler is advanced into the soil a total of 18 to 24 inches by striking the drill rod using a 140-pound automatic hammer falling 30 inches.

Exhibit A-5 – Field Exploration Description

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
Terracon Project No. 8623P180 | SCDOT Project ID: P043138



The number of blows required to advance the sampler for each of three to four, 6-inch increments is recorded. The sum of the number of blows for the second and third increments is called the "Standard Penetration Value", or N-value (N_{meas} , blows per foot). The N-value, when properly evaluated, is an index to the soil strength.

Soil classification provides a general guide to the engineering properties of various soil types and enables the engineer to apply his experience to current situations. In our exploration, samples obtained during drilling operations are examined and visually classified by a geotechnical engineer using the procedures outlined in ASTM D2487 - Standard Classification of Soils for Engineering Purposes (Unified Soil Classification System). Laboratory testing was also performed on select split-spoon samples to evaluate index properties for further classification. The soils are described according to color, texture, and relative density or consistency (based on standard penetration resistance). The designations shown on the logs are described in the 2022 SCDOT Geotechnical Design Manual, Chapter 6.

The borings were advanced either to the planned drilling depth at which they were terminated, or to refusal of the drilling equipment. Select borings were continued below this depth using diamond bit rock coring techniques. NQ2 sized cores were recovered from the borehole. The rock recovery ratios (REC, percentage of the total core run), Rock Quality Designation (RQD, percentage of the total core run of pieces greater than 4 inches) were recorded along with a description of the rock. An explanation of the rock descriptions shown on the logs is provided in the SCDOT GDM Chapter 6. Photos of the recovered rock core specimens are provided in the Rock Core Photograph Log.

As practical, groundwater readings were collected from each of the soil test borings after 24 hours. These water levels are indicated on the boring logs. The borings were advanced using mud rotary drilling techniques. As the drilling method introduces water into the borehole, time-of-drilling water levels may not be reliable.

At the conclusion of the work, the boreholes and sounding holes were backfilled with the drill cuttings and clean sand. The upper 20 feet of those in the embankments were grouted with a cement bentonite grout and capped with cold-patch asphalt.

SOIL DESCRIPTION TERMS

Relative Density/Consistency Terms

<u>Relative Density</u> ¹			<u>Consistency</u> ²		
Descriptive Term	Relative Density	SPT Blow Count	Descriptive Term	Unconfined Compression Strength (q _u) (tsf)	SPT Blow Count
Very Loose	0 to 15%	4 and less	Very Soft	0.25 and less	2 and less
Loose	16 to 35%	5 to 10	Soft	0.26 to 0.50	3 to 4
Medium Dense	36 to 65%	11 to 30	Firm	0.51 to 1.00	5 to 8
Dense	66 to 85%	31 to 50	Stiff	1.01 to 2.00	9 to 15
Very Dense	86 to 100%	51 and more	Very Stiff	2.01 to 4.00	16 to 30
			Hard	4.01 and more	31 and more

Moisture Condition

<u>Descriptive Term</u>	<u>Criteria</u>
Dry	Absence of moisture, dusty, dry to the touch
Moist	Damp but no visible water
Wet	Visible free water, usually in coarse-grained soils below the water table

Color

Describe the sample color while sample is still moist.

Angularity¹

<u>Descriptive Term</u>	<u>Criteria</u>
Angular	Particles have sharp edges and relatively plane sides with unpolished surfaces.
Subangular	Particles are similar to angular description but have rounded edges.
Subrounded	Particles have nearly plane sides but have well-rounded corners and edges.
Rounded	Particles have smoothly curved sides and no edges.

HCl Reaction³

<u>Descriptive Term</u>	<u>Criteria</u>
None Reactive	No visible reaction
Weakly Reactive	Some reaction, with bubbles forming slowly
Strongly Reactive	Violent reaction, with bubbles forming immediately

Cementation³

<u>Descriptive Term</u>	<u>Criteria</u>
Weakly Cemented	Crumbles or breaks with handling or little finger pressure Moderately
Cemented	Crumbles or breaks with considerable finger pressure
Strongly Cemented	Will not crumble or break with finger pressure

Particle-Size Range¹

<u>Gravel</u>	Diameter, mm	Sieve Size	<u>Sand</u>	Diameter, mm	Sieve Size
Fine	4.76 to 19.1	#4 to ¾ inch	Fine	0.074 to 0.42	#200 to #40
Coarse	19.1 to 76.2	¾ inch to 3 inch	Medium	0.42 to 2.00	#40 to #10
			Coarse	4.00 to 4.76	#10 to #4

Primary Soil Type^{1, 2}

The primary soil type will be shown in all capital letters.

USCS Soil Designation

Indicate USCS soil designation as defined in ASTM D-2487 and D-2488

AASHTO Soil Designation

Indicate AASHTO soil designation as defined in AASHTO M-145 and ASTM D-3282

¹Applies to coarse-grained soils (major portion retained on No. 200 sieve)

²Applies to fine-grained soils (major portion passing No. 200 sieve)

³Use as required

DESCRIPTION OF ROCK PROPERTIES

WEATHERING

Fresh	Rock fresh, crystals bright, few joints may show slight staining. Rock rings under hammer if crystalline.
Very slight	Rock generally fresh, joints stained, some joints may show thin clay coatings, crystals in broken face show bright. Rock rings under hammer if crystalline.
Slight	Rock generally fresh, joints stained, and discoloration extends into rock up to 1 in. Joints may contain clay. In granitoid rocks some occasional feldspar crystals are dull and discolored. Crystalline rocks ring under hammer.
Moderate	Significant portions of rock show discoloration and weathering effects. In granitoid rocks, most feldspars are dull and discolored; some show clayey. Rock has dull sound under hammer and shows significant loss of strength as compared with fresh rock.
Moderately Severe	All rock except quartz discolored or stained. In granitoid rocks, all feldspars dull and discolored and majority show kaolinization. Rock shows severe loss of strength and can be excavated with geologist's pick.
Severe	All rock except quartz discolored or stained. Rock "fabric" clear and evident, but reduced in strength to strong soil. In granitoid rocks, all feldspars kaolinized to some extent. Some fragments of strong rock usually left.
Very severe	All rock except quartz discolored or stained. Rock "fabric" discernible, but mass effectively reduced to "soil" with only fragments of strong rock remaining.
Complete	Rock reduced to "soil". Rock "fabric" not discernible or discernible only in small, scattered locations. Quartz may be present as dikes or stringers.

HARDNESS (for engineering description of rock – not to be confused with Moh's scale for minerals)

Very hard	Cannot be scratched with knife or sharp pick. Breaking of hand specimens requires several hard blows of geologist's pick.
Hard	Can be scratched with knife or pick only with difficulty. Hard blow of hammer required to detach hand specimen.
Moderately hard	Can be scratched with knife or pick. Gouges or grooves to ¼ in. deep can be excavated by hard blow of point of a geologist's pick. Hand specimens can be detached by moderate blow.
Medium	Can be grooved or gouged 1/16 in. deep by firm pressure on knife or pick point. Can be excavated in small chips to pieces about 1-in. maximum size by hard blows of the point of a geologist's pick.
Soft	Can be gouged or grooved readily with knife or pick point. Can be excavated in chips to pieces several inches in size by moderate blows of a pick point. Small thin pieces can be broken by finger pressure.
Very soft	Can be carved with knife. Can be excavated readily with point of pick. Pieces 1-in. or more in thickness can be broken with finger pressure. Can be scratched readily by fingernail.

Joint, Bedding, and Foliation Spacing in Rock^a

Spacing	Joints	Bedding/Foliation
Less than 2 in.	Very close	Very thin
2 in. – 1 ft.	Close	Thin
1 ft. – 3 ft.	Moderately close	Medium
3 ft. – 10 ft.	Wide	Thick
More than 10 ft.	Very wide	Very thick

^aSpacing refers to the distance normal to the planes, of the described feature, which are parallel to each other or nearly so.

Rock Quality Designation (RQD)^a

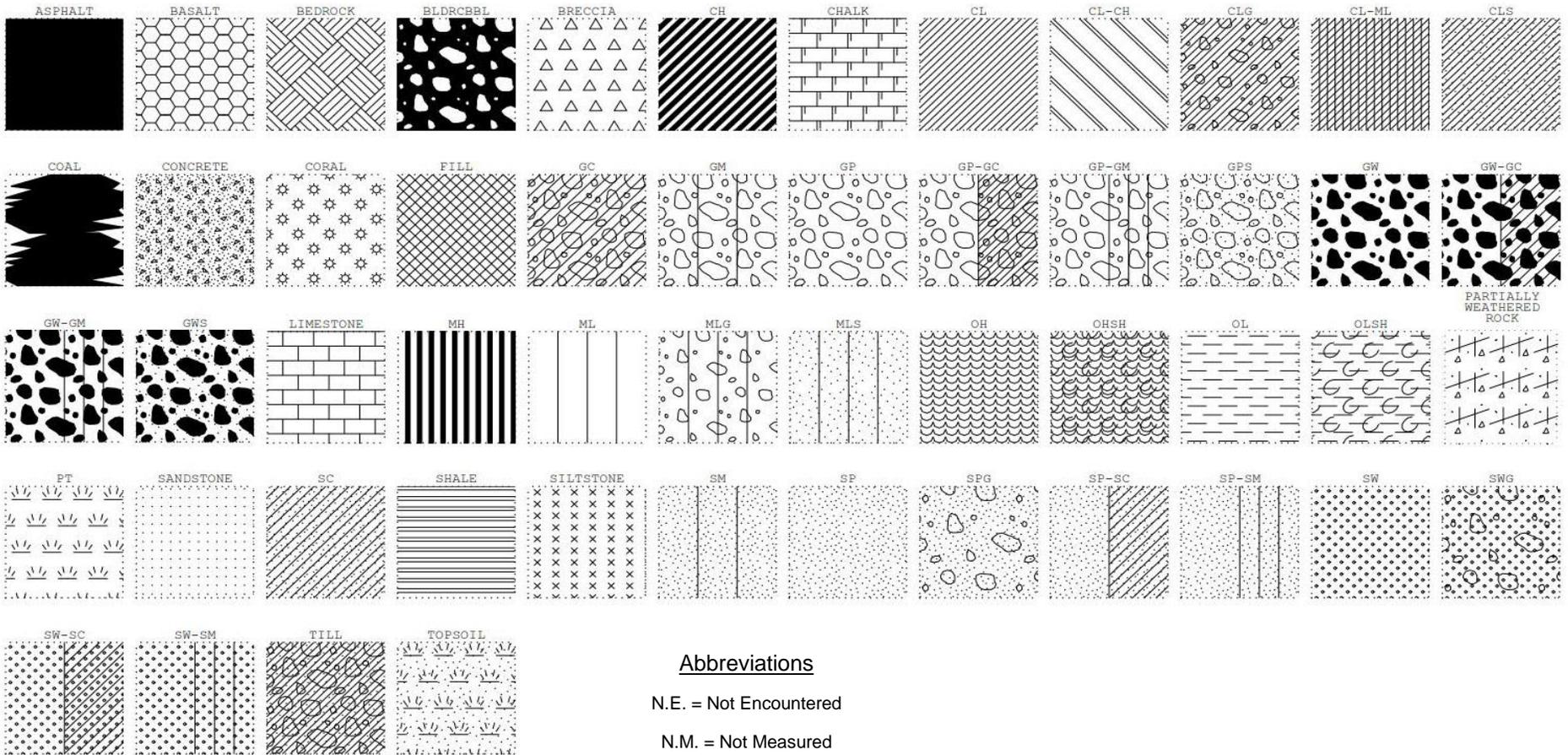
RQD, as a percentage	Diagnostic Description
Exceeding 90	Excellent
90 – 75	Good
75 – 50	Fair
50 – 25	Poor
Less than 25	Very poor

^aRQD (given as a percentage) = length of core in pieces 4 in. and longer/length of run.

Joint Openness Descriptors

Openness	Descriptor
No Visible Separation	Tight
Less than 1/32 in.	Slightly open
1/32 to 3/8 in.	Moderately open
1/8 to 3/8 in.	Open
3/8 in. to 0.1 ft.	Moderately wide
Greater than 0.1 ft.	Wide

References: American Society of Civil Engineers. Manuals and Reports on Engineering Practice - No. 56. Subsurface Investigation for Design and Construction of Foundations of Buildings. New York: American Society of Civil Engineers, 1976. U.S. Department of the Interior, Bureau of Reclamation, Engineering Geology Field Manual.



Abbreviations

N.E. = Not Encountered

N.M. = Not Measured

Project Manager:
MEM
Drawn by:
K.JZ
Checked by:
SG
Approved by:
DJC

Project No.
8623P180
Scale:
N.T.S.
File Name:
Soil - Rock - Log
Date:
Jul 2023



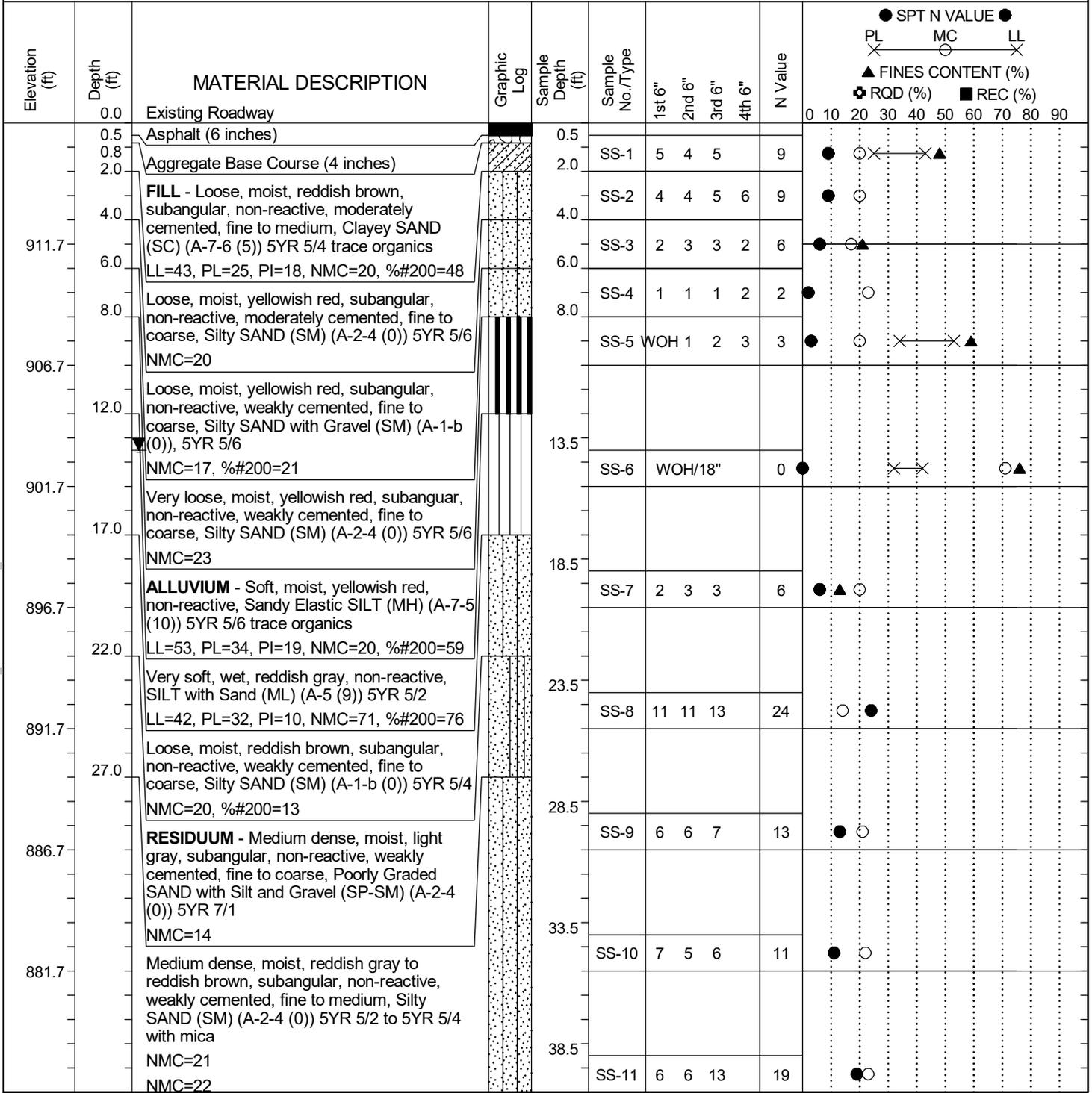
72 Pointe Circle
Greenville, SC 29615
PH. (864) 292-2901
FAX. (864) 292-6361

SOIL AND ROCK SYMBOLS

Exhibit A-7

SCDOT Soil Test Log

Project ID: P043138	County: Pickens	Boring No.: S-39-26-1
Site Description: S-39-26 BRO Tributary to South Saluda River	Route: S-39-26	
Eng./Geo.: S. Greaber	Boring Location: 27+69	Offset: 4 R
Alignment: Existing		
Elev.: 916.7 ft	Latitude: 35.01125	Longitude: -82.57016
Date Started: 8/14/2024		
Total Depth: 69.5 ft	Soil Depth: 59.5 ft	Core Depth: 10 ft
Date Completed: 8/14/2024		
Bore Hole Diameter (in): 4	Sampler Configuration	Liner Required: Y (N)
Liner Used: Y (N)		
Drill Machine: DR#1327	Drill Method: RW/RC	Hammer Type: Automatic
Energy Ratio: 92.6%		
Core Size: NQ2	Driller: B. Burnette	Groundwater: TOB N.M.
24HR: 13.5 ft		



LEGEND

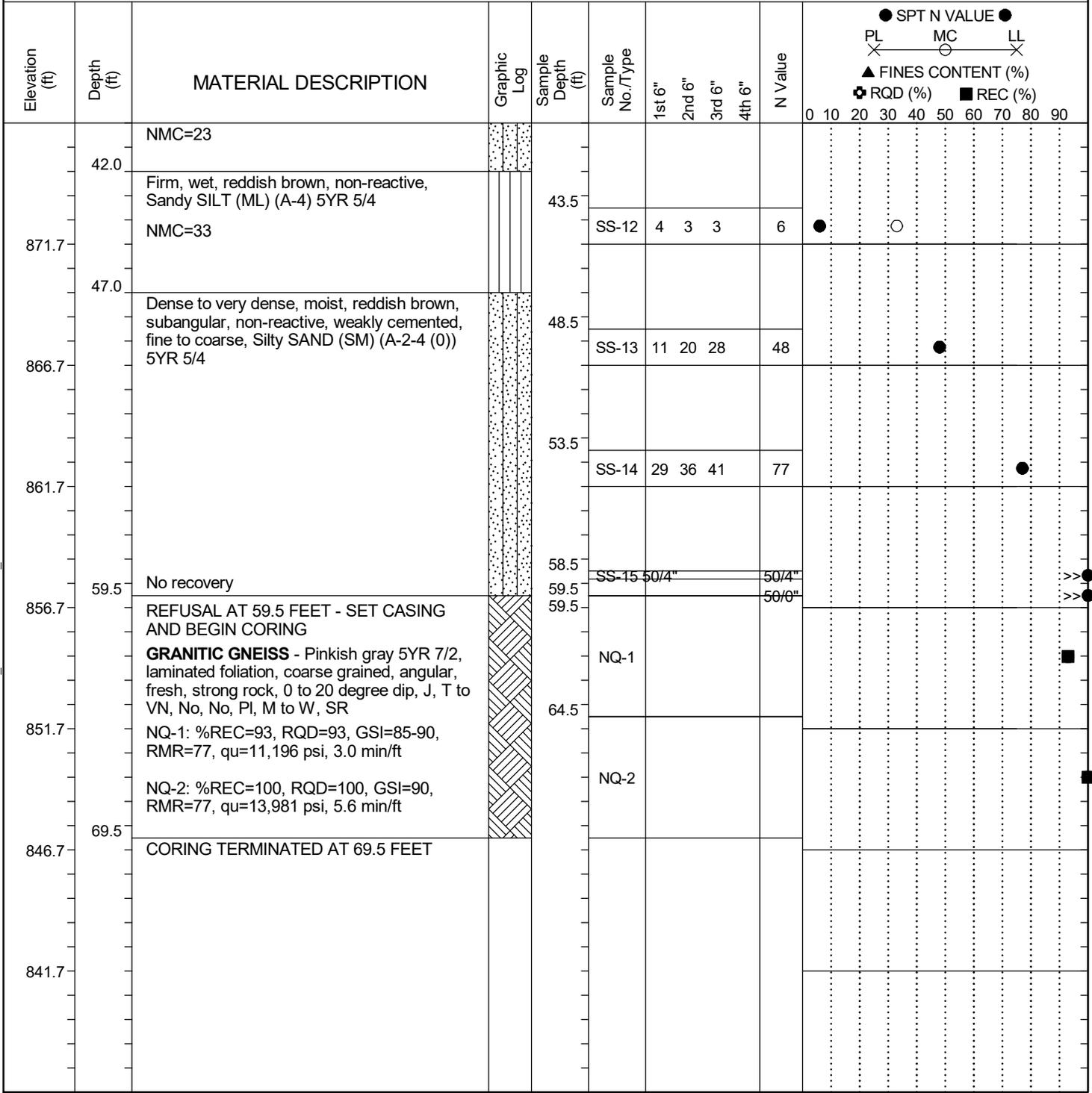
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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC.DOT 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER.DOT_JNA.GPJ SCDOT_DATATEMPLATE.GDT 9/26/24

SCDOT Soil Test Log

Project ID: P043138	County: Pickens	Boring No.: S-39-26-1
Site Description: S-39-26 BRO Tributary to South Saluda River		Route: S-39-26
Eng./Geo.: S. Greaber	Boring Location: 27+69	Offset: 4 R
Alignment: Existing		
Elev.: 916.7 ft	Latitude: 35.01125	Longitude: -82.57016
Date Started: 8/14/2024		
Total Depth: 69.5 ft	Soil Depth: 59.5 ft	Core Depth: 10 ft
Date Completed: 8/14/2024		
Bore Hole Diameter (in): 4	Sampler Configuration	Liner Required: Y (N)
Liner Used: Y (N)		
Drill Machine: DR#1327	Drill Method: RW/RC	Hammer Type: Automatic
Energy Ratio: 92.6%		
Core Size: NQ2	Driller: B. Burnette	Groundwater: TOB N.M.
24HR: 13.5 ft		



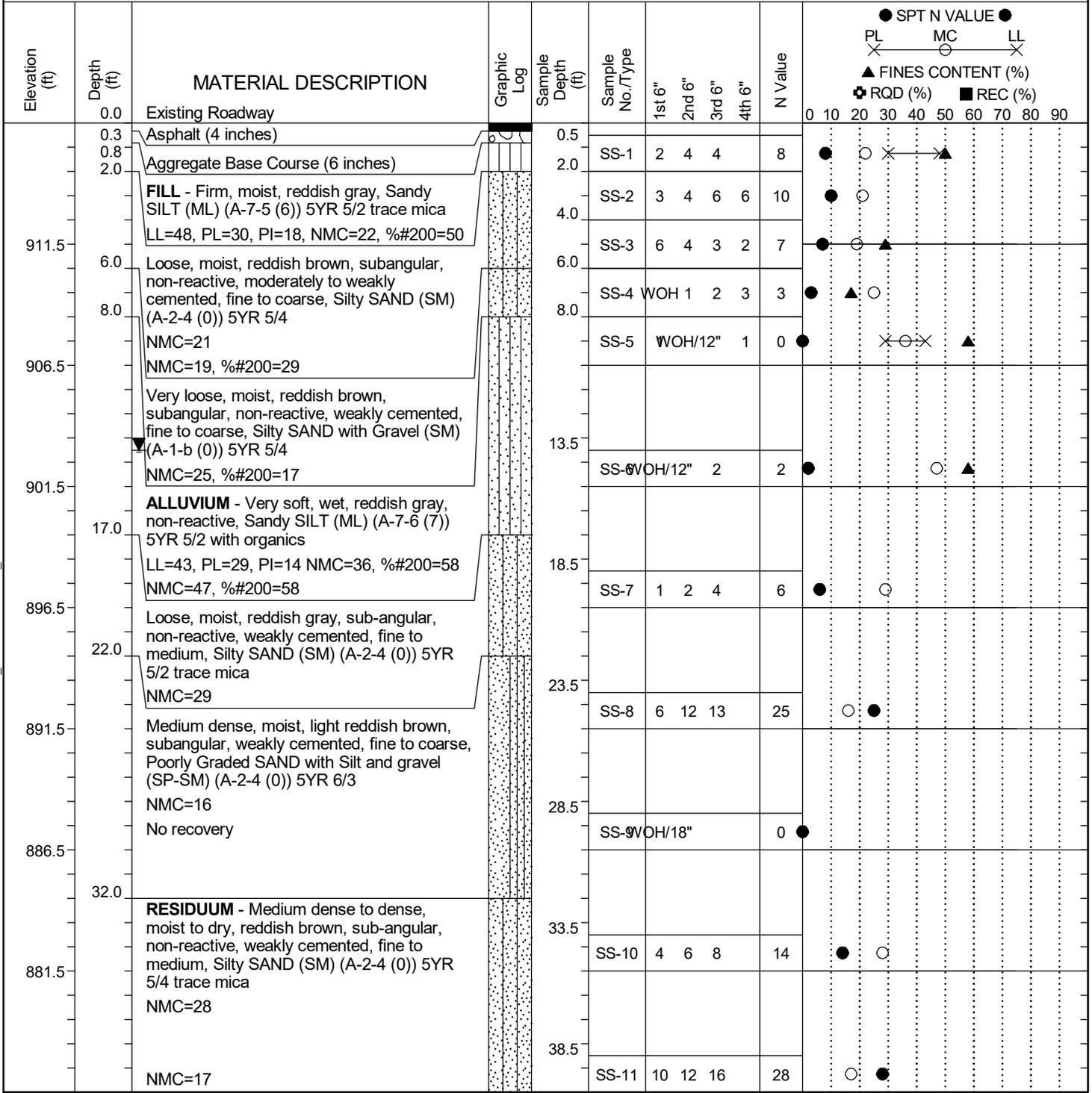
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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC.DOT 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER-DOT_JNA.GPJ SCDOT_DATATEMPLATE.GDT 9/26/24

SCDOT Soil Test Log

Project ID: P043138	County: Pickens	Boring No.: S-39-26-2
Site Description: S-39-26 BRO Tributary to South Saluda River		Route: S-39-26
Eng./Geo.: S. Greaber	Boring Location: 28+26	Offset: 5 L
Alignment: Existing	Elev.: 916.5 ft	Latitude: 35.01138
Longitude: -82.57025	Date Started: 8/20/2024	
Total Depth: 70.5 ft	Soil Depth: 60.5 ft	Core Depth: 10 ft
Date Completed: 8/20/2024	Bore Hole Diameter (in): 4	Sampler Configuration
Liner Required: Y (N)	Liner Used: Y (N)	
Drill Machine: DR#1327	Drill Method: RW/RC	Hammer Type: Automatic
Energy Ratio: 92.6%	Core Size: NQ2	Driller: B. Burnette
Groundwater: TOB	N.M.	24HR: 13.5 ft



LEGEND

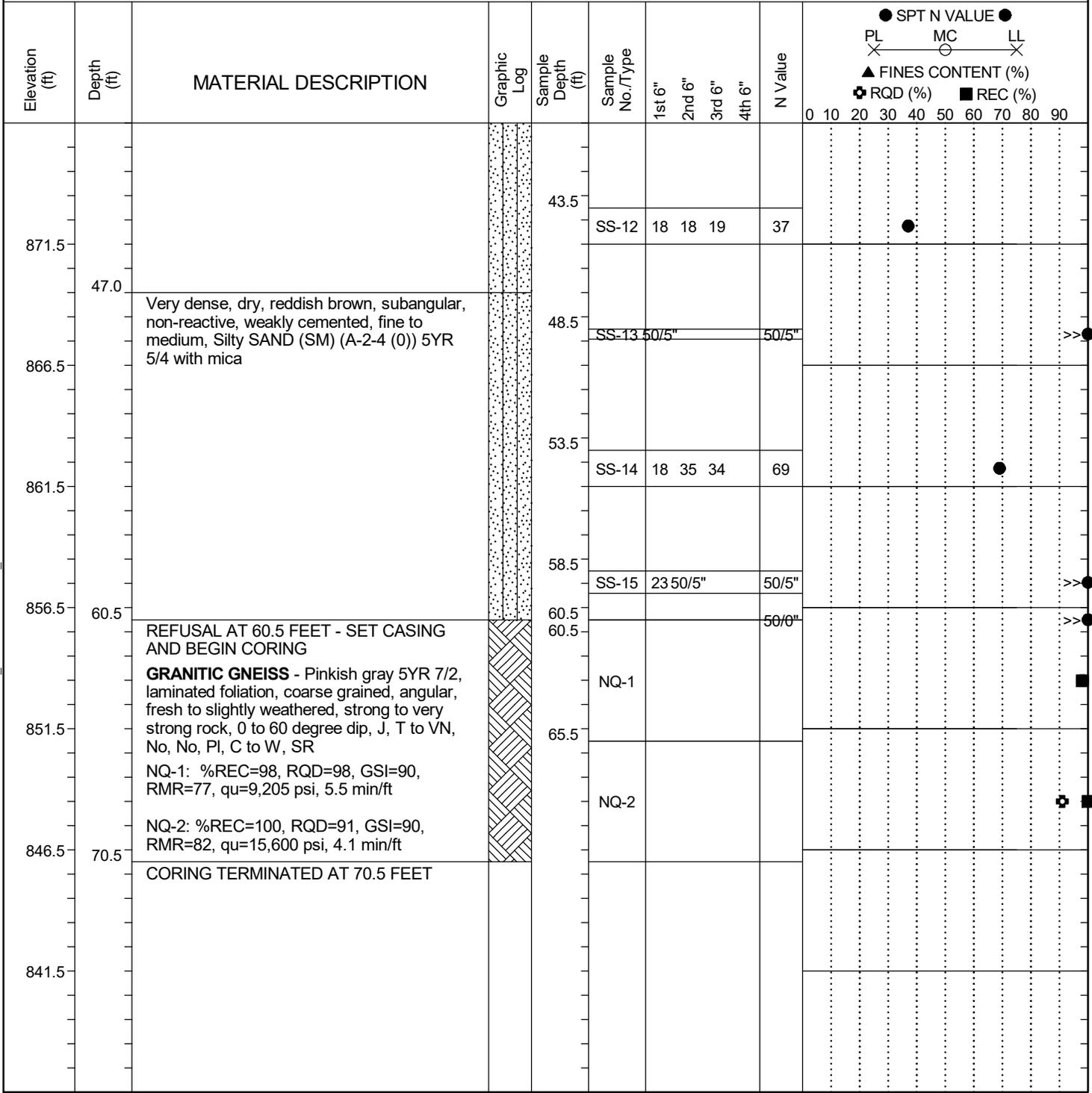
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SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

SC.DOT 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER.DOT_JNA.GPJ SCDOT DATATEMPLATE.GDT 9/26/24

SCDOT Soil Test Log

Project ID: P043138	County: Pickens	Boring No.: S-39-26-2
Site Description: S-39-26 BRO Tributary to South Saluda River		Route: S-39-26
Eng./Geo.: S. Greaber	Boring Location: 28+26	Offset: 5 L
Alignment: Existing		
Elev.: 916.5 ft	Latitude: 35.01138	Longitude: -82.57025
Date Started: 8/20/2024		
Total Depth: 70.5 ft	Soil Depth: 60.5 ft	Core Depth: 10 ft
Date Completed: 8/20/2024		
Bore Hole Diameter (in): 4	Sampler Configuration	Liner Required: Y (N)
Liner Used: Y (N)		
Drill Machine: DR#1327	Drill Method: RW/RC	Hammer Type: Automatic
Energy Ratio: 92.6%		
Core Size: NQ2	Driller: B. Burnette	Groundwater: TOB N.M.
24HR: 13.5 ft		



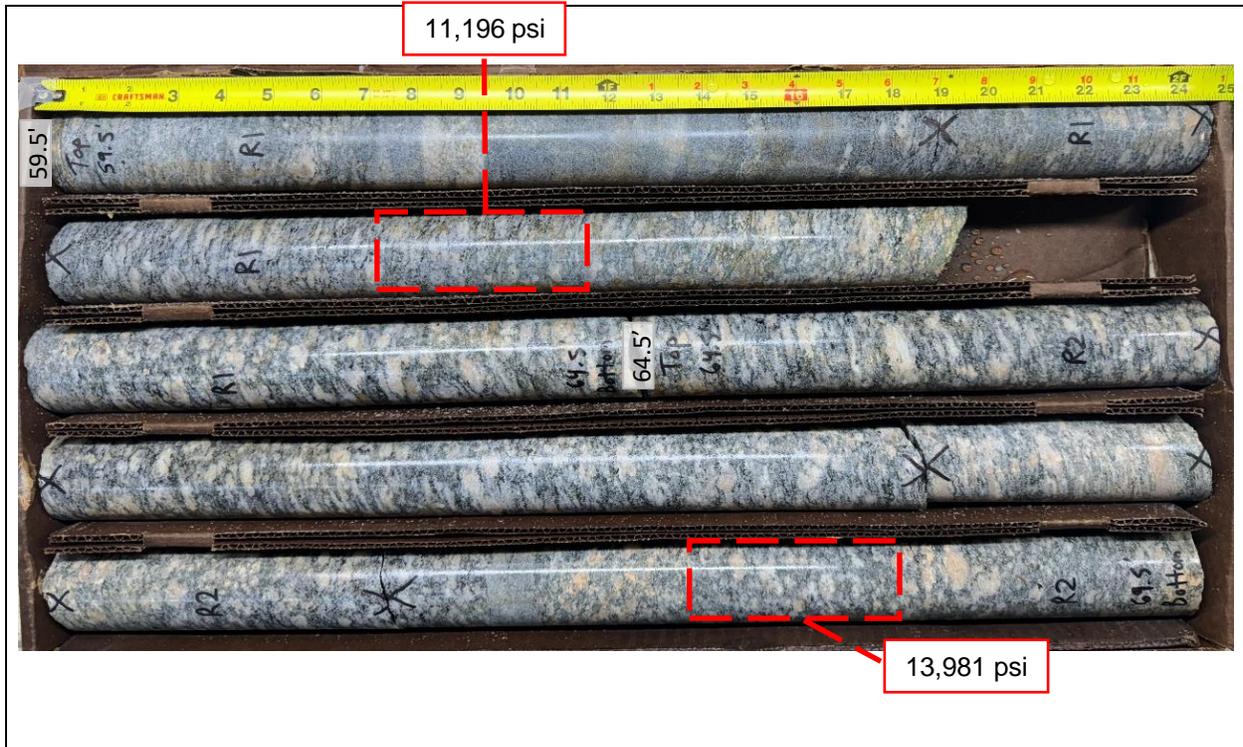
LEGEND

SAMPLER TYPE		DRILLING METHOD	
SS - Split Spoon	NQ - Rock Core, 1-7/8"	HSA - Hollow Stem Auger	RW - Rotary Wash
UD - Undisturbed Sample	CU - Cuttings	CFA - Continuous Flight Augers	RC - Rock Core
AWG - Rock Core, 1-1/8"	CT - Continuous Tube	DC - Driving Casing	

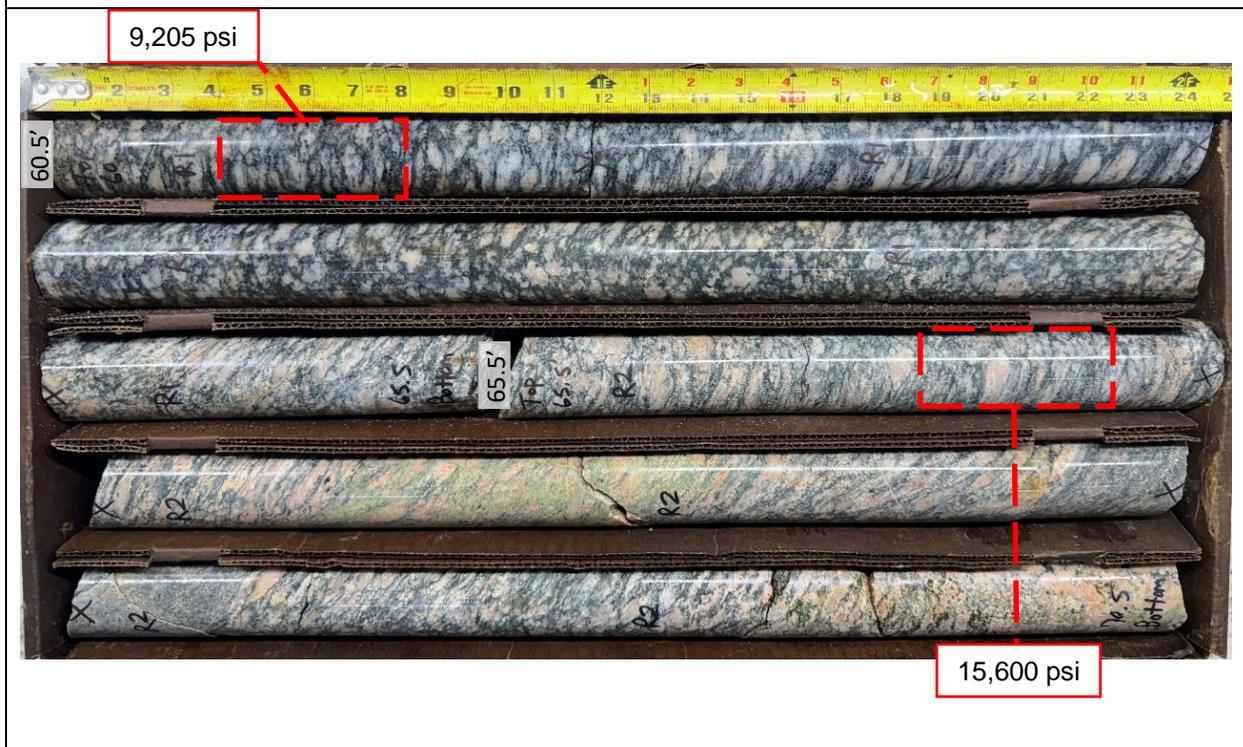
SC.DOT 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER.DOT_JNA.GPJ SCDOT DATATEMPLATE.GDT 9/26/24

Rock Core Photograph Logs – Exhibit A-9

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
Terracon Project No. 8623P180 | SCDOT Project ID: P043138



S-39-26-1, NQ-1 and NQ-2 (59.5 to 69.5 feet)



S-39-26-2, NQ-1 and NQ-2 (60.5 to 70.5 feet)

Appendix B – Laboratory Testing

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
Terracon Project No. 8623P180 | SCDOT Project ID: P043138



Appendix B

Laboratory Testing

Exhibit B-1 – Laboratory Testing Description
Summary of Laboratory Data (2 Pages)
Laboratory Data Sheets (20 Pages)

Note: All exhibits are one page unless noted above.

Summary of Laboratory Results

Boring ID	Depth (Ft.)	Soil Classification USCS & AASHTO	Liquid Limit	Plastic Limit	Plasticity Index	% Gravel	% Sand	% Fines	% Silt	% Clay	Water Content (%)	Proctor Dry Density (pcf)/Opt. Moisture (%)
S-39-26-1	0.5-2	CLAYEY SAND(SC) / A-7-6 (5)	43	25	18	2.6	49.9	47.5			19.5	
S-39-26-1	2-4	SILTY SAND(SM) / A-2-4 (0)									20.1	
S-39-26-1	4-6	SILTY SAND with GRAVEL(SM) / A-1-b (0)				18.9	60.2	20.9			16.6	
S-39-26-1	6-8	SILTY SAND(SM) / A-2-4 (0)									23.4	
S-39-26-1	8-10	SANDY ELASTIC SILT(MH) / A-7-5 (10)	53	34	19	1.1	40.3	58.7	24.0	34.6	19.5	
S-39-26-1	13.5-15	SILT WITH SAND(ML) / A-5 (9)	42	32	10	0.0	24.3	75.7	38.4	37.3	70.6	
S-39-26-1	18.5-20	SILTY SAND(SM) / A-1-b (0)				5.0	82.5	12.5			20.1	
S-39-26-1	23.5-25	POORLY GRADED SAND with SILT and GRAVEL(SP-SM) / A-2-4 (0)									14.0	
S-39-26-1	28.5-30	SILTY SAND(SM) / A-2-4 (0)									20.9	
S-39-26-1	33.5-35	SILTY SAND(SM) / A-2-4 (0)									22.4	
S-39-26-1	38.5-40	SILTY SAND(SM) / A-2-4 (0)									22.6	
S-39-26-1	43.5-45	SANDY SILT(ML) / A-4									33.1	
S-39-26-2	0.5-2	SANDY SILT(ML) / A-7-5 (6)	48	30	18	0.0	49.6	50.4			22.3	
S-39-26-2	2-4	SILTY SAND(SM) / A-2-4 (0)									21.3	
S-39-26-2	4-6	SILTY SAND(SM) / A-2-4 (0)				8.0	62.6	29.4			19.3	
S-39-26-2	6-8	SILTY SAND with GRAVEL(SM) / A-1-b (0)				26.5	56.5	17.0	8.4	8.6	24.8	
S-39-26-2	8-10	SANDY SILT(ML) / A-7-6 (7)	43	29	14	0.0	42.4	57.6	28.7	28.9	35.5	
S-39-26-2	13.5-15	SANDY SILT(ML) / A-7-6 (7)				0.0	41.9	58.1			47.4	
S-39-26-2	18.5-20	SILTY SAND(SM) / A-2-4 (0)									28.5	



INDEX PROPERTIES VERSUS DEPTH

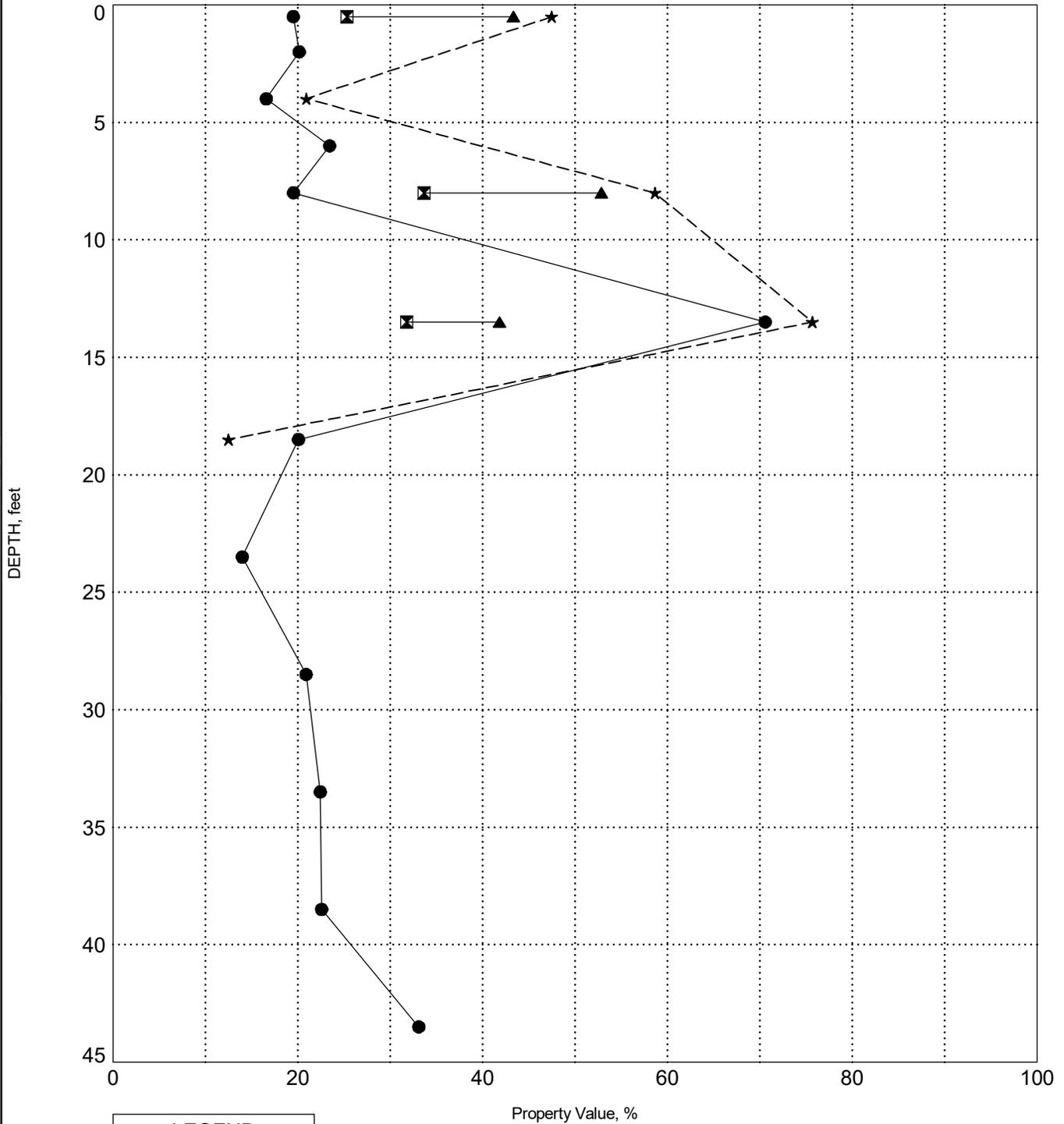
PROJECT ID P043138

PROJECT NAME S-39-26 BRO Tributary to South Saluda River

PROJECT COUNTY Pickens

BORING S-39-26-1

SURFACE ELEVATION: 916.7



LEGEND	
●	Water Content
☒	Plastic Limit
▲	Liquid Limit
★	Fines

INDEX PROPS 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER-DOT_JNA.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 9/26/24



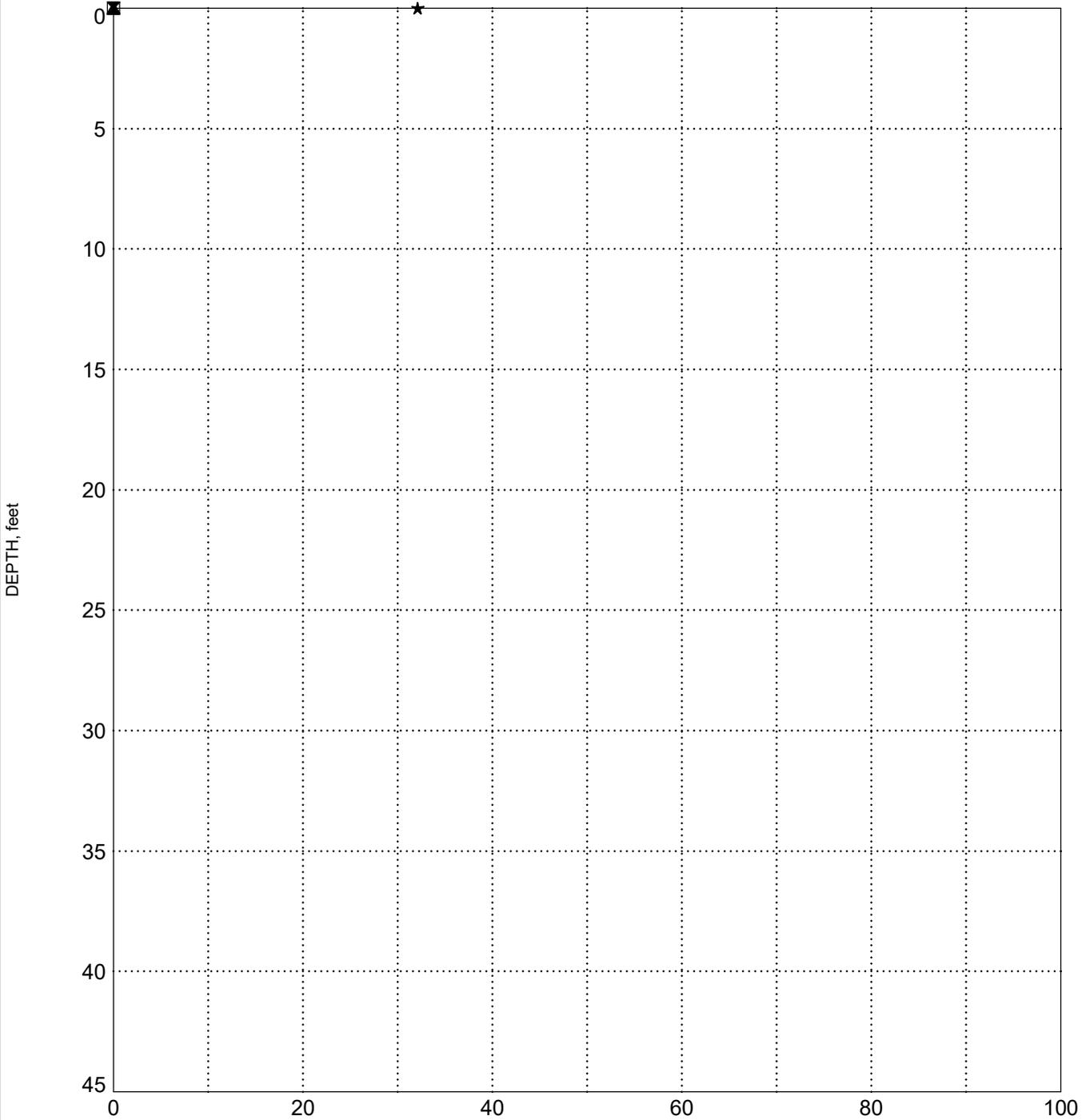
INDEX PROPERTIES VERSUS DEPTH

PROJECT ID P043138

PROJECT NAME S-39-26 BRO Tributary to South Saluda River

PROJECT COUNTY Pickens

BORING S-39-26-1/2 Offset



INDEX PROPS 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER-DOT_JNA.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 9/26/24

LEGEND	
●	Water Content
☒	Plastic Limit
▲	Liquid Limit
★	Fines



INDEX PROPERTIES VERSUS DEPTH

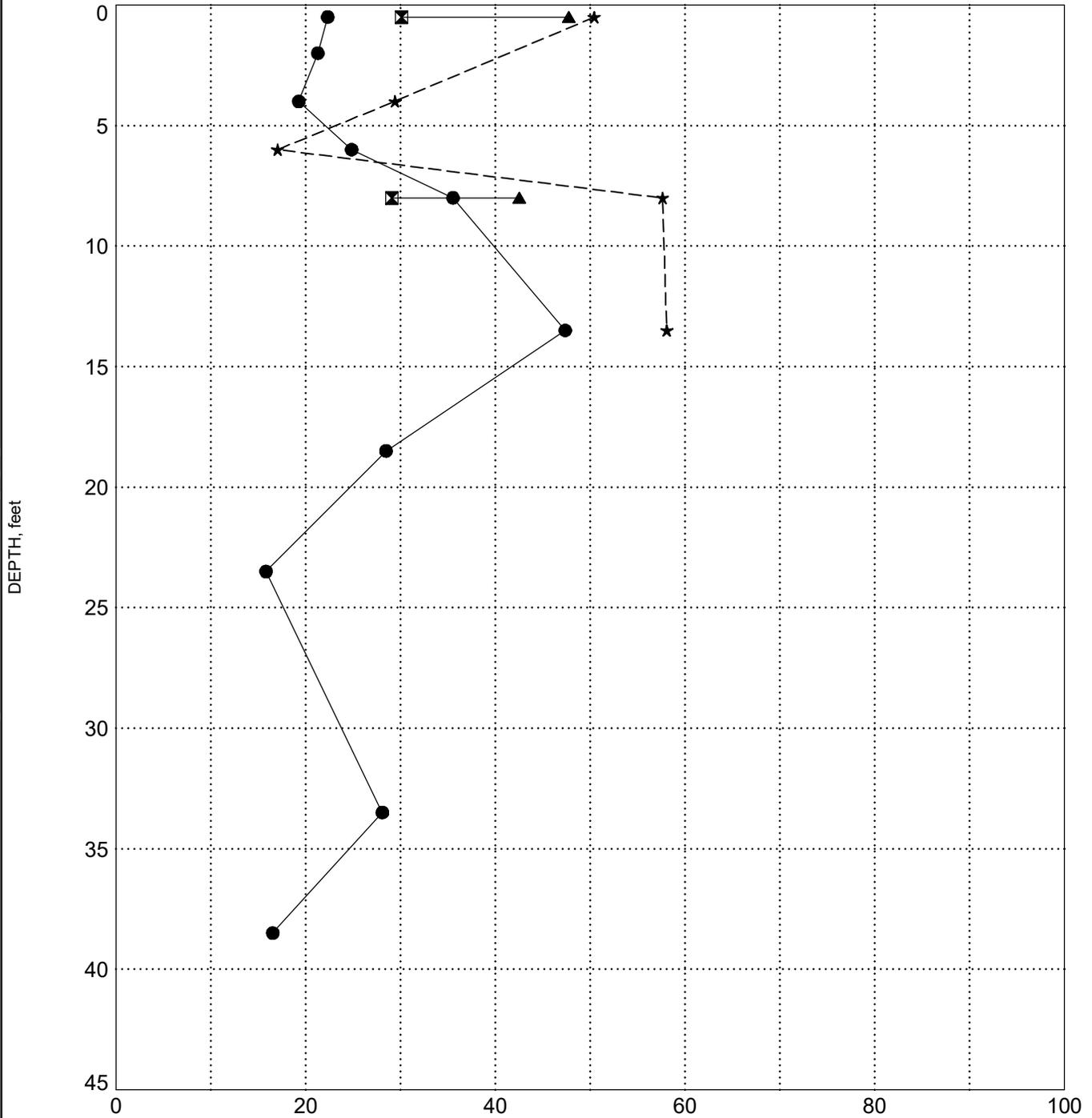
PROJECT ID P043138

PROJECT NAME S-39-26 BRO Tributary to South Saluda River

PROJECT COUNTY Pickens

SURFACE ELEVATION: 916.5

BORING S-39-26-2

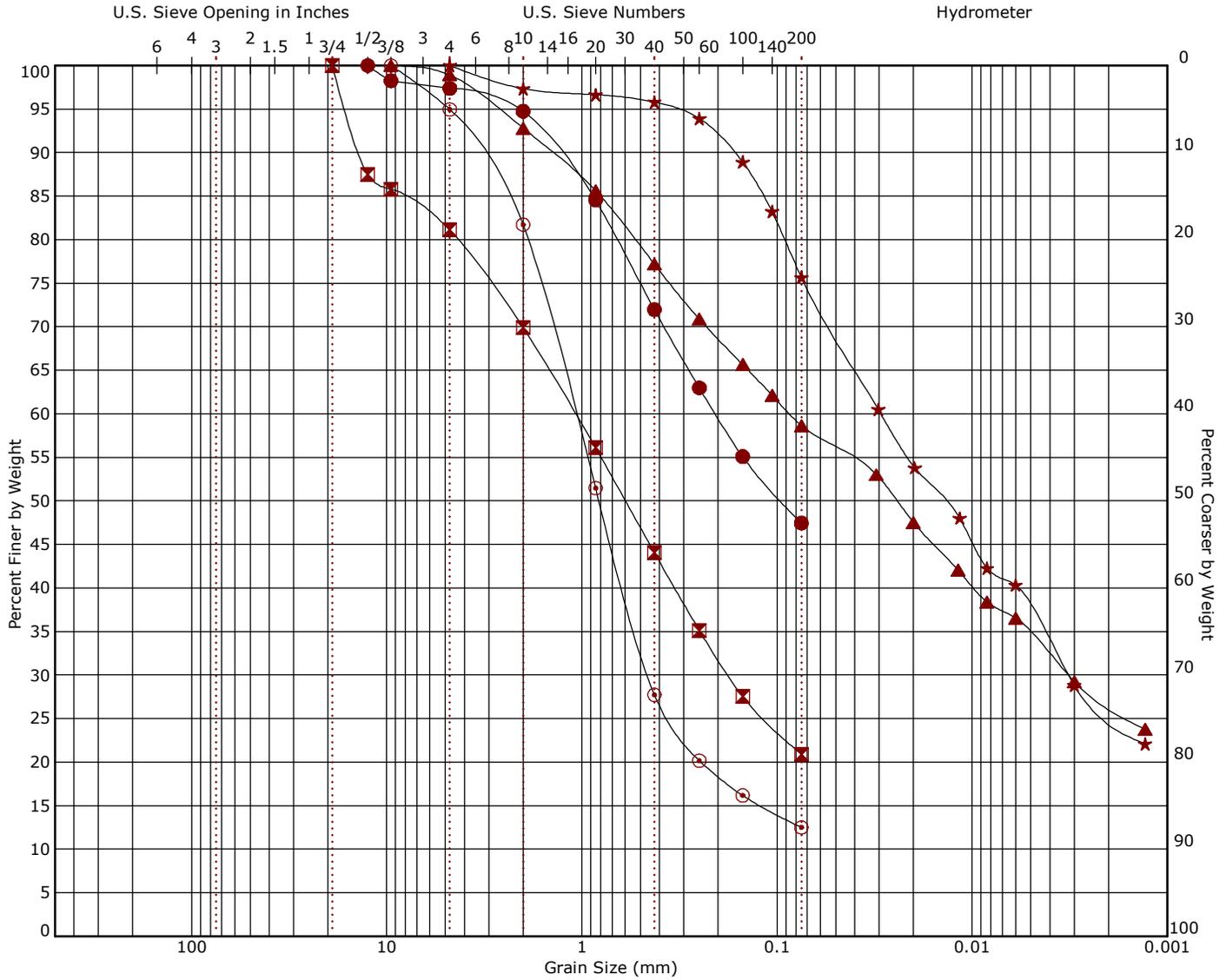


LEGEND	
●	Water Content
■	Plastic Limit
▲	Liquid Limit
★	Fines

INDEX PROPS 8623P180T SCDOT BRIDGE PACK 19 OVER TRIB TO SOUTH SALUDA RIVER-DOT_JNA.GPJ SCDOT DATA TEMPLATE 01_30_2015.GDT 9/26/24

Grain Size Distribution

ASTM D422 / ASTM C136

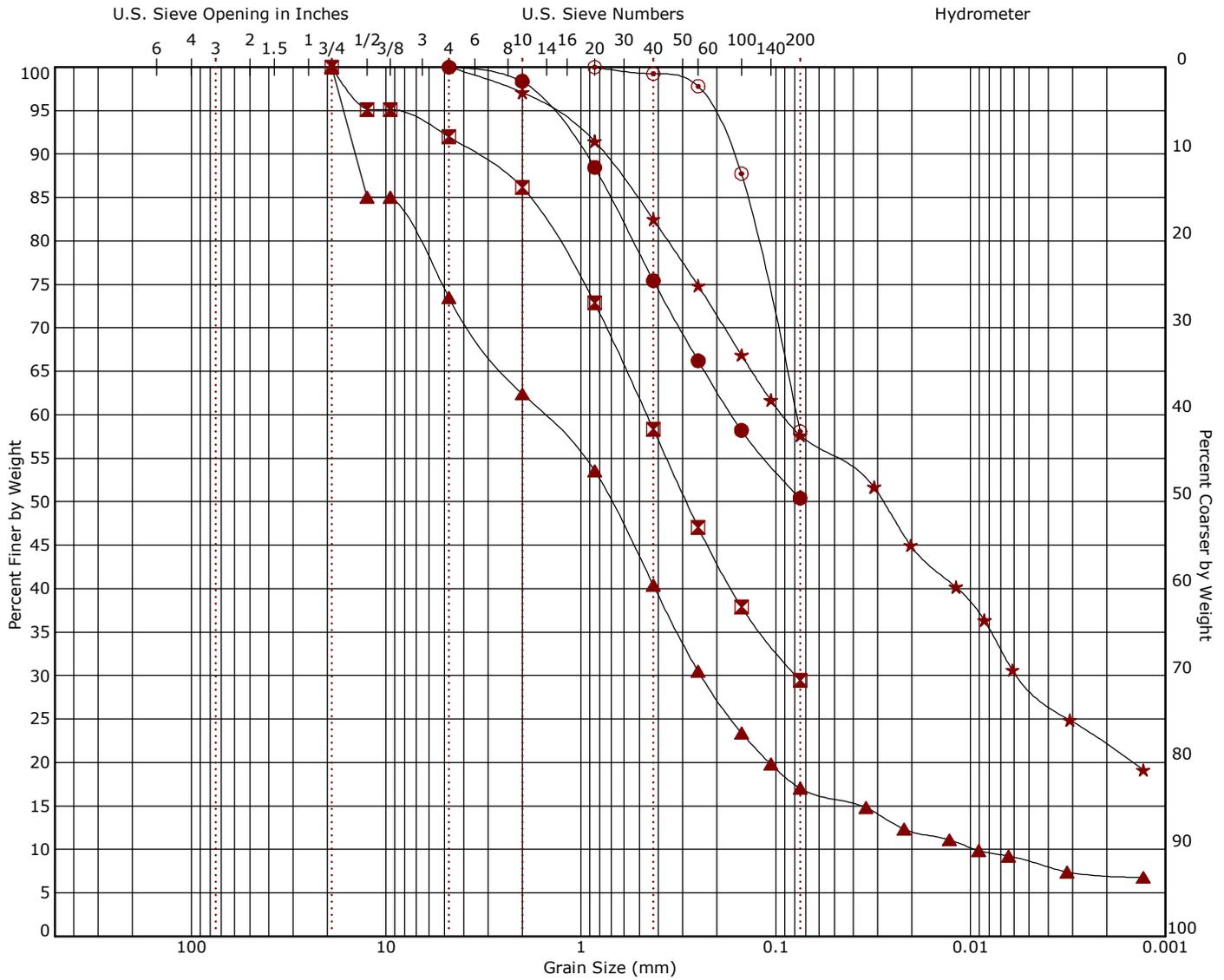


Boring ID	Depth (Ft)	USCS Classification	USCS	AASHTO	LL	PL	PI	Cc	Cu
● S-39-26-1	0.5 - 2	CLAYEY SAND	SC	A-7-6 (5)	43	25	18		
☒ S-39-26-1	4 - 6	SILTY SAND with GRAVEL	SM	A-1-b (0)					
▲ S-39-26-1	8 - 10	SANDY ELASTIC SILT	MH	A-7-5 (10)	53	34	19		
★ S-39-26-1	13.5 - 15	SILT with SAND	ML	A-5 (9)	42	32	10		
⊙ S-39-26-1	18.5 - 20	SILTY SAND	SM	A-1-b (0)					

Boring ID	Depth (Ft)	D ₁₀₀	D ₆₀	D ₃₀	D ₁₀	%Cobbles	%Gravel	%Sand	%Fines	%Silt	%Clay
● S-39-26-1	0.5 - 2	12.5	0.206			0.0	2.6	49.9	47.5		
☒ S-39-26-1	4 - 6	19	1.081	0.177		0.0	18.9	60.2	20.9		
▲ S-39-26-1	8 - 10	9.5	0.086	0.003		0.0	1.1	40.3		24.0	34.6
★ S-39-26-1	13.5 - 15	4.75	0.029	0.003		0.0	0.0	24.3		38.4	37.3
⊙ S-39-26-1	18.5 - 20	9.5	1.082	0.454		0.0	5.0	82.5	12.5		

Grain Size Distribution

ASTM D422 / ASTM C136

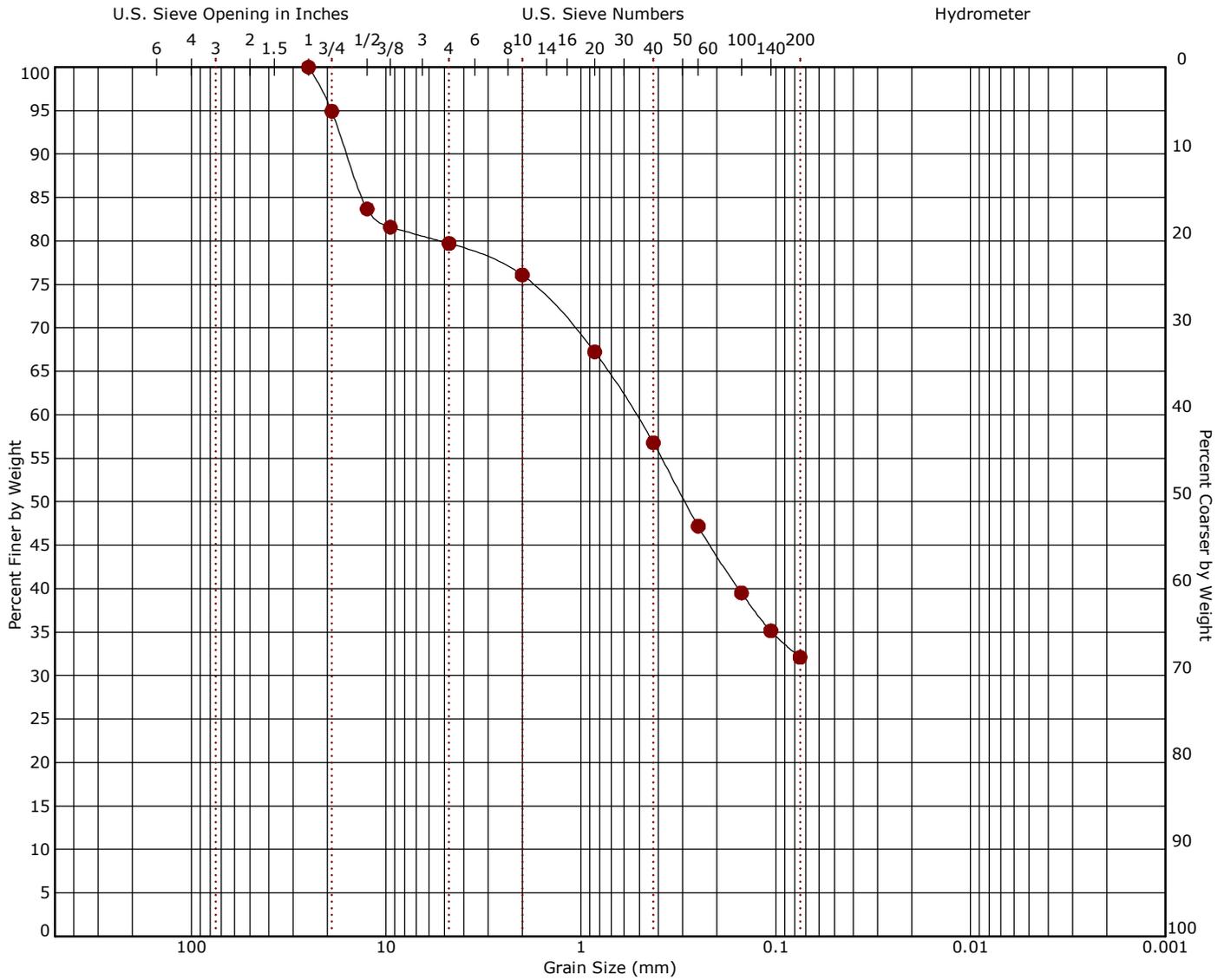


Boring ID	Depth (Ft)	USCS Classification	USCS	AASHTO	LL	PL	PI	Cc	Cu
● S-39-26-2	0.5 - 2	SANDY SILT	ML	A-7-5 (6)	48	30	18		
☒ S-39-26-2	4 - 6	SILTY SAND	SM	A-2-4 (0)					
▲ S-39-26-2	6 - 8	SILTY SAND with GRAVEL	SM	A-1-b (0)				3.90	167.98
★ S-39-26-2	8 - 10	SANDY SILT	ML	A-7-6 (7)	43	29	14		
⊙ S-39-26-2	13.5 - 15	SANDY SILT	ML	A-7-6 (7)					

Boring ID	Depth (Ft)	D ₁₀₀	D ₆₀	D ₃₀	D ₁₀	%Cobbles	%Gravel	%Sand	%Fines	%Silt	%Clay
● S-39-26-2	0.5 - 2	4.75	0.168			0.0	0.0	49.6	50.4		
☒ S-39-26-2	4 - 6	19	0.46	0.079		0.0	8.0	62.6	29.4		
▲ S-39-26-2	6 - 8	19	1.584	0.241	0.009	0.0	26.5	56.5		8.4	8.6
★ S-39-26-2	8 - 10	4.75	0.092	0.006		0.0	0.0	42.4		28.7	28.9
⊙ S-39-26-2	13.5 - 15	0.85	0.078			0.0	0.0	41.9	58.1		

Grain Size Distribution

ASTM D422 / ASTM C136



Cobbles |
 Gravel |
 Sand |
 Silt or Clay

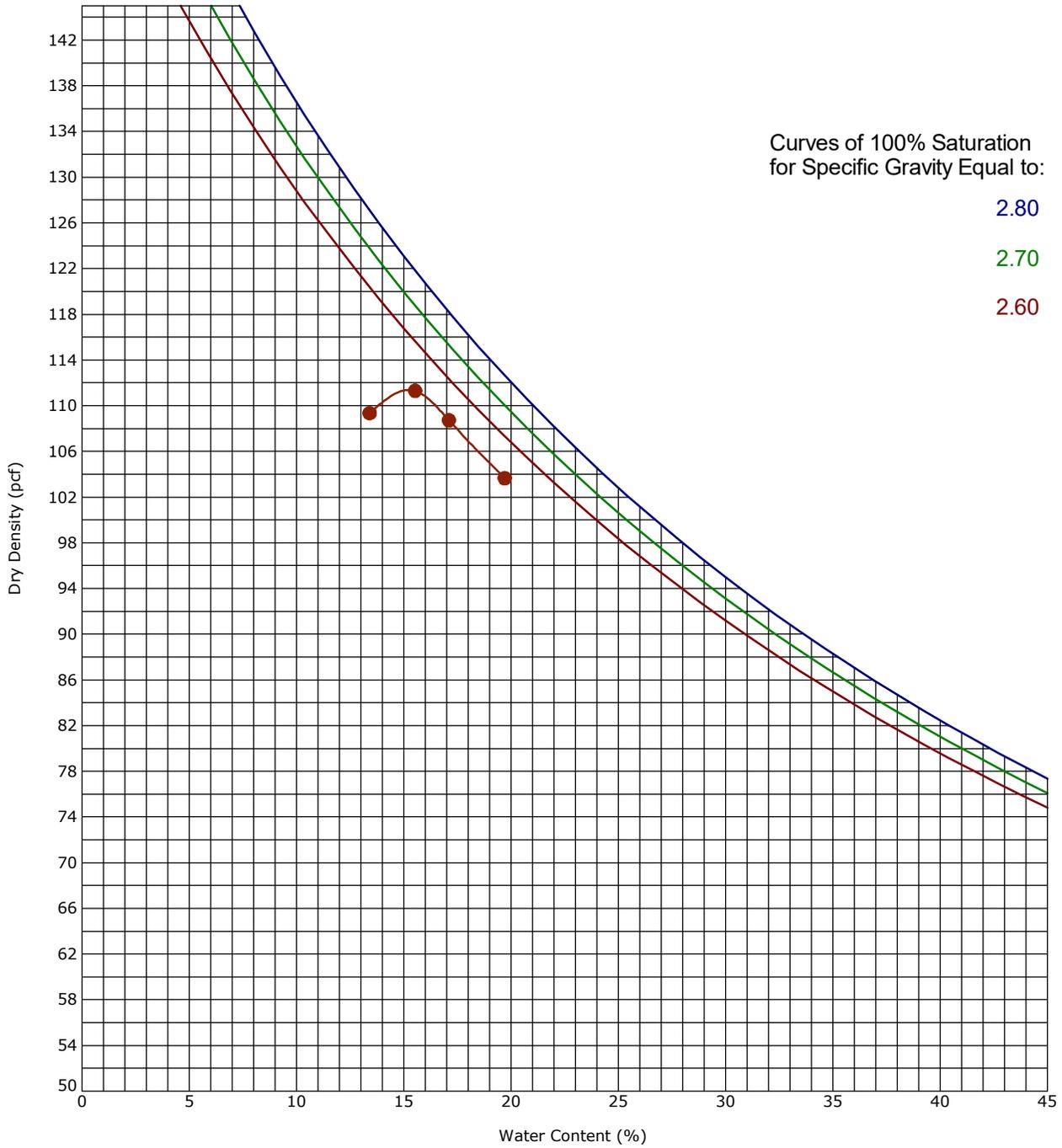
coarse | fine | coarse | medium | fine

Boring ID	Depth (Ft)	USCS Classification	USCS	AASHTO	LL	PL	PI	Cc	Cu
S-39-26-1/2 Offset	0 - 5	SILTY SAND with GRAVEL	SM	A-2-4 (0)	NP	NP	NP		

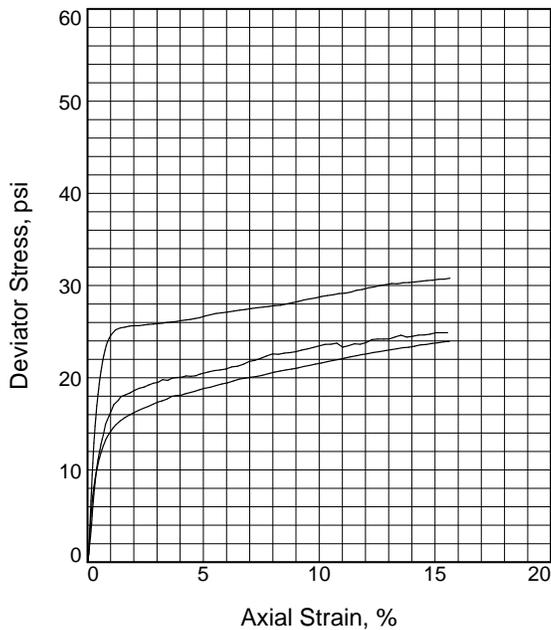
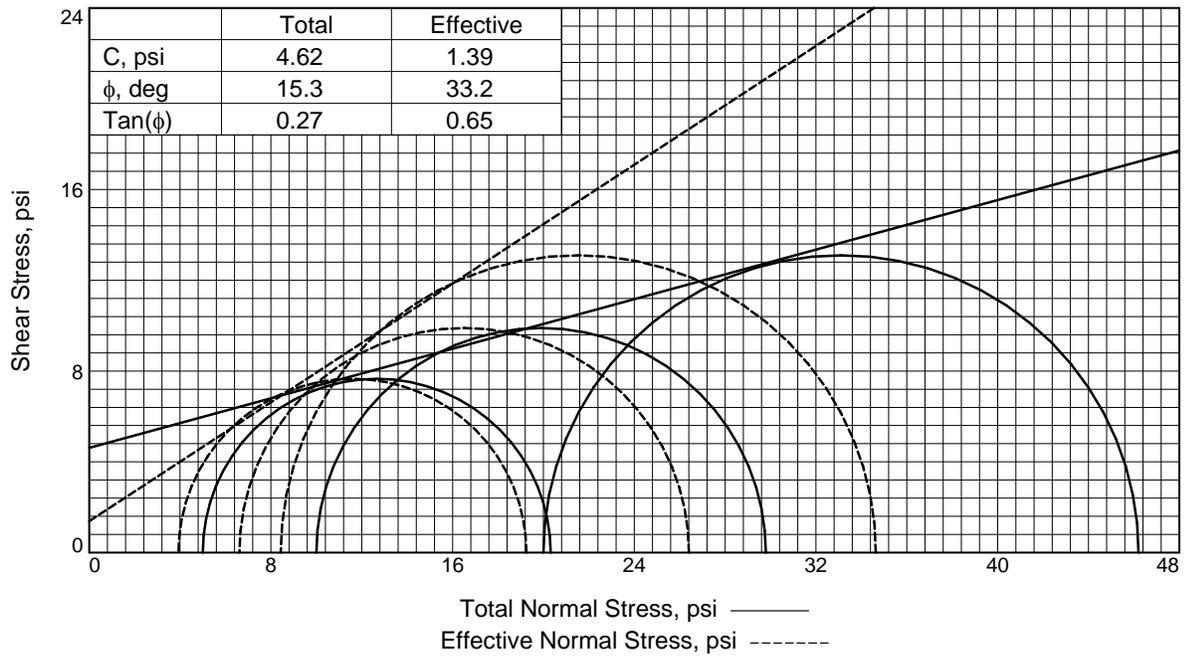
Boring ID	Depth (Ft)	D ₁₀₀	D ₆₀	D ₃₀	D ₁₀	%Cobbles	%Gravel	%Sand	%Fines	%Silt	%Clay
S-39-26-1/2 Offset	0 - 5	25	0.526			0.0	20.3	47.6	32.1		

Moisture-Density Relationship

ASTM D698-Method B



Boring ID		Depth (Ft)		Description of Materials				
S-39-26-1/2 Offset		0 - 5		SILTY SAND with GRAVEL(SM)				
Fines (%)	Fraction > mm size	LL	PL	PI	Test Method	Maximum Dry Density (pcf)	Optimum Water Content (%)	
32	0.0	NP	NP	NP	ASTM D698-Method B	111.4	15.2	



Sample No.	1	2	3	
Initial	Water Content, %	15.0	14.9	15.3
	Dry Density, pcf	106.2	106.4	106.0
	Saturation, %	69.1	68.6	70.2
	Void Ratio	0.5868	0.5848	0.5896
	Diameter, in.	2.80	2.80	2.80
	Height, in.	5.62	5.62	5.62
At Test	Water Content, %	20.0	20.0	19.9
	Dry Density, pcf	109.4	109.4	109.7
	Saturation, %	100.0	100.0	100.0
	Void Ratio	0.5409	0.5412	0.5369
	Diameter, in.	2.77	2.77	2.76
	Height, in.	5.58	5.58	5.57
Strain rate, in./min.	0.001	0.001	0.001	
Back Pressure, psi	50.0	50.0	50.0	
Cell Pressure, psi	55.0	60.0	70.0	
Fail. Stress, psi	15.3	19.8	26.2	
Excess Pore Pr., psi	1.1	3.4	11.6	
Ult. Stress, psi	23.8	24.9	30.7	
Excess Pore Pr., psi	-2.4	1.4	9.6	
$\bar{\sigma}_1$ Failure, psi	19.2	26.4	34.6	
$\bar{\sigma}_3$ Failure, psi	3.9	6.6	8.4	

Type of Test:

CU with Pore Pressures

Sample Type: Remolded

Description: Silty Sand with Gravel (SM)

LL= NV

PI= NP

Specific Gravity= 2.7

Remarks: Specimens were remolded to approximately 95% MDD at optimum water content.

Figure _____

Client: HNTB North Carolina PC

Project: S-39-26 BRO Tributary to South Saluda River

Source of Sample: S-39-26-1/2 Offset **Depth:** 0-5'

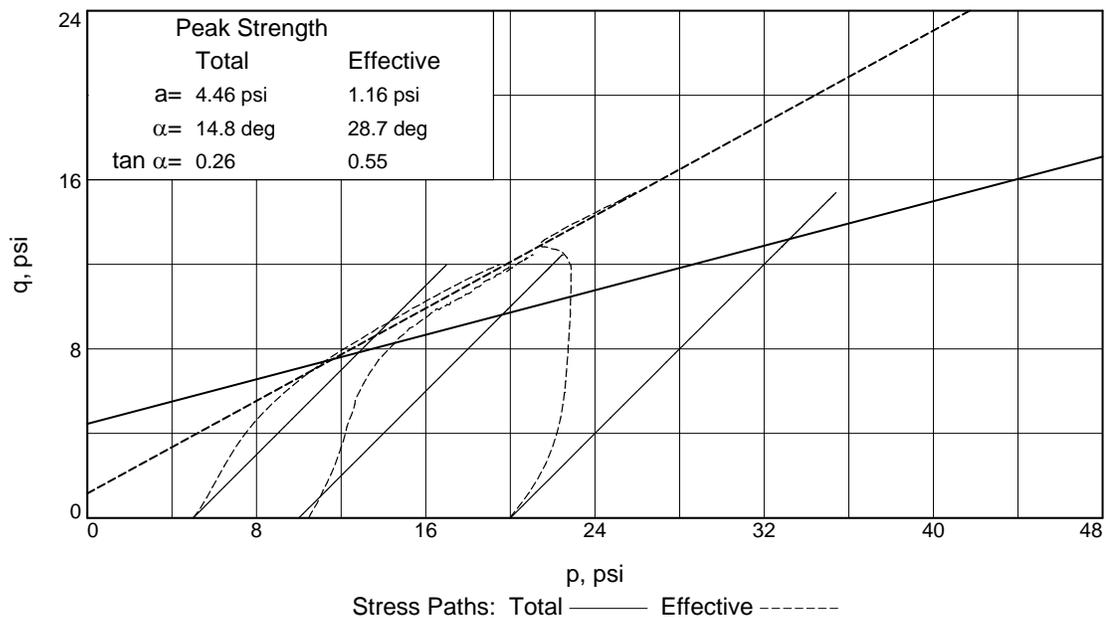
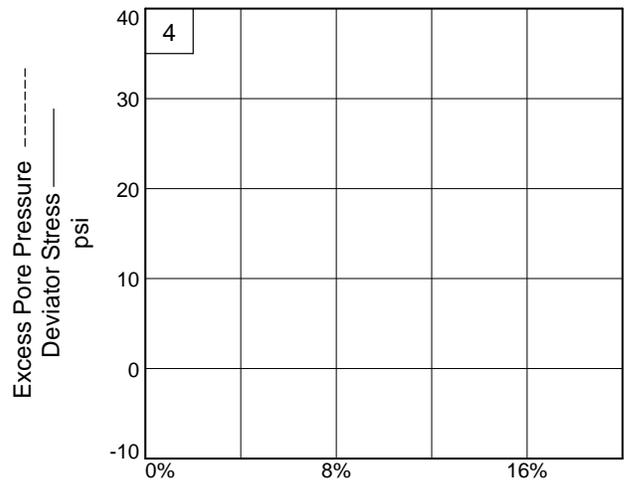
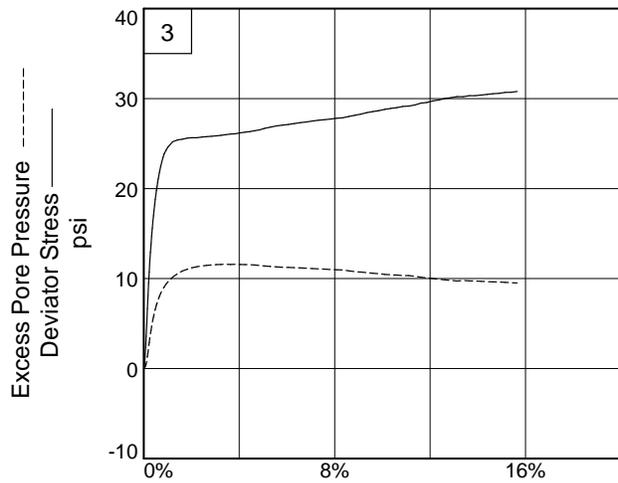
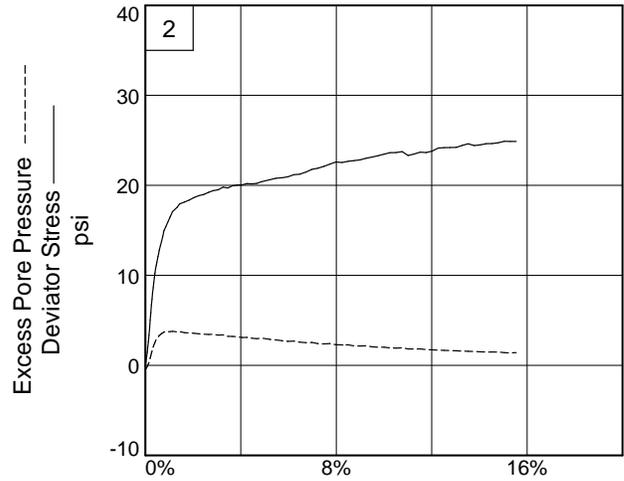
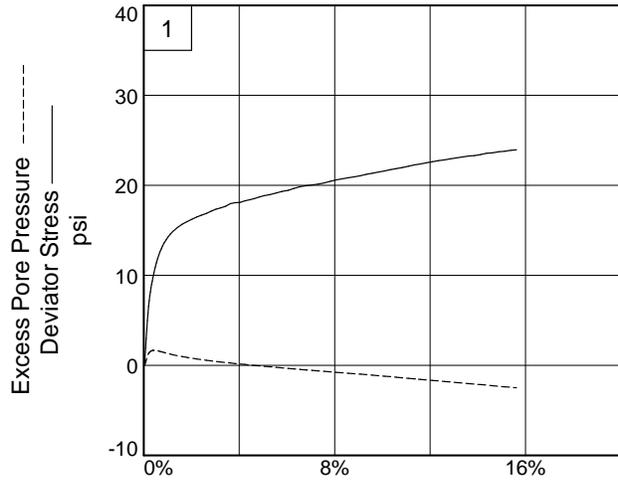
Proj. No.: 8623P180

Date Sampled: N/A

TRIAxIAL SHEAR TEST REPORT

Terracon Consultants, Inc.

Chattanooga, TN



Client: HNTB North Carolina PC

Project: S-39-26 BRO Tributary to South Saluda River

Source of Sample: S-39-26-1/2 Offset **Depth:** 0-5'

Project No.: 8623P180

Figure _____

Terracon Consultants, Inc.

750 Pilot Road, Suite F
Las Vegas, Nevada 89119
(702) 597-9393



Client

HNTB North Carolina PC

Project

S-39-26 BRO Tributary to South Saluda River

Sample Submitted By: Terracon (86)

Date Received: 8/16/2024

Lab No.: 24-0279

Results of Corrosion Analysis

Sample Number	S-39-26-1
Sample Location	--
Sample Depth (ft.)	0.5-15.0
pH Analysis, AASHTO T289	5.71
Water Soluble Sulfate (SO4), AASHTO T290 (mg/kg)	55
Chlorides, AASHTO T291, (mg/kg)	110
Saturated Minimum Resistivity, AASHTO T288, (ohm-cm)	2376

A handwritten signature in black ink, appearing to read "N. Campo".

Analyzed By _____

Nathan Campo
Laboratory Coordinator

The tests were performed in general accordance with applicable ASTM and AWWA test methods. This report is exclusively for the use of the client indicated above and shall not be reproduced except in full without the written consent of our company. Test results transmitted herein are only applicable to the actual samples tested at the location(s) referenced and are not necessarily indicative of the properties of other apparently similar or identical materials.



Rock Coring Summary

PROJECT ID P043138

PROJECT NAME S-39-26 BRO Tributary to South Saluda River

PROJECT COUNTY Pickens

Borehole	Core Run Number	Core Run Top Depth	REC (%)	RQD (%)	q _u (psi)	Poisson's Ratio	Secant Modulus (ksi)	Unit Weight (pcf)	RMR	GSI
S-39-26-1	NQ-1	59.5	93	93	11196	0.065	1167	163	77	85
S-39-26-1	NQ-2	64.5	100	100	13981	0.044	1394	166	77	90
S-39-26-2	NQ-1	60.5	98	98	9205	0.001	1095	167	77	90
S-39-26-2	NQ-2	65.5	100	91	15600	0.001	1366	165	82	90

Client

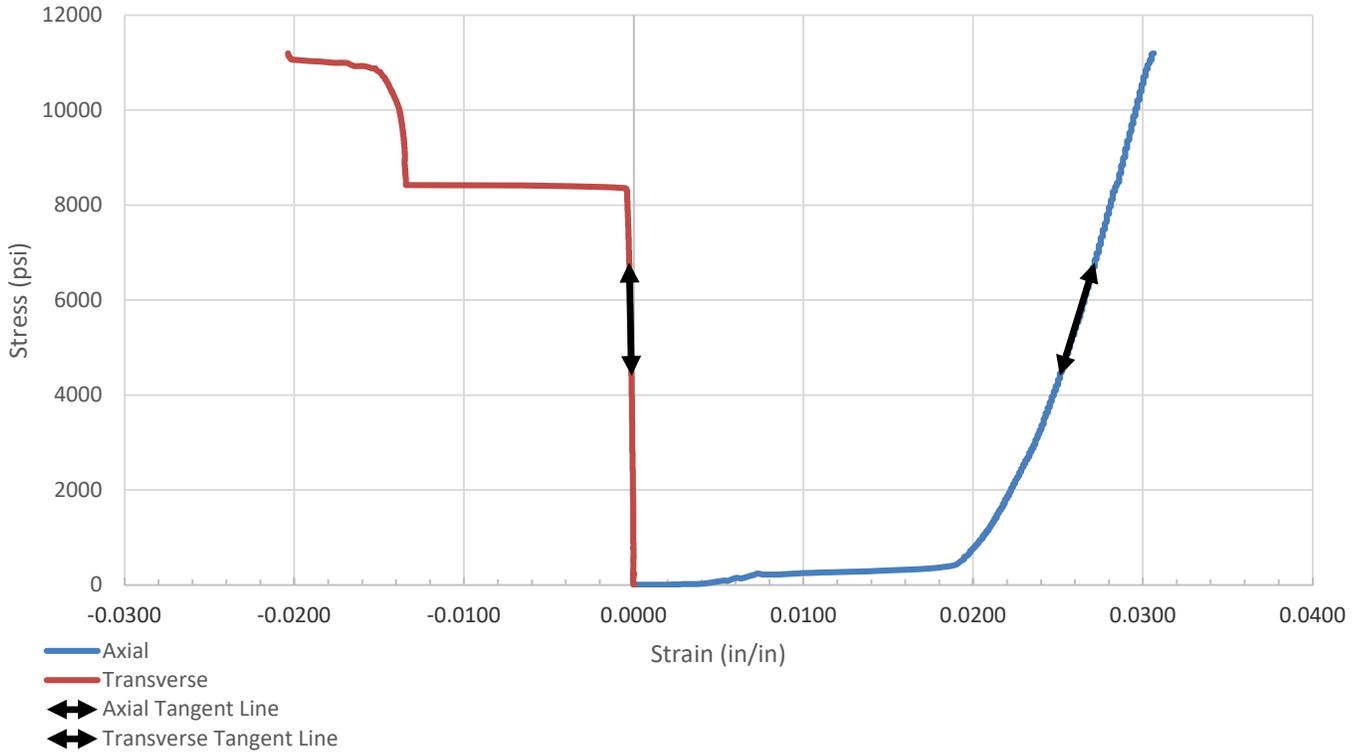
HNTB North Carolina PC
 Attn: Spencer Franklin
 343 E Six Forks Rd Ste 200
 Raleigh, NC 27609

Project

S-39-26 BRO Tributary to South Saluda River

Project No. 8623P180

ASTM D7012 Stress/ Strain Curve



SAMPLE LOCATION

Site:	SCDOT Bridge Package 19		
Description:	Gneiss		
Boring:	S-39-26-1	Depth (feet):	61.6-62.8

SPECIMEN INFORMATION

Sample No.:	NQ 1	Mass (g):	539.68
Length (in.):	4.17	Diameter (in.):	1.96
L/D Ratio:	2.13	Density (pcf):	163.41

TEST RESULTS

Failure Load (lbs):	33782
Failure Strain (%):	3.06
Unconfined Compressive Strength (psi):	11,196
Elastic Modulus, E, (ksi):	1167
Poisson's Ratio, u:	0.065
Time of Failure (min):	01:45
Rate of Loading (psi/sec):	0.042
Moisture Content Post-break:	0.0014

Client

HNTB North Carolina PC
Attn: Spencer Franklin
343 E Six Forks Rd Ste 200
Raleigh, NC 27609

Project

SCDOT Bridge Package 19

Project No. 8623P180

Equipment:

	Calipers	TICCS ID: W-54522
	Scale	B-71466
	Dial Indicator	C-70608
	Compression (spherically seated)	C-48999

Samples were prepared and tested in accordance with ASTM D4543 and D7012. Deviations, if any, are noted below:

Notes:

- Per ASTM D4543, this specimen has not met the requirements for perpendicularity, by exceeding 0.250°.
 - Per ASTM D4543, this specimen has not met the requirements for flatness, by exceeding 0.001 inches.
 - Per ASTM D4543, this specimen has not met the requirements for parallelism, by exceeding 0.25°.
- According to ASTM D7012 Section 8.2.1, this specimen, although not meeting all requirements of ASTM D4543 is acceptable for testing. However, the results reported may differ from results obtained from a test specimen that meets the requirements of D4543.

Client

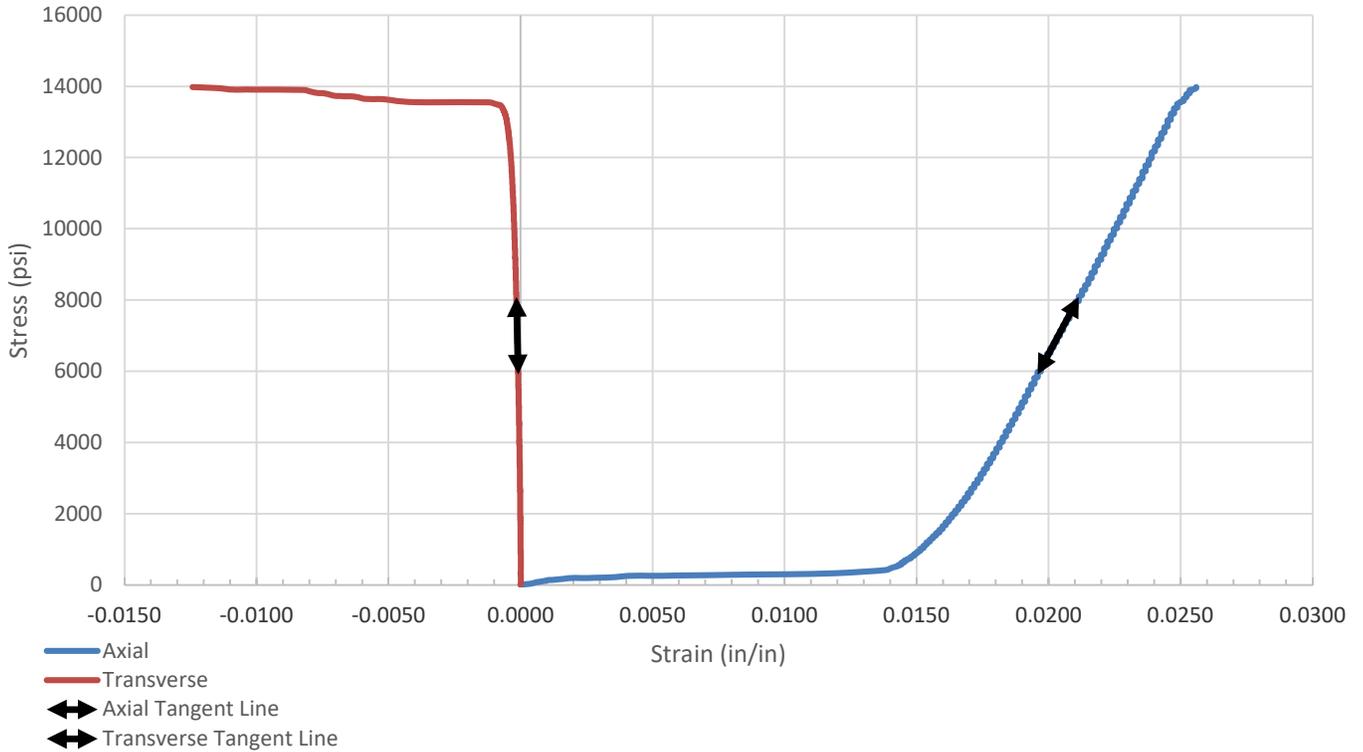
HNTB North Carolina PC
 Attn: Spencer Franklin
 343 E Six Forks Rd Ste 200
 Raleigh, NC 27609

Project

S-39-26 BRO Tributary to South Saluda River

Project No. 8623P180

ASTM D7012 Stress/ Strain Curve



SAMPLE LOCATION

Site:	SCDOT Bridge Package 19		
Description:	Gneiss		
Boring:	S-39-26-1	Depth (feet):	68.2-69.5

SPECIMEN INFORMATION

Sample No.:	NQ 2	Mass (g):	548.01
Length (in.):	4.17	Diameter (in.):	1.96
L/D Ratio:	2.13	Density (pcf):	165.93

TEST RESULTS

Failure Load (lbs):	42184
Failure Strain (%):	2.94
Unconfined Compressive Strength (psi):	13,981
Elastic Modulus, E, (ksi):	1394
Poisson's Ratio, u:	0.044
Time of Failure (min):	02:08
Rate of Loading (psi/sec):	0.042
Moisture Content Post-break:	0.0012

Client

HNTB North Carolina PC
Attn: Spencer Franklin
343 E Six Forks Rd Ste 200
Raleigh, NC 27609

Project

SCDOT Bridge Package 19

Project No. 8623P180

Equipment:

	Calipers	TICCS ID:	W-54522
	Scale		B-71466
	Dial Indicator		C-70608
	Compression (spherically seated)		C-48999

Samples were prepared and tested in accordance with ASTM D4543 and D7012. Deviations, if any, are noted below:

Notes:

- Per ASTM D4543, this specimen has not met the requirements for perpendicularity, by exceeding 0.250°.
 - Per ASTM D4543, this specimen has not met the requirements for flatness, by exceeding 0.001 inches.
 - Per ASTM D4543, this specimen has not met the requirements for parallelism, by exceeding 0.25°.
- According to ASTM D7012 Section 8.2.1, this specimen, although not meeting all requirements of ASTM D4543 is acceptable for testing. However, the results reported may differ from results obtained from a test specimen that meets the requirements of D4543.

Client

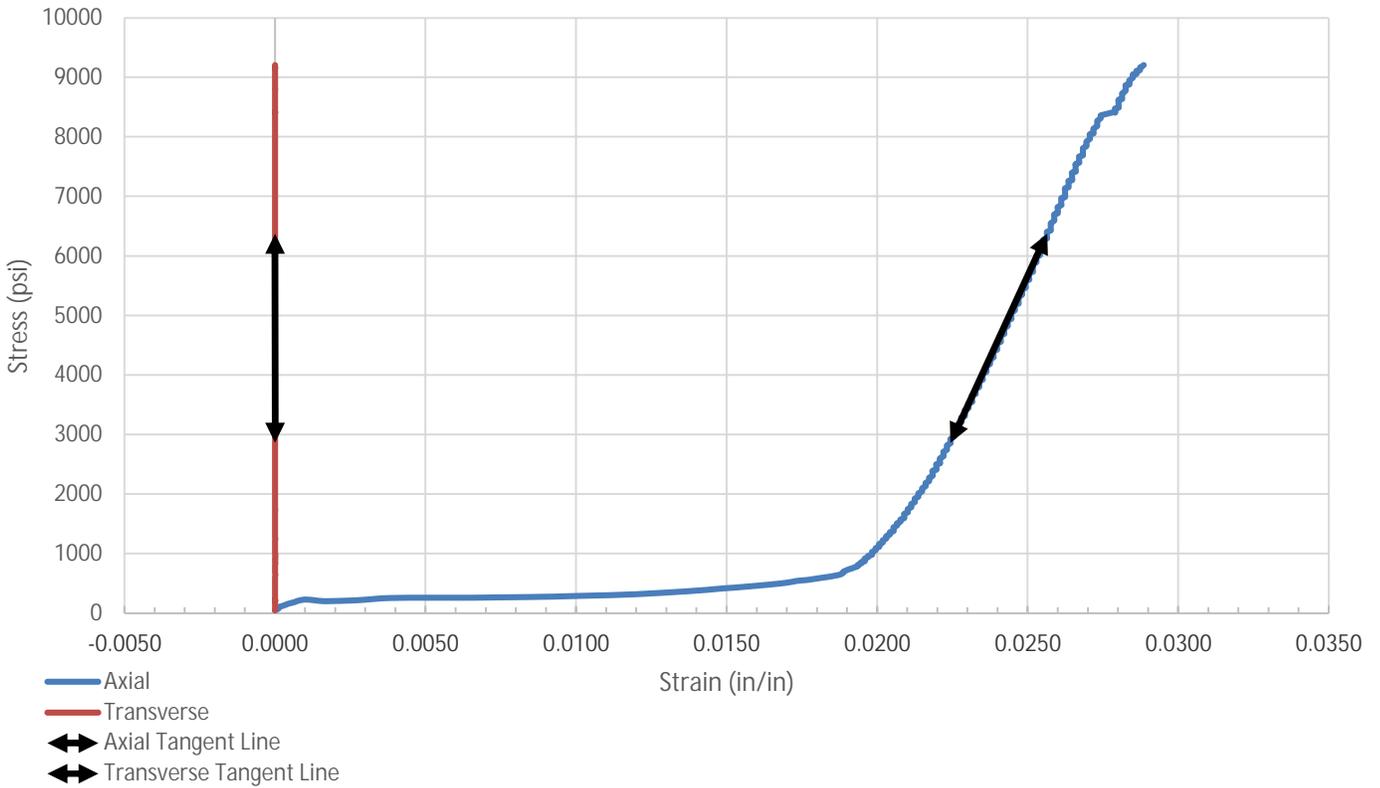
HNTB North Carolina PC
 Attn: Spencer Franklin
 343 E Six Forks Rd Ste 200
 Raleigh, NC 27609

Project

S-39-26 BRO Tributary to South Saluda River

Project No. 8623P180

ASTM D7012 Stress/ Strain Curve



SAMPLE LOCATION

Site:	SCDOT Bridge Package 19		
Rock Type:	Granite		
Boring:	S-39-26-2	Depth (feet):	60.5-61.5

SPECIMEN INFORMATION

Sample No.:	NQ1	Mass (g):	575.14
Length (in.):	4.22	Diameter (in.):	1.99
L/D Ratio:	2.1	Density (pcf):	166.93

TEST RESULTS

Failure Load (lbs):	28630
Failure Strain (%):	3.26
Unconfined Compressive Strength (psi):	9,205
Elastic Modulus, E, (ksi):	1095
Poisson's Ratio, u:	0.001
Time of Failure (min):	01:24
Rate of Loading (psi/sec):	109.845
Moisture Content Post-break:	0.01%



Client

HNTB North Carolina PC
Attn: Spencer Franklin
343 E Six Forks Rd Ste 200
Raleigh, NC 27609

Project

SCDOT Bridge Package 19

Project No. 8623P180

Equipment:

	TICCS ID:
Calipers:	W-54522
Scale:	B-71466
Dial Indicator:	C-70608
Compression (spherically seated):	C-48999

Samples were prepared and tested in accordance with ASTM D4543 and D7012. Deviations, if any, are noted below:
Notes:

Per ASTM D4543, this specimen has not met the requirements for perpendicularity, by exceeding 0.250°.

Per ASTM D4543, this specimen has not met the requirements for flatness, by exceeding 0.001 inches.

Per ASTM D4543, this specimen has not met the requirements for parallelism, by exceeding 0.25°.

According to ASTM D7012 Section 8.2.1, this specimen, although not meeting all requirements of ASTM D4543 is acceptable for testing. However, the results reported may differ from results obtained from a test specimen that meets the requirements of D4543.

Client

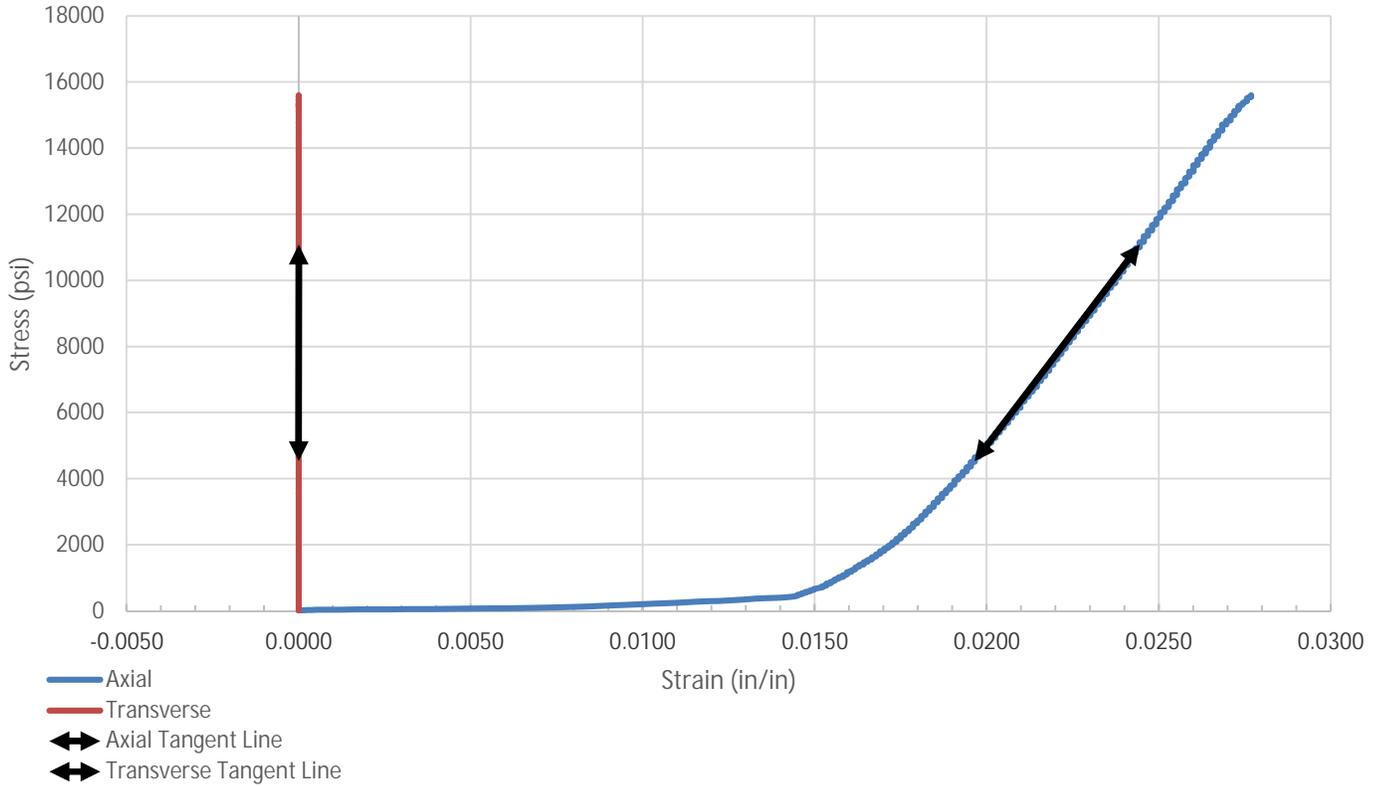
HNTB North Carolina PC
 Attn: Spencer Franklin
 343 E Six Forks Rd Ste 200
 Raleigh, NC 27609

Project

S-39-26 BRO Tributary to South Saluda River

Project No. 8623P180

ASTM D7012 Stress/ Strain Curve



SAMPLE LOCATION

Site:	SCDOT Bridge Package 19		
Rock Type:	Granite		
Boring:	S-39-26-2	Depth (feet):	66-66.8

SPECIMEN INFORMATION

Sample No.:	NQ2	Mass (g):	561.51
Length (in.):	4.18	Diameter (in.):	1.99
L/D Ratio:	2.1	Density (pcf):	164.54

TEST RESULTS

Failure Load (lbs):	48519
Failure Strain (%):	3.43
Unconfined Compressive Strength (psi):	15,600
Elastic Modulus, E, (ksi):	1366
Poisson's Ratio, u:	0.001
Time of Failure (min):	02:23
Rate of Loading (psi/sec):	109.089
Moisture Content Post-break:	0.01%



Client

HNTB North Carolina PC
Attn: Spencer Franklin
343 E Six Forks Rd Ste 200
Raleigh, NC 27609

Project

SCDOT Bridge Package 19

Project No. 8623P180

Equipment:

	TICCS ID:
Calipers:	W-54522
Scale:	B-71466
Dial Indicator:	C-70608
Compression (spherically seated):	C-48999

Samples were prepared and tested in accordance with ASTM D4543 and D7012. Deviations, if any, are noted below:
Notes:

Per ASTM D4543, this specimen has not met the requirements for perpendicularity, by exceeding 0.250°.

Per ASTM D4543, this specimen has not met the requirements for flatness, by exceeding 0.001 inches.

Per ASTM D4543, this specimen has not met the requirements for parallelism, by exceeding 0.25°.

According to ASTM D7012 Section 8.2.1, this specimen, although not meeting all requirements of ASTM D4543 is acceptable for testing. However, the results reported may differ from results obtained from a test specimen that meets the requirements of D4543.

Appendix C – Supporting Documents

S-39-26 BRO Tributary to South Saluda River | Pickens County, SC
Terracon Project No. 8623P180 | SCDOT Project ID: P043138



Appendix C

Supporting Documents

Rig Calibration Report – DR#1327 (8 Pages)

Note: All exhibits are one page unless noted above.

SPT Automatic Hammer Energy Measurement Report

Drill Rig Model: Geoprobe 3126GT
 Drill Rig Serial Number: 3126S5V224106
 Asset Number: DR#1327

September 13, 2024

September 13, 2024

Terracon Consultants Inc.
 72 Pointe Circle
 Greenville, SC 29615

Attn: Nitin Dudani
 E: nitin.dudani@terracon.com

Re: SPT Automatic Hammer Energy Measurement Report
 Rig No: 1327
 Terracon Project Number: 73245115

Dear Mr. Dudani:

This report provides the Energy Transfer Ratio (ETR) for the Standard Penetration Testing (SPT) automatic hammer as summarized below:

Table 1: Hammer Efficiency Summary

Drill Rig Make/Model	Drill Rig Serial Number	Drill Rig Year	Asset Number	Energy Transfer Ratio (ETR)	Hammer Efficiency Correction (C _e)
Geoprobe	3126S5V224106	2024	DR#1327	92.6% ± 1.75%	1.54

*Please Note: according to ASTM standard, a minimum of three recordings should be collected at five-foot intervals no shallower than twenty feet below current ground surface (bgs). The sample intervals were obtained between 30 and 50 feet bgs.

If you have any questions concerning this summary, or if we may be of further service, please contact us.

Ryan C. Wakeford, P.E.
 Geotechnical Engineer

Susheel R. Kolwalkar, Ph.D., P.E.
 Regional Services Manager

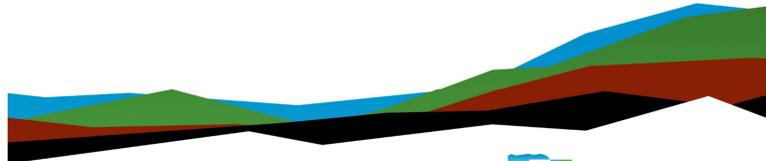


Micah Hatch, P.E.
 Geotechnical Department Manager



Attachments:

- Exhibit A: SPT Representative Blow
- Exhibit B: SPT Analyzer Literature and Equipment Calibrations
- Exhibit C: SPT Analyzer Results
- Exhibit D: Field Log
- Exhibit E: Copy of Certificate of Proficiency



Prepared for:
 Terracon Consultants, Inc.
 Greenville, South Carolina



1.0 MEASUREMENT SUMMARY

ITEM	DESCRIPTION
Drill Rig Owner	Terracon Consultant, Inc. – Greenville, SC
Drill Rig Operator	Brett Burnett: Terracon Exploration
Testing Date	9/5/2024
Testing Location	Sumter County, SC
Boring Identification	B-3
Energy Measurement Depths	30 ft, 40 ft, 45 ft, 50 ft
Subsurface Soils	Poorly graded sands (SP) to clayey sands (SC)
Hammer Type/Height	140 pounds (automatic) with 2.5-foot drop height
Boring Method	Mud rotary
Drill Rods	<ul style="list-style-type: none"> AWJ 1-3/4" outside diameter 1-1/4" inside diameter 1.15 in² cross sectional area 1/4" wall thickness
Calibration Testing Equipment	<ul style="list-style-type: none"> 2-foot AWJ rod instrumented w/ two strain gauges and two accelerometers manufactured by Pile Dynamics Inc. (PDI) SN: 746AWJ Model SPT Analyzer™ (PDA) SN: 4621 TB
ASTM Methods Used	ASTM D1586, Standard Test Method for Standard Penetration Test and Split-Barrel Sampling of Soils ASTM D4633-16, Standard Method for Energy Measurement for Dynamic Penetrometers
SPT Calibration Personnel	Ryan Wakeford – Intermediate PDA Proficiency, Terracon Consultants, Inc.

2.0 PURPOSE AND SCOPE OF WORK

The North Charleston office of Terracon Consultants, Inc. conducted SPT energy measurements in accordance with ASTM D4633-16 at a site off Panola Road in Sumter County, South Carolina. Energy measurements on the rig were taken during eight samples events.

3.0 TEST RESULTS

Table 2: SPT Hammer Energy Calibration Testing Summary

Boring	Start Depth ¹ (ft)	Rod Length ² (ft)	Rod Sections ³				Measured Blow Counts (blows/6 inches)				SPT N _{meas} (bpf)	Soil Type ⁴
			2 ft	5 ft	10 ft	1 st 1 inc.	2 nd 1 inc.	3 rd 1 inc.	4 th 1 inc.			
B-3	28.5	33.7	0	6	0	4	5	6	-	11	SP	
	38.5	43.7	0	8	0	7	10	10	-	20	SP	
	43.5	48.7	0	9	0	4	5	7	-	12	SP	
	48.5	53.7	0	10	0	4	4	7	-	11	SP	

- Depth from existing ground surface to start of SPT
- Total rod length from instrumentation to bottom of sampler
- Two-foot section is instrumented and is located at top of drill rods
- Soil type visually classified by Terracon

Table 3: Energy Measurement and Analysis Summary

Boring	Start Depth ¹ (ft)	SPT N _m (bpf)	No. of Blows ²	EMX ³ (ft-lbs)			ETR ³ (%)		
				Max.	Min.	Ave.	Std. Dev.	Ave.	Std. Dev.
B-3	28.5	11	11	340	313	327	8.8	93.4	2.5
	38.5	20	20	334	309	318	5.6	90.9	1.6
	43.5	12	12	330	309	323	5.5	92.4	1.6
	48.5	11	11	334	320	328	4.5	93.7	1.3
Average:				335	313	334	6.1	92.6	1.75

- Boring ID and depth from existing ground surface to start of SPT
- Number of blows used in energy calibration analysis; limited to measurements recorded during the second and third 6-inch sampling intervals at each depth or during the first increment if refusal were encountered
- EMX = Maximum Transferred Energy, ETR = Energy Transfer Ratio.

Table 4: Hammer Blow Rate Summary

Boring	Start Depth ¹ (ft)	SPT N _{meas} (bpf)	No. of Blows ²	BPM ³			
				Max.	Min.	Ave.	Std. Dev.
B-3	28.5	11	11	53.8	53.1	53.5	0.2
	38.5	20	20	53.7	53.0	53.4	0.1
	43.5	12	12	53.6	53.2	53.4	0.1
	48.5	11	11	53.8	53.1	53.4	0.2
Average:				53.7	53.1	53.4	0.2

- Boring ID and depth from existing ground surface to start of SPT.
- Number of blows used in energy calibration analysis. Limited to measurements recorded during the second and third 6-inch sampling intervals at each depth or during the 1st increment if refusal conditions were encountered.
- BPM = Blows per minute

Exhibit A

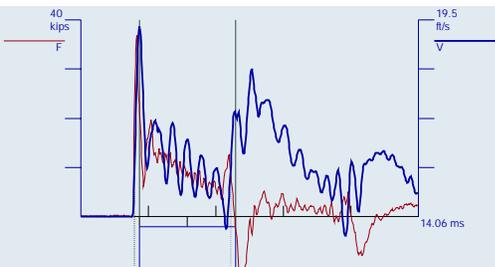
SPT Representative Blow

GRL Engineers, Inc.
 GEOPROBE 3126GT
 28.5-30
 B3
 PDA Operator: RW

Pile Driving Analyzer ® (PDA)
 Version: 2022.35.2

GRL Engineers, Inc.
 GEOPROBE 3126GT
 38.5-40
 B3
 PDA Operator: RW

Pile Driving Analyzer ® (PDA)
 Version: 2022.35.2

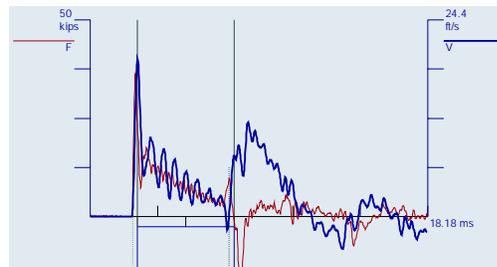


BN 13
 05Sep2024 10:07:23 AM

CSX	32.1 ksi
DMX	1.11 in
EFV	331 ft-lb
ETR	94.7 %
BPM	53.8 bpm
RAT	1.0
VMX	18.9 ft/s
FMX	37 kips
DFN	1.00 in
MEX	1070 µE
AMX	3001 g/s
FVP	0.6

LE	33.70 ft
AR	1.15 in ²
EM	30000 ksi
SP	0.492 k-ft/3
WS	16807.9 ft/s
WC	16766.2 ft/s
JC	0.90
JF	1.00

F1: [746AWJ1]	222.05 PDICAL (1) FF1
F2: [746AWJ2]	222.19 PDICAL (1) FF1
A3 (PR): [K14007]	407.233 mv/6.4v/5000g (1) VF1
A4 (PR): [K14006]	375.226 mv/6.4v/5000g (1) VF1

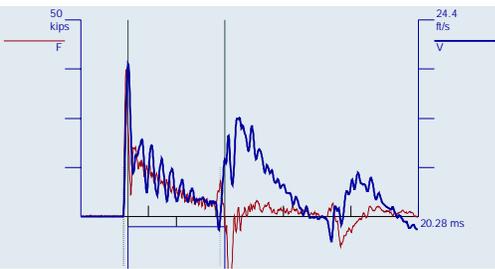


BN 25
 05Sep2024 10:24:35 AM

CSX	31.7 ksi
DMX	0.66 in
EFV	324 ft-lb
ETR	92.6 %
BPM	53.4 bpm
RAT	1.1
VMX	19.6 ft/s
FMX	36 kips
DFN	0.60 in
MEX	1056 µE
AMX	3358 g/s

LE	43.70 ft
AR	1.15 in ²
EM	30000 ksi
SP	0.492 k-ft/3
WS	16807.9 ft/s
WC	16807.7 ft/s
JC	0.90
JF	1.00

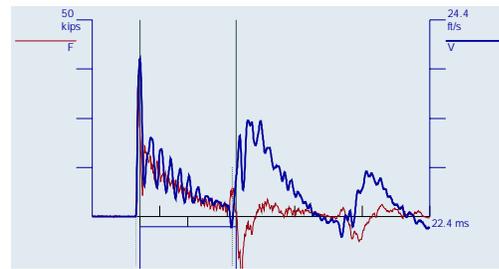
F1: [746AWJ1]	222.05 PDICAL (1) FF1
F2: [746AWJ2]	222.19 PDICAL (1) FF1
A3 (PR): [K14007]	407.233 mv/6.4v/5000g (1) VF1
A4 (PR): [K14006]	375.226 mv/6.4v/5000g (1) VF1



BN 14
05Sep2024 10:32:57 AM

CSX	32.6 ksi
DMX	0.91 in
EFV	325 ft-lb
ETR	92.8 %
BPM	53.4 bpm
RAT	1.0
VMX	19.0 ft/s
FMX	37 kips
DFN	0.86 in
MEX	1086 µE
AMX	3426 g's
LE	48.70 ft
AR	1.15 m ²
EM	30000 ksi
SP	0.492 k-ft ³
WS	16807.9 ft/s
WC	16793.1 ft/s
JC	0.90
JF	1.00

F1: [746AWJ1] 222.05 PDICAL (1) FF1
 F2: [746AWJ2] 222.19 PDICAL (1) FF1
 A3 (PR): [K14007] 407.233 mv/6.4v/5000g (1) VF1
 A4 (PR): [K14006] 375.226 mv/6.4v/5000g (1) VF1



BN 13
05Sep2024 10:42:13 AM

CSX	31.5 ksi
DMX	1.01 in
EFV	320 ft-lb
ETR	91.4 %
BPM	53.7 bpm
RAT	1.1
VMX	19.6 ft/s
FMX	36 kips
DFN	0.86 in
MEX	1049 µE
AMX	4077 g's
LE	53.70 ft
AR	1.15 m ²
EM	30000 ksi
SP	0.492 k-ft ³
WS	16807.9 ft/s
WC	16781.3 ft/s
JC	0.90
JF	1.00

F1: [746AWJ1] 222.05 PDICAL (1) FF1
 F2: [746AWJ2] 222.19 PDICAL (1) FF1
 A3 (PR): [K14007] 407.233 mv/6.4v/5000g (1) VF1
 A4 (PR): [K14006] 375.226 mv/6.4v/5000g (1) VF1

Exhibit B

SPT Analyzer Literature and Equipment Calibrations



SPT Analyzer

SPT Analyzer

Measures the energy transferred into an instrumented SPT rod during a Standard Penetration Test (SPT)

Reliable. Simplified. Rugged.

The SPT Analyzer determines the energy transferred by SPT hammers using force and velocity measurements, for improved reliability of SPT N-values.

What is SPT?

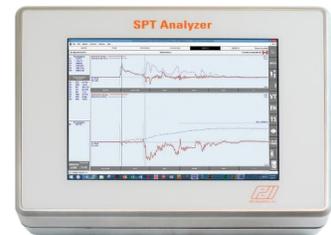
The Standard Penetration Test (SPT) is a widely-employed soil exploration tool that involves using an SPT hammer to drive a split sampler at the bottom of a drill string to obtain soil samples. The number of blows required to penetrate the last 300mm (1ft) is the "N value" which is related to soil strength.

Why measure the energy transferred by the SPT hammer?

Several different types of SPT hammers are used to conduct Standard Penetration Tests. Their varying efficiencies influence the N value. The measured N value is normalized by multiplying it by the ratio of the measured energy transferred to the rod to 60% of the theoretical potential energy. The normalization compensates for the variability of the efficiencies of different SPT hammer types, and improves the reliability of soil strength estimates used in geotechnical applications.

The SPT Analyzer is furnished with a 0.6m sub assembly (or section) of an SPT rod (AW, NW or other type) instrumented with two strain gage bridges, and calibrated by Pile Dynamics. Once in the field, two accelerometers are bolted to the rod section. The instrumented section is inserted at the top of the drill string between the hammer and the existing sampling rod. The sensors on the rod are connected to the SPT Analyzer.

Smart Sensor technology allows the SPT Analyzer to read the rod instrumentation, obtaining the sensor calibration and rod cross sectional area.



- Calculates energy transferred by SPT hammers using force and velocity measurements
- Determines N value to help improve reliability of soil strength estimates
- Offers simplified reporting and analysis option to speed testing results
- Operates in English, SI, or Metric units



EN ISO 22486-3:2005/ASTM Compliant

The SPT Analyzer is compliant with EN ISO 22476-3:2005. ASTM D1586 recommends normalizing results from any SPT test using energy measurements. When these tests are performed to determine the liquefaction potential of sands, ASTM D6066 not only recommends but mandates the normalization. ASTM D4633 states that the only acceptable method of determining energy for normalization of N values is by force and velocity measurements.

These quantities are input to the SPT Analyzer automatically. This significantly simplifies the initial test setup.

The strain gages and accelerometers obtain the force and velocity signals necessary for the calculation of transferred energy to the drill string for each hammer blow. The energy is displayed in real time on the SPT Analyzer screen.

Output

SPT Analyzer data is stored and transferred to a computer via USB memory stick. The software furnished with the SPT Analyzer has a Report Creation Option that makes it quick and easy to summarize results and create output graphs of Force, Velocity, Energy and Displacement versus Time, as well as numerical, statistical, and graphical results for each data set. The software is fully customizable.



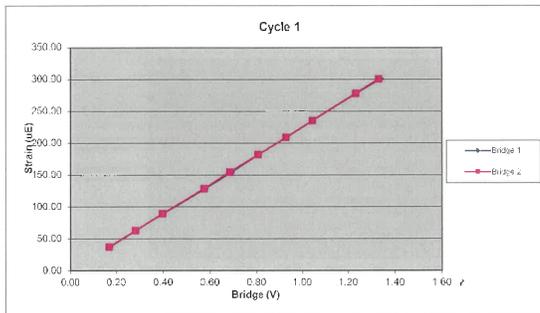
Pile Dynamics, Inc. (PDI) is the world leader in developing, manufacturing and supplying state of the art QA/QC products and systems for the deep foundations industry. The company is headquartered in Cleveland, Ohio, USA, with offices and representatives worldwide. For additional information visit us at www.pile.com or contact info@pile.com.

www.pile.com | +1 (216) 831-6131 | info@pile.com

746AWJ		Cycle 1		
Sample	Force (lb)	Strain (µE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	1296.93	37.22	0.17	0.17
3	2135.32	62.74	0.28	0.28
4	3028.79	89.39	0.40	0.40
5	4377.09	128.61	0.58	0.57
6	5243.07	154.57	0.69	0.68
7	6143.17	181.90	0.81	0.81
8	7067.95	208.93	0.93	0.93
9	7958.18	238.42	1.04	1.05
10	9380.66	278.02	1.23	1.23
11	10161.74	300.76	1.34	1.33

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7605.07	Force Calibration (lb/V)	7606.74
Offset	-0.16	Offset	12.66
Correlation	0.999997	Correlation	0.999999
Strain Calibration (µE/V)	225.99	Strain Calibration (µE/V)	226.04
Offset	-1.01	Offset	-8.33
Correlation	0.999989	Correlation	0.999992

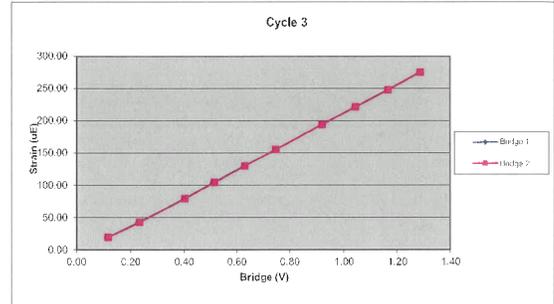
Force Strain Calibration	
EA (Kips)	33651.50
Offset	33.98
Correlation	0.999994



746AWJ		Cycle 3		
Sample	Force (lb)	Strain (µE)	Bridge 1 (V)	Bridge 2 (V)
1	0.00	0.00	0.00	0.00
2	838.16	19.27	0.11	0.12
3	1786.75	42.28	0.23	0.23
4	3083.67	79.12	0.40	0.40
5	3943.80	104.13	0.51	0.51
6	4839.52	129.87	0.63	0.63
7	5750.14	155.24	0.75	0.75
8	7079.92	194.22	0.92	0.92
9	8007.70	221.43	1.04	1.05
10	8943.28	247.95	1.17	1.17
11	9871.55	275.44	1.29	1.29

Bridge 1		Bridge 2	
Force Calibration (lb/V)	7659.96	Force Calibration (lb/V)	7667.39
Offset	13.76	Offset	-1.59
Correlation	0.999999	Correlation	0.999998
Strain Calibration (µE/V)	219.43	Strain Calibration (µE/V)	219.64
Offset	-7.95	Offset	-8.39
Correlation	0.999934	Correlation	0.999939

Force Strain Calibration	
EA (Kips)	34904.41
Offset	291.93
Correlation	0.999935



Accelerometer Calibration Certificate
Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on **MAY 16 2024**

Serial No: K14006 Temperature: 24.0 °C
Model: PR Humidity: 42%
Calibrated on: Channel 3 on 8G 5161 LE

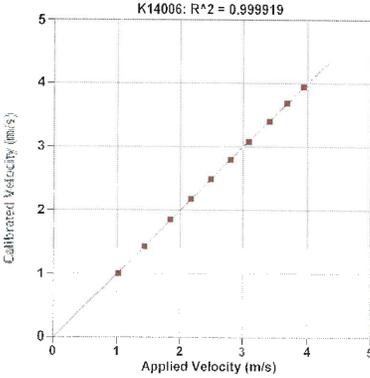
PDA CALIBRATION FACTOR
375.2 mv/5000g
(75.0 μv/g)
R²: 0.999919 [Chip programmed]

Operator: William Johnson

Signed

Ref Acc 1: 78268! Cal on: 11Jan2024
986 g/s/volt
Ref Acc 2: 78270! Cal on: 11Jan2024
971 g/s/volt

Reference accelerometer calibrations are traceable to the United States National Institute of Standards and Technology (NIST).



Version: 2023-09-17 4: 17

Accelerometer Calibration Certificate
Pile Dynamics, Inc.



Calibrated by Pile Dynamics, Inc.
Calibration performed on **MAY 16 2024**

Serial No: K14007 Temperature: 23.8 °C
Model: PR Humidity: 42%
Calibrated on: Channel 4 on 8G 5161 LE

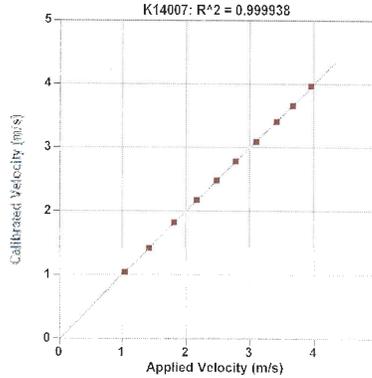
PDA CALIBRATION FACTOR
407.2 mv/5000g
(81.4 μv/g)
R²: 0.999938 [Chip programmed]

Operator: William Johnson

Signed

Ref Acc 1: 78268! Cal on: 11Jan2024
986 g/s/volt
Ref Acc 2: 78270! Cal on: 11Jan2024
971 g/s/volt

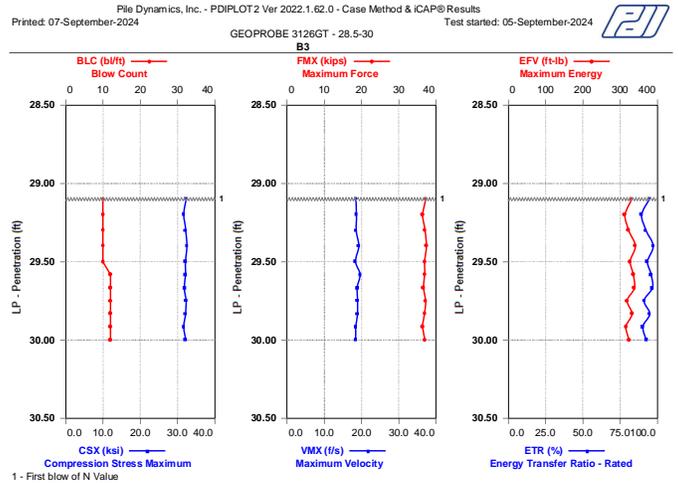
Reference accelerometer calibrations are traceable to the United States National Institute of Standards and Technology (NIST).



Version: 2023-09-17 4: 24



Exhibit C
SPT Analyzer Results





GEOPROBE 3126GT - 28.5-30

Case Method & iCAP® Results

Date: 05-September-2024

OP: RW
AR: 1.15 in² SP: 0.492 klf²
LE: 33.70 ft EM: 30,000 ksi
WS: 16,807.9 f/s JC: 0.00

FMX: Maximum Force
VMX: Maximum Velocity
EMX: Maximum Energy
EFV: Maximum Energy
ETR: Energy Transfer Ratio - Rated

BPM: Blows/Minute
DMX: Maximum Displacement
DFN: Final Displacement
CSX: Compression Stress Maximum

BL#	Depth ft	BLC b/ft	FMX kips	VMX f/s	EMX ft-lb	EFV ft-lb	ETR (%)	BPM bpm	DMX in	DFN in	CSX ksi
5	29.10	10	37	18.4	331.0	331.0	94.6	53.1	1.58	1.20	32.3
6	29.20	10	36	18.7	312.7	312.7	89.3	53.4	1.47	1.20	31.7
7	29.30	10	37	18.5	323.0	323.0	92.3	53.6	1.54	1.20	32.2
8	29.40	10	37	19.2	340.4	340.4	97.3	53.4	1.57	1.20	32.5
9	29.50	10	37	18.4	326.6	326.6	93.3	53.5	1.48	1.20	32.1
10	29.58	12	37	19.6	335.5	335.5	95.9	53.3	1.41	1.00	32.1
11	29.67	12	37	18.8	338.0	338.0	96.6	53.7	1.58	1.00	31.8
12	29.75	12	37	18.9	318.3	318.3	90.9	53.5	1.37	1.00	32.3
13	29.83	12	37	18.9	331.4	331.4	94.7	53.8	1.11	1.00	32.1
14	29.92	12	36	18.5	315.2	315.2	90.1	53.8	1.09	1.00	31.7
15	30.00	12	37	18.4	324.1	324.1	92.6	53.6	1.07	1.00	32.1
Average			37	18.8	326.9	326.9	93.4	53.5	1.39	1.09	32.1
Std. Dev.			0	0.4	8.8	8.8	2.5	0.2	0.19	0.10	0.3
Maximum			37	19.6	340.4	340.4	97.3	53.8	1.58	1.20	32.5
Minimum			36	18.4	312.7	312.7	89.3	53.1	1.07	1.00	31.7

Total number of blows analyzed: 11

BL# Sensors

5-15 F1: [746AWJ1] 222.1 (1.00); F2: [746AWJ2] 222.2 (1.00); A3: [K14007] 407.2 (1.00); A4: [K14006] 375.2 (1.00)

BL# Comments

5 First blow of N Value

Time Summary

Drive 15 seconds 10:07 AM - 10:07 AM BN 1 - 15



GEOPROBE 3126GT - 38.5-40

Case Method & iCAP® Results

Date: 05-September-2024

OP: RW
AR: 1.15 in² SP: 0.492 klf²
LE: 43.70 ft EM: 30,000 ksi
WS: 16,807.9 f/s JC: 0.00

FMX: Maximum Force
VMX: Maximum Velocity
EMX: Maximum Energy
EFV: Maximum Energy
ETR: Energy Transfer Ratio - Rated

BPM: Blows/Minute
DMX: Maximum Displacement
DFN: Final Displacement
CSX: Compression Stress Maximum

BL#	Depth ft	BLC b/ft	FMX kips	VMX f/s	EMX ft-lb	EFV ft-lb	ETR (%)	BPM bpm	DMX in	DFN in	CSX ksi
7	39.05	20	36	18.7	320.4	320.4	91.5	53.3	0.91	0.60	31.6
8	39.10	20	36	18.5	313.6	313.6	89.6	53.2	0.65	0.60	31.6
9	39.15	20	37	18.9	318.4	318.4	91.0	53.4	0.66	0.60	32.1
10	39.20	20	37	18.9	309.8	309.8	88.5	53.5	0.64	0.60	31.9
11	39.25	20	37	19.1	321.4	321.4	91.8	53.2	0.93	0.60	31.9
12	39.30	20	36	18.5	309.3	309.3	88.4	53.5	0.64	0.60	31.5
13	39.35	20	37	19.5	320.6	320.6	91.6	53.0	0.69	0.60	31.9
14	39.40	20	36	18.4	314.3	314.3	89.8	53.3	0.80	0.60	30.9
15	39.45	20	37	19.5	326.5	326.5	93.3	53.5	0.92	0.60	32.0
16	39.50	20	36	18.6	320.6	320.6	91.6	53.5	1.02	0.60	31.7
17	39.55	20	37	19.1	316.4	316.4	90.4	53.7	0.68	0.60	31.8
18	39.60	20	36	19.0	312.4	312.4	89.2	53.3	0.66	0.60	31.7
19	39.65	20	36	18.8	315.8	315.8	90.2	53.5	0.70	0.60	31.1
20	39.70	20	36	19.2	320.1	320.1	91.5	53.4	0.78	0.60	31.1
21	39.75	20	36	19.5	320.9	320.9	91.7	53.3	0.63	0.60	31.0
22	39.80	20	37	19.2	317.1	317.1	90.6	53.5	0.74	0.60	31.7
23	39.85	20	36	18.8	315.1	315.1	90.0	53.5	0.61	0.60	31.1
24	39.90	20	36	19.7	333.6	333.6	95.3	53.5	0.83	0.60	31.3
25	39.95	20	36	19.6	323.9	323.9	92.6	53.4	0.66	0.60	31.7
26	40.00	20	35	18.9	313.5	313.5	89.6	53.5	0.60	0.60	30.6
Average			36	19.0	318.2	318.2	90.9	53.4	0.74	0.60	31.5
Std. Dev.			0	0.4	5.6	5.6	1.6	0.1	0.12	0.00	0.4
Maximum			37	19.7	333.6	333.6	95.3	53.7	1.02	0.60	32.1
Minimum			35	18.4	309.3	309.3	88.4	53.0	0.60	0.60	30.6

Total number of blows analyzed: 20

BL# Sensors

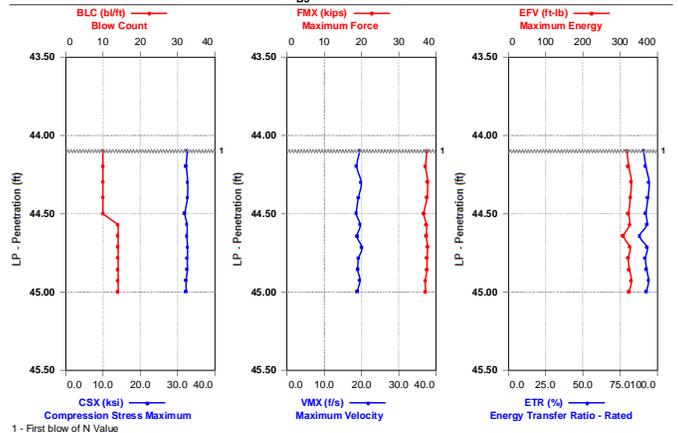
7-26 F1: [746AWJ1] 222.1 (1.00); F2: [746AWJ2] 222.2 (1.00); A3: [K14007] 407.2 (1.00); A4: [K14006] 375.2 (1.00)

BL# Comments

7 First blow of N Value

Time Summary

Drive 28 seconds 10:24 AM - 10:24 AM BN 1 - 26



1 - First blow of N Value



1 - First blow of N Value



GEOPROBE 3126GT - 43.5-45

Case Method & iCAP® Results

B3

OP: RW Date: 05-September-2024
AR: 1.15 in² SP: 0.492 klf/ft
LE: 48.70 ft EM: 30,000 ksi
WS: 16,807.9 f/s JC: 0.00

FMX: Maximum Force BPM: Blows/Minute
VMX: Maximum Velocity DMX: Maximum Displacement
EMX: Maximum Energy DFN: Final Displacement
EFV: Maximum Energy CSX: Compression Stress Maximum

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC b/ft	FMX kips	VMX f/s	EMX ft-lb	EFV ft-lb	ETR (%)	BPM bpm	DMX in	DFN in	CSX ksi
5	44.10	10	37	19.5	317.4	317.4	90.7	53.2	1.23	1.19	32.6
6	44.20	10	37	18.7	322.7	322.7	92.2	53.3	1.22	1.20	32.4
7	44.30	10	38	19.9	330.1	330.1	94.3	53.4	1.30	1.20	32.8
8	44.40	10	38	19.2	327.2	327.2	93.5	53.5	1.22	1.20	32.6
9	44.50	10	37	18.6	323.0	323.0	92.3	53.5	1.21	1.20	32.0
10	44.57	14	37	19.7	325.2	325.2	92.9	53.4	0.95	0.85	32.6
11	44.64	14	37	18.8	309.1	309.1	88.3	53.6	0.90	0.85	32.5
12	44.71	14	38	20.1	326.0	326.0	93.2	53.5	1.06	0.86	32.8
13	44.79	14	37	19.2	321.1	321.1	91.8	53.4	1.05	0.86	32.6
14	44.86	14	37	19.0	324.7	324.7	92.8	53.4	0.91	0.86	32.6
15	44.93	14	37	19.5	329.6	329.6	94.2	53.5	0.99	0.86	32.3
16	45.00	14	37	18.8	323.5	323.5	92.4	53.4	0.89	0.86	32.3
Average			37	19.3	323.3	323.3	92.4	53.4	1.08	1.00	32.5
Std. Dev.			0	0.5	5.5	5.5	1.6	0.1	0.15	0.17	0.2
Maximum			38	20.1	330.1	330.1	94.3	53.6	1.30	1.20	32.8
Minimum			37	18.6	309.1	309.1	88.3	53.2	0.89	0.85	32.0

Total number of blows analyzed: 12

BL# Sensors

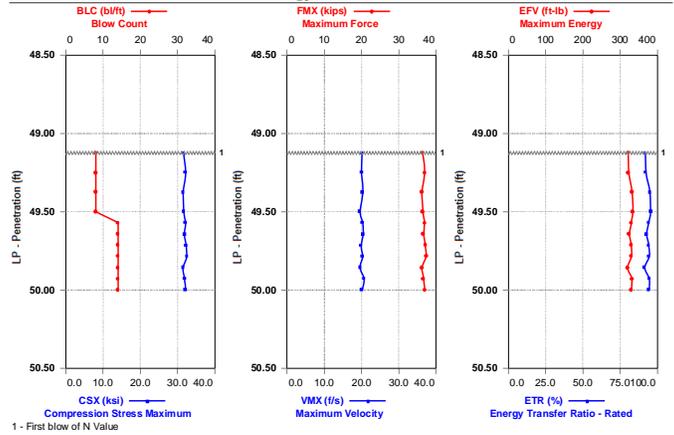
5-16 F1: [746AWJ1] 222.1 (1.00); F2: [746AWJ2] 222.2 (1.00); A3: [K14007] 407.2 (1.00);
A4: [K14006] 375.2 (1.00)

BL# Comments

5 First blow of N Value

Time Summary

Drive 16 seconds 10:32 AM - 10:33 AM BN 1 - 16



CSX (ksi) Compression Stress Maximum
VMX (f/s) Maximum Velocity
ETR (%) Energy Transfer Ratio - Rated
1 - First blow of N Value

GEOPROBE 3126GT - 48.5-50

Case Method & iCAP® Results

B3

OP: RW Date: 05-September-2024
AR: 1.15 in² SP: 0.492 klf/ft
LE: 53.70 ft EM: 30,000 ksi
WS: 16,807.9 f/s JC: 0.00

FMX: Maximum Force BPM: Blows/Minute
VMX: Maximum Velocity DMX: Maximum Displacement
EMX: Maximum Energy DFN: Final Displacement
EFV: Maximum Energy CSX: Compression Stress Maximum

ETR: Energy Transfer Ratio - Rated

BL#	Depth ft	BLC b/ft	FMX kips	VMX f/s	EMX ft-lb	EFV ft-lb	ETR (%)	BPM bpm	DMX in	DFN in	CSX ksi
5	49.13	8	36	20.1	321.6	321.6	91.9	53.3	1.81	1.50	31.6
6	49.25	8	37	20.1	323.0	323.0	92.3	53.4	1.81	1.50	32.1
7	49.38	8	36	20.3	332.2	332.2	94.9	53.5	1.50	1.50	31.5
8	49.50	8	36	19.6	334.0	334.0	95.4	53.3	1.50	1.50	31.7
9	49.57	14	37	20.3	329.3	329.3	94.1	53.8	0.87	0.86	32.1
10	49.64	14	37	20.4	324.8	324.8	92.8	53.4	1.00	0.86	31.9
11	49.71	14	37	19.9	329.7	329.7	94.2	53.2	0.89	0.86	32.2
12	49.79	14	37	20.2	330.1	330.1	94.3	53.7	0.89	0.86	32.4
13	49.86	14	36	19.6	319.8	319.8	91.4	53.7	1.01	0.86	31.5
14	49.93	14	37	20.7	331.0	331.0	94.6	53.1	0.91	0.86	31.9
15	50.00	14	37	20.1	330.2	330.2	94.4	53.2	1.03	0.86	32.1
Average			37	20.1	327.8	327.8	93.7	53.4	1.20	1.09	31.9
Std. Dev.			0	0.3	4.5	4.5	1.3	0.2	0.36	0.31	0.3
Maximum			37	20.7	334.0	334.0	95.4	53.8	1.81	1.50	32.4
Minimum			36	19.6	319.8	319.8	91.4	53.1	0.87	0.86	31.5

Total number of blows analyzed: 11

BL# Sensors

5-15 F1: [746AWJ1] 222.1 (1.00); F2: [746AWJ2] 222.2 (1.00); A3: [K14007] 407.2 (1.00);
A4: [K14006] 375.2 (1.00)

BL# Comments

5 First blow of N Value

Time Summary

Drive 15 seconds 10:42 AM - 10:42 AM BN 1 - 15



Exhibit D

Field Log



SPT HAMMER CALIBRATION FIELD WORKSHEET

PROJECT NAME: 7324515
PROJECT NO.: Terracon Assets Site
BORING NO.: 8-3
CLIENT:

ARRIVAL TIME:
DEPART TIME:
TOTAL TRAVEL:
TOTAL TIME:
CLIENT REP:
MILEAGE:
DATE: 9/5/24
TERRACON REP: (u)
PDA MODEL/SN: SPT 4021 TR
TERRACON RIG #: 1307

DRILL RIG DATA
Type/Transport: Fork
Manufacturer: Geopole
Model No.: 3126 GS
Serial No.: 7126550224106
Year Built: 2024
Modifications: N/A
Maint. Schedule: 50 hrs

SPT HAMMER DATA
Type: A10
Manufacturer: Geopole
Lifting Mechanism: Claw
Model No.: AD1131
Serial No.: 10001
Hammer Weight: 140
Hammer Operator(s): B. R. HEAT

PDA INPUT DATA
Operator: OP (u)
Project No./Location: PJ 7324515/
Rig Mode & SN: PN 60000/3126 GS
Hammer Type, LM, Rods: PD A10/AWJ
Drill Rod Area (in^2): AR 115
Elastic Modulus (ksi): EM 3000
Specific Weight (kips/ft^3): SP 0.492
Wave Speed (ft/sect): WS 16808
Increment Length (ft): LI 0.5
Sampling Freq (kHz): FR 50

TRANSDUCER INFORMATION
Gage SN Calibration
F1/F3: 746 AWJ1 222.05
F2/F4: 746 AWJ2 222.09
A1/A3: K14002 402.23
A2/A4: K14006 375.83
NOTES: 286.25 + 1.875 = 288.125
34.38 * 25 + 10.5 = 886.75
SPLIT SPOON SAMPLER LENGTH: 38K + 0.88 = 38.88
LE is measured from the center of the strain gauges to the bottom of split spoon sampler

SPT TESTING INFORMATION table with columns: Start Time, Soil, Stick Up Length (ft), Depth (ft), LE (ft), Rods & Lengths, PDA Blows, SPT Blows.

Individual pairs of F or V signals versus time shall be very similar for good quality data.
If you see Force goes negative before 2L/C after impact, drill rod joints should be carefully tightened for good quality data

PICTURE NUMBERS AND INFO:
Take Photo of Each Rigs, Boring Locations at the Site

Terracon SPT Rig Calibration Worksheet.xlsx



This documents that
Susheel R. Kolwalker
Terracon Consultants
has on March 11, 2016 achieved the rank of
EXPERT

on the Dynamic Measurement and Analysis Proficiency Test.

The individual identified on this document demonstrated to the degree granted above an understanding of theory, data quality evaluation, interpretation and signal matching for high strain dynamic testing of deep foundations.

The ability of the individual named to provide appropriate knowledge and advice on a specific project is not implied or warranted by the Pile Driving Contractors Association or Pile Dynamics, Inc. The Pile Driving Contractors Association or Pile Dynamics, Inc. assumes no liability for foundation testing and analysis work performed by the bearer of this certificate. This certificate can be verified at www.PDAproficiencytest.com.

Steven A. Hall, Executive Director
Pile Driving Contractors Association

Garland Likins, Senior Partner
Pile Dynamics, Inc.

No. 2005



Exhibit E

Copy of Certificate of Proficiency

Certificate of Proficiency for Ryan Wakeford, Terracon Consultants, Inc. on the Dynamic Measurement and Analysis Proficiency Test. Includes PDCA and PDI logos, signatures of Frank T. Peters and Garland Likins, and a gold seal.