# Hot Mix Asphalt (HMA) Quality Assurance

# SCDOT Designation: SC-M-400 (05/10)

## 1. SCOPE

Base field acceptance of hot mix asphalt (HMA) mixtures on asphalt binder content, air voids, voids in mineral aggregate (VMA), and in-place mat density of the pavement. Warm mix asphalt (WMA) contracts will use this specification for mixture acceptance if the individual contract specification requires WMA mixtures in lieu of HMA. Base decisions regarding acceptance, rejection, or acceptance at an adjusted price upon the percentage of the lot that is within the specification limits. Apply all other acceptance criteria documented in the special provisions, supplemental specifications, and sections of the Standard Specifications, except as noted herein. If unable to meet these other acceptance criteria, cease production and take steps necessary to bring the process into compliance with the acceptance criteria.

This specification is comprised of three sections:

- Section 3 GENERAL Describes what is required to meet the Hot Mix Asphalt (HMA) Quality Assurance (QA) Specification. This section describes requirements, frequency, sampling and testing methods, acceptance and verification, and the party responsible for each item.
- Section 4 ACCEPTANCE OF MAINLINE PAVING Describes what mainline production consists of (including shoulders, ramps, and acceleration/deceleration lanes), and the requirements and pay factor calculations for mainline paving on a LOT basis as described in Subsection 4.1.1 and Subsection 4.1.2.1.
- Section 5 ACCEPTANCE OF LOW TONNAGE PAVING Describes what low tonnage is, and the requirements and pay factor calculations associated with low tonnage paving. Low tonnage is defined as 2500 tons or less of a specific HMA mixture on a project or when the specific HMA mixture is to be used for non-mainline work, such as patching, leveling, widening less than 8-feet, wedging and driveway paving. The pay factor calculations for non mainline paving will be calculated on a LOT-to-LOT basis as described in Subsection 5.1.1 and Subsection 5.1.2.1.

# 2. REFERENCED DOCUMENTS

- 2.1 SCDOT Standard Specifications
- 2.1.1 Division 300, Division 400
- 2.2 SCDOT Supplemental Technical Specifications
- 2.2.1 SC-M-404, SC-M-405
- 2.3 AASHTO and ASTM Standards
- 2.3.1 R 11, R 18, ASTM E29
- 2.4 SCDOT Test Methods

2.4.1 SC-T-1, SC-T-2, SC-T-4, SC-T-62, SC-T-65, SC-T-68, SC-T-71,SC-T-72, SC-T-75, SC-T-78, SC-T-80, SC-T-83, SC-T-84, SC-T-85, SC-T-86, SC-T-87, SC-T-96, SC-T-97, SC-T-98, SC-T-101, SC-T-102, and SC-T-103.

### 3. GENERAL

#### 3.1 Job Mix Formula

Combine the mineral aggregates and asphalt binder in accordance with **SC-T-80** in such proportions that the finished HMA mixture complies with all applicable requirements specified in the Standard Specifications (including any supplemental specifications) and the special provisions. When allowed by **SC-M-402**, and used in the HMA, liquid anti-stripping additives must be introduced into the mixture and controlled in the field in accordance with **SC-M-406**. A Surface course is defined as the following; Surface Types A, B, CM, C, D and E. An Intermediate course is defined as the following mix types; Intermediate Types A, B and C, and Base mixtures are Base Types A, B, C and D. Open Graded Friction Course (OGFC) and Asphalt Shoulder Widening Course are also referred to in the specification.

If the HMA mixture does not meet the acceptance control limits, submit a revision to the job mix acceptance target values provided the revised job mix meets all of the requirements of the specifications. A job mix revision is only allowed between LOTS. Fax a copy of all job mix revisions to the District Asphalt Manager (**DAM**), the Asphalt Materials Engineer (**AME**), and, if appropriate, the District Materials Laboratory before starting the LOT on which the revised job mix will first be used. Attach all supporting data, including volumetric properties and gradation from previous laboratory tests, to job mix revisions. The Department will accept all revisions as submitted unless the revisions are made outside of the acceptable tolerances and specifications.

Initial job mix formulas are valid for 2 years with a maximum of 3 revisions. If additional revisions are required after the allowable 3 have been made, a new job mix formula is required. Prepare the new job mix formula in accordance with **SC-T-80** or **SC-T-88** and comply with all applicable requirements specified in the Standard Specifications (including any supplemental specifications) and the special provisions.

Job mix formulas are associated with a specific plant, which will be approved for an individual project. Therefore the start of a new project constitutes the beginning of a new set of LOT numbers. A calibration period for either a project or a job mix formula is not permitted. LOT numbers begin immediately with the production of the mixture. If during production of a particular type of mix, a new job mix formula is needed, LOTS run continuously until the project is complete.

#### 3.2 Personnel Requirements

Provide sufficient SCDOT certified personnel trained to perform the required inspections, sampling, testing, verification, and documentation at the plant and on the roadway. A certified Level 2S HMA Technician will prepare mix designs in an SCDOT approved mix design laboratory meeting the requirements outlined in **SC-M-405**. Provide certified Level 1 HMA Technicians at each plant site used to furnish material to the project. Conduct all sampling and testing at the plant by a certified Level 1 HMA Technician or by a candidate for certification working in the presence and under direct observation of a certified Level 1 HMA Technician. Provide certified Asphalt Roadway Technicians or candidates for certification working in the presence and under direct observation of a certified Roadway Technician to perform the necessary inspection, sampling, testing and documentation on the roadway, however, the certified Level 1 or Roadway Technician is responsible for all testing and reporting. Have a certified Level 3 HMA Quality Control Manager readily available to be on site within an hour and a half, to make necessary process adjustments, make periodic visits to each active plant at a rate of no less than two times per month, review calibration and verification records as needed,

be responsible for all quality control activities at each plant they oversee, and monitor mixture production, placement and testing on each project. The Contractor Level 3 QC Manager will provide insight to problems that arise during mix design and production, and therefore <u>should</u> be employed by the company he/she is representing. This person is the Department's primary contact should a problem develop during a project and will be held responsible for all Quality Control / Quality Acceptance testing.

Ensure that technician certifications are in accordance with the Department's HMA Technician Certification Program. Post a current organizational chart, including names, telephone numbers and current certification, of those responsible for the Quality Control program in the laboratory and provide a copy to the **DAM**. Update this chart with appropriate changes, as they become available.

The Department will provide certified Asphalt Roadway Technicians and/or certified Level 1 HMA Technicians or candidates for certification working in the presence and under direct observation of certified personnel to perform the necessary inspection, documentation and testing on either the roadway, in the plant laboratory or in the testing laboratories. Verification laboratories will be AASHTO accredited and lab technicians will be responsible for performing yearly AMRL proficiency samples.

#### 3.3 Field Laboratory Requirements

Provide a laboratory at the plant. The laboratory will be inspected annually by a representative of the **AME** in accordance with **SC-M-404** and *SCDOT Qualified Product Policy 76*. Ensure that the laboratory is listed in the most recent edition of *SCDOT Qualified Product List 76*.

Maintain the laboratory and calibrate and verify all equipment in accordance with **AASHTO R 18.** Maintain records of calibration and verification in the laboratory. The **AME** or a District representative will inspect measuring and testing devices to confirm both calibration and condition. If the laboratory is found to be in satisfactory compliance with **SC-M-404** and SCDOT *Qualified Product Policy 76*, it will be placed on *SCDOT Qualified Product List 76*. If it is determined that the equipment is not within the limits of dimensions or calibration described in the appropriate test method, the **AME** representative may stop production until corrective action is taken. If the necessary laboratory equipment is inoperable at the time of a required acceptance test, cease HMA mixture production.

#### 3.4 Quality Control (QC) Program

Provide to the **AME** a QC program that defines all activities, including mix design, process control inspection, sampling, testing, and necessary adjustments in the process that are related to the production and placing of an HMA pavement. At a minimum, conform the QC program to meet the entire specifications and requirements stipulated herein as well as all other acceptance criteria documented in the special provisions, supplemental specifications, and applicable sections of the Standard Specifications. Detail actions that will take place in the absence of a certified Level 3 QC Manager and what steps will take place to ensure all specifications are being met. Document any additional testing that is required by your company to ensure process control, such as obtaining additional check samples to determine whether or not the asphalt plant production shall be ceased before the next quality acceptance sample is obtained. The Department can require production to cease if procedures and requirements stated in the QC program are not followed, until such steps are taken to ensure that all QC program procedures are followed and all requirements are met.

3.5 Required Plant and Roadway QC Tests and Verifications

Perform or have performed the quality control tests specified herein.

#### 3.5.1 Required Plant QC Tests and Verifications

Use the test methods identified in Table 1 to perform QC tests and verifications at a frequency not less than that indicated. All other acceptance criteria documented in the special provisions, supplemental specifications, and sections of the Standard Specifications, except as noted herein, still apply. If unable to meet other acceptance criteria not specifically stated in this specification, cease production and take necessary steps to bring the process into compliance with the acceptance criteria.

| Parameter   | Minimum Frequency                             | Sampling<br>Method                             | Test Method           |
|---|---|--|-----------------------|
| Maximum Specific Gravity<br>(excluding Base Courses, Surface<br>Type E, and OGFC) | 1 per SUBLOT                                  | SC-T-101,<br>SC-T-62,<br>SC-T-72 or<br>SC-T-93 | SC-T-83               |
| Mixture Gradation   | 1 per Odd numbered<br>SUBLOT                  | SC-T-101,<br>SC-T-62,<br>SC-T-72 or<br>SC-T-93 | SC-T-102              |
| Mixture Stability<br>(Base C&D, Surface Type E)                                   | 1 per LOT                                     | SC-T-101,<br>SC-T-62,<br>SC-T-72 or<br>SC-T-93 | SC-T-96               |
| Lime Rate Verification  | 2 per LOT                                     | SC-T-71  | SC-T-71 or<br>SC-T-78 |
| Individual Aggregate<br>Stockpile Gradation                                       | 1 per 10,000 tons<br>(or min. of 1 per month) | SC-T-1,<br>SC-T-2                              | SC-T-4                |

| Table 1. Required | Plant QC Tests ar | nd Verifications |
|-------------------|-------------------|------------------|
| Table II Required |                   |                  |

#### 3.5.2 Required Roadway QC Verifications

Maintain an approved density gauge, on site, during all HMA placing and compaction operations and use the gauge to assist in the quality control of the compaction process. Require the proper number and type of rollers needed to obtain density as determined by **SC-T-65**. When density is used for acceptance, ensure that rollers meet the requirements in Section 401.3 of the Standard Specifications. Maintain roller pattern documentation (SCDOT Form 400.21) on site and perform new roller patterns when there is a change in underlying support, type of asphalt, thickness in mat or other elements (such as different rollers) that might affect the final density. Monitor the roller patterns, mixture placement, and mixture compaction during production on all projects except for driveways and full-depth patching. Verify and document the ambient air temperature and the HMA mix temperature at the roadway, at a frequency not less than that indicated in Table 2. The Department will verify temperatures, calculate and document both the lay down rate for each 200 tons and the cumulative lay down rate (in pounds per square yard), and verify and document the tack rate and type at frequencies not less than those indicated in Table 2.

| Parameter             | Minimum Frequency | Test Method | Responsible<br>Party |
|-----------------------|-------------------|-------------|----------------------|
| Monitoring of density | Continuous        | SC-T-65     | Contractor           |

| Table 2. Required | Road QC T | ests and \ | /erifications |
|-------------------|-----------|------------|---------------|
|-------------------|-----------|------------|---------------|

| Temperature:<br>Ambient air         | Before paving starts,<br>then 2 per LOT | SC-T-84 | Department |
|-------------------------------------|---|---------|------------|
| Mat                                 | 4 per LOT                               | SC-T-84 | Department |
| Mixture Temperature<br>Verification | 4 per LOT                               | SC-T-84 | Department |
| Calculated Lay Down<br>Rate         | 1 per 200 tons                          | SC-T-85 | Department |
| Tack Rate, Type                     | 1 per application                       | SC-T-86 | Department |

#### 3.6 Acceptance Program

Perform or have performed the acceptance tests specified herein.

#### 3.6.1 Plant Calibration

Calibrate the plant so that the mix conforms to the job mix formula and field acceptance criteria prior to production.

#### 3.6.2 Required Plant Acceptance Tests

Use the test methods identified in Table 3 and perform the plant acceptance tests at a frequency not less than that indicated. Carry calculations for the test results for asphalt binder content, air voids, and VMA to the thousandths (0.001) and round to the nearest hundredth (0.01). Carry calculations for the test results for gradation to the hundredths (0.01) and round to the nearest tenth (0.1) except for the No. 200 sieve and dust to asphalt ratio. Carry the No. 200 sieve and the D/A ratio to the thousandths (0.001) and round to the nearest hundredth (0.01). Carry calculations for averages to the thousandths (0.001) and round to the nearest hundredth (0.01). Carry calculations for averages to the thousandths (0.001) and round to the nearest hundredth (0.01). Round the calculations in accordance with the **ASTM E29** rules of rounding.

#### Table 3. Required Plant Acceptance Tests

| Test Parameter   | Typical Frequency | Sampling Method                                 | Test Method             |
|--|-------------------|---|-------------------------|
| Asphalt Binder Content, %  | 1 per SUBLOT      | SC-T-101, SC-T-62<br>and<br>SC-T-72 or SC-T-93  | SC-T-75                 |
| Voids Analysis<br>Air Voids, %<br>VMA, %<br>(excluding Base Courses,<br>Surface Type E and OGFC) | 1 per SUBLOT      | SC-T-101, SC-T-62,<br>and<br>SC-T-72 or SC-T-93 | SC-T-103<br>and SC-T-68 |
| Mixture Gradation<br>(Base Courses, Surface Type E,<br>and OGFC only)                            | 1 per SUBLOT      | SC-T-101, SC-T-62,<br>and<br>SC-T-72 or SC-T-93 | SC-T-102                |

#### 3.6.2.1 Asphalt Binder Content

When using the procedures in **SC-T-62**, obtain a mixture sample of at least 35 pounds. Split the sample into 3 approximately equal sized samples in accordance with procedures in **SC-T-72 or SC-T-93**. The 3 samples will be identified as acceptance test sample, verification test sample, and referee sample. Bag, label and store the portions of mixture for the Department's verification test sample and the referee sample for later testing as required in Subsection 3.8, "Split Test Sample Program." Retain the split samples in a dry, protected location for a minimum

of 4 production days. A production day is defined as a day that mixture is produced for Department projects. Dispose of split samples that have not been selected by the Department for verification testing after 4 production days. For all verification samples selected by the Department, retain the corresponding referee split sample in a dry, protected location until the verification test result is available and it is determined that no referee testing will be required for the split sample. In the event that a referee sample has been disposed of by the contractor, verification test results will be used to compute LPF.

Calibrate the ignition oven for each job mix prior to producing mix. Perform oven calibrations and verifications in accordance with **SC-T-75**. Keep all calibrations and verifications along with supporting data in a notebook readily available in the field laboratory. The **DAM** or **AME** may require re-calibration of the ignition oven if the verification test and the referee test do not compare within allowable limits.

#### 3.6.2.2 Voids analysis

Compact the specimens in accordance with **SC-T-103.** Determine the percent air voids and VMA by **SC-T-68**. Compare the bulk specific gravity of the compacted mixture with the maximum mixture specific gravity determined by **SC-T-83** to determine the air voids. Retain compacted specimens in a dry, protected location for a minimum of 4 production days. Dispose of the compacted specimens that have not been selected by the Department for verification testing after 4 production days. Use the average of a minimum of 2 maximum specific gravity specimens for each SUBLOT when computing air voids. The maximum allowable individual difference for bulk specific gravity and maximum specific gravity specimens are 0.020 and 0.018, respectively. Inform the **DAM** or **AME** immediately if specimens do not compare. Voids analysis will not apply for Base Courses, Surface Type E and OGFC.

3.6.2.3 Gradation (For Base Courses, Shoulder Widening Course, Surface Type E, and OGFC Only)

Perform gradation **SC-T-102** for each SUBLOT for acceptance purposes for Base Courses, SWC, PMS, Surface Course Type E, and OGFC. Evaluate each SUBLOT's gradation on an individual basis for pay purposes.

- 3.6.3 Required In-Place Density Acceptance Tests
- 3.6.3.1 Intermediate Courses and Surface Courses Type A, B, CM

SCDOT will compute in-place density on cores obtained from the pavement for Intermediate courses, and Surface courses Type A, B, and CM. Use **SC-T-87** as identified in Table 4 to perform the density acceptance tests at the frequency indicated.

3.6.3.2 Base Courses, and Surface Course Type C and D

Determine the in-place density for Base courses, and Surface Course Type C and D, by the use of an approved density gauge and procedure. Ensure that the gauge has been approved by the **AME**. Furnish and operate the gauge to determine in-place density results at a frequency not less than that indicated in Table 4. Divide each LOT into equal SUBLOTS corresponding to the number of density values to be obtained. Use **SC-T-101** and determine one gauge density value at a randomly selected location within each SUBLOT. Express the in-place density as a percentage of the target density. The target density shall be determined from a control strip constructed in accordance with **SC-T-65**. Carry out calculations for density to the hundredths (0.01) and round to the nearest tenth (0.1) in accordance with **ASTM E29** rules of rounding. Allow Department personnel to witness the above procedure being performed.

| Test Parameter  | Typical Frequency |                            | Sampling<br>Method  | Test<br>Method |
|---|-------------------|----------------------------|---------------------|----------------|
| In-Place Density<br>(% of Max. Theoretical)<br>Note: Requirements apply to  | Surface           | 1 per 2,000 foot<br>SUBLOT | SC-T-101<br>SC-T-87 | SC-T-87        |
| Intermediate Courses and to Surface<br>Courses Type A, B CM   | Intermediate      | 1 per 1,500 foot<br>SUBLOT |                     |                |
| In-Place Density<br>(% of Target Gauge Control<br>Strip Density)<br>Note: Requirements apply for Base<br>Courses and Surface Courses<br>Type C& D | 10 p              | er LOT                     | SC-T-101            | SC-T-65        |

#### Table 4. Required Roadway Acceptance Tests

#### 3.6.3.4 Surface Course Type E and Open Graded Friction Course (OGFC)

Surface Type E and OGFC will not have in place density performed. Place these mixes at the proper rate and promptly roll as indicated in the standard specifications.

#### 3.7 Failing Samples and Plant Operations

Obtain another sample, a check sample, when a sample fails to meet the specification limits as outlined in Subsection 4.2.1.1, "Specification Limits," on any one of the following properties: asphalt binder content, air voids, VMA, or fails to meet the job mix formula requirements for gradation, and/or dust to asphalt ratio. Denote the check sample as a check sample and do not use it in calculating pay factors. Only the samples obtained at the predetermined random sample tonnage can be used for computing the daily pay factors. If however, the random sample tonnage fails within the 3-and-hold segment, obtain a sample from the first truckload produced after the 3-and-hold segment and use this sample as the pay factor sample. If no more truckloads are needed on the project, use only the samples obtained in accordance to **SC-T-101**. Use all other samples taken between random sampling tons for informational purposes only.

Make necessary adjustments, produce 3 truckloads of mix and hold plant production until the test results are obtained from the third truckload when 2 consecutive acceptance samples fail on any one of the following properties: asphalt binder content, air voids, VMA, gradation, and/or dust to asphalt ratio. If this sample fails, discard the mixture in the silo, clean out the plant and resume production only when the mix produced meets the all job mix properties. If at the end of the day the mix still fails to meet specifications, make necessary adjustments or changes before starting the next day's production, produce 3 truckloads and hold plant production until results are obtained from the third truck load. When on 3-and-hold, do not send mix to the project until a sample meets all specification limits. This procedure may be altered when the Resident Construction Engineer (**RCE**) deems necessary.

Immediately inform the **DAM**, or the **DAM**'s appointed Departmental representative when 2 consecutive failing samples occur. All 3-and-hold plant or mix adjustments must be documented on a corrective action form and posted in the field laboratory. This form must be filed and a copy of the form must be turned into the DAM once mixture is back within all JMF criteria.

Perform at least one entire series of required plant acceptance tests on the next random sampled following a failing sample as outlined in Tables 1 and 3 for information purposes only to ensure conformity within specifications limits.

#### 3.8 Split Test Sample Program

Department personnel may witness the Contractor quality control and acceptance sampling and testing being performed. If it is observed that the sampling or the quality control or acceptance tests are not being performed in accordance with the applicable test procedures, the Department personnel witnessing the sampling and testing will immediately notify the Contractor and the **DAM** of the observed deficiencies. The **DAM** will investigate the observed deficiencies and, if the deficiencies are not immediately corrected, the **RCE**, **DAM** or the **AME** may stop production until corrective action is taken. The Department representative will document all witnessed samples and tests. The Department representative may elect to obtain samples for testing, separate from the Contractor's sampling and testing process, to augment validation of specification compliance.

The Department will conduct its own tests to validate test results. The validation tests for asphalt binder content and maximum specific gravity will be on split test samples (see Subsection 3.6.2, "Required Plant Acceptance Tests"). The acceptance tests for in-place density will be on the cores (see Subsection 3.6.3, "Required In-Place Density Acceptance Tests"), or based on density gauge readings.

The frequency of the Department's split test samples will in general be equal to or greater than ten percent (10%) of the tests required. The Department will provide the split test sample results within 6 working days of the sample being obtained by the laboratories. Conduct at least one split test sample for asphalt binder content, gradation, in-place density, and voids analysis from the first 2 days of production. Additionally, the Department may select any or all retained samples for further testing. All split test samples testing and data analysis will be performed by or under the supervision of a Certified HMA Level 1 Technician. Inspect measuring and testing devices to confirm both calibration and condition. Calibrate and correlate all testing equipment in accordance with **AASHTO R18**.

#### 3.8.1 Asphalt Binder Content and Maximum Specific Gravity

For split samples that are tested by both the Contractor and the Department, the test results for asphalt binder content and maximum specific gravity will be compared to each other. If the differences are within the allowable differences listed in Table 5, no further testing or analysis will be necessary and the Contractor's test values will be used in the computation of the asphalt binder content LOT pay factor.

When differences between the Contractor's and Department's test results are not within the allowable limits in Table 5, referee testing will be required. When referee testing is required, the Office of Materials and Research (**OMR**) will test the referee sample. If the original verification sample was tested in the **OMR**, then a District Materials Laboratory (**DML**) will test the referee sample. If the difference between the referee sample test result and the Contractor's initial test result is within the allowable limits in Table 5, then the initial Contractor's test result will be used in the computation. If the difference between the referee sample test result and the Contractor's initial test result is not within the allowable limits in Table 5, then the referee sample test result and the Contractor's initial test result is not within the allowable limits in Table 5, then the referee sample test result and the Contractor's initial test result is not within the allowable limits in Table 5, then the referee sample test result will be used in lieu of the Contractor's test result in the computation. In the event that referee binder content does not compare the referee result will be entered by the DAM into the contractor's daily report, and pay factors for Binder Content and % VMA will be recomputed for a revised LPF. In the event that a referee maximum specific gravity does not compare, the referee result will be entered by the DAM into the contractor's daily report, and pay factors for % Air voids, % VMA, and In-Place Density will be recomputed for a revised LPF.

In the event comparison of the required test results is outside the allowable differences in Table 5, Department verification samples fail the specification limits, or a continual trend of difference between Contractor and Department test results is identified, the **DAM** will immediately investigate. The **DAM** may suspend production while the investigation is in progress. The investigation may include testing by the Department of any remaining split samples or a

comparison of split sample test results on the mixture currently being produced. The investigation may also include review and observation of the Contractor's technician's performance, testing procedure, and equipment.

| Test Parameter            |                          | Allowable Difference |
|---------------------------|--------------------------|----------------------|
| Asphalt Binder Content, % |                          | ± 0.40               |
| Maximum Sp                | Maximum Specific Gravity |                      |
| Bulk Specific 0           | Gravity of Cores         | ± 0.035              |
|                           | 1⁄2" and greater         | ± 7.0                |
| Gradation                 | 3/8"                     | ± 6.0                |
| (Base, Shoulder           | No. 4                    | ± 6.0                |
| Widening, Surface Type E  | No. 8                    | ± 5.0                |
| and OGFC only)            | No. 30                   | ± 4.0                |
|                           | No. 100                  | ± 3.0                |

#### Table 5. Allowable Differences Between Contractor Tests and Department Split Sample Tests

#### 3.8.2 Gyratory Density Cores

For the gyratory cores that are tested by the Contractor for material acceptance, the Department will perform split sample testing by either directly observing the contractor running the bulk specific gravity tests or later by performing the test by re-weighing the retained gyratory cores. If the bulk specific gravity differences are within the allowable differences listed in Table 5, no further testing or analysis will be necessary and the Contractor's values will be used in the computations for LOT pay factor. If the bulk specific gravity differences are not within the allowable differences are not within the allowable differences are not within the allowable differences listed in Table 5, referee testing will be required.

When referee testing is required for bulk specific gravity, the **OMR** will test the retained core. In either event, the bulk specific gravity referee test result will be used in lieu of the Contractor's test result to calculate the density of that core. The density obtained using the referee bulk specific gravity will be used in lieu of the Contractor's value in the computation of the LOT pay factor.

In the event comparison of the required test results is outside the allowable differences in Table 5, Department verification samples fail the specification limits, or a continual trend of difference between Contractor and Department test results is identified, the **DAM** will immediately investigate. The **DAM** may suspend production while the investigation is in progress. The investigation may include testing by the Department of any remaining retained cores. The investigation may also include review and observation of the Contractor's technician's performance, testing procedure, and equipment.

#### 3.8.2.2 Verification of Contractor's Density - Base Courses, Surface Course Type C and D

The Department will observe the establishment of the target density in accordance to **SC-T-65**. The Contractor, for verification of the established roller pattern, will retain a copy of Form 400.21 on the roadway and forward to the **RCE**. The Department will observe and document on Form 400.04 the density readings equal to or greater than 10% of the tests required for the Contractor.

In the event that a problem with density arises, the **DAM** will immediately investigate. The **DAM** may suspend production while the investigation is in progress. The investigation may include testing by the Department of other LOTS. The investigation may also include review and observation of the Contractor's technician's performance, testing procedure, and equipment.

#### 3.8.3 Voids Analysis

In the event that a Contractor has comparison issues as compared to SCDOT Independent Assurance Samples, the **DAM** and the **AME** will immediately investigate. The **DAM** may suspend production while the investigation is in progress. The investigation may include testing by the Department of additional samples, or a comparison of split sample test results on the mixture currently being produced. The investigation may also include review and observation of the Contractor's technician's performance, testing procedure, and equipment.

#### 3.9 Verification Program

The Department's verification tests will be conducted at an SCDOT HMA Verification Laboratory, or at the **OMR**'s Central or District Laboratories. The Department will coordinate verification testing in an effort to minimize the impact on normal quality control and acceptance testing.

Department verification tests will be compared statistically to Contractor acceptance tests following **SC-T-97**, "Method for Verification of Contractor HMA Acceptance Test Results." The Department's HMA Verification Manager will perform this comparison in conjunction with the applicable managers of the Verification Laboratories for this project and the applicable **DAM**. Because a sufficient number of samples are needed for this statistically-based verification process, the contract unit price will be paid on the monthly estimates until the verification process is complete. Projects are not considered complete until the HMA Verification Manager has all data, has performed all analyses required, and has provided the **DAM** the necessary information to complete all payment related functions.

#### 3.10 Documentation

Document all observations, records of inspection, adjustments to the mixture, test results, QC verifications, and corrective actions. Provide legible copies of this documentation to the **RCE** within 30 calendar days of the completion of the hot mix asphalt work on the project. Maintain all permanent records unless the Department is given the permanent records during production of the mixture. Provide Department representatives full access to all QC, acceptance, and verification documentation throughout the progress of the work. Make available at all times these documents, either in paper form or viewable on a computer monitor, to the Department representatives for review.

Continue from contract to contract, charts, records, and testing frequencies for a HMA mixture produced at plant site.

### 4. ACCEPTANCE OF MAINLINE PAVING

Evaluate all materials used for mainline paving for acceptance by the Department's Acceptance Procedures specified herein. Utilize results from the acceptance testing when determining the acceptability of the materials. In addition, the Department will conduct limited testing and monitor and observe sampling and testing procedures to verify the data used for acceptance purposes. The Department's data will be compared with data from the acceptance testing program as described in Subsection 3.8, "Split Test Sample Program" and Subsection 3.9, "Verification Program." Conduct acceptance test sampling and testing on a random basis according to frequencies indicated in Subsection 3.6, "Acceptance Program." Determine all sampling tons and roadway locations randomly using **SC-T-101**. Notify the **DAM** at least one day prior to any production in order to make necessary arrangements for verification. Failure to do so could result in no payment for that given day's production.

Record all inspections and test results on approved forms and charts and keep up to date records that are available at all times to the Department during the performance of the work. Utilize only those tests designated in advance as acceptance tests in the computation of pay

factors. Record test results on forms provided by the Department. The Department will prepare and distribute uniform forms for reproduction for use as required. Deliver, either by person, email or fax all test results necessary to calculate payment factors to the **DAM** no later than 3 working days after the completion of the LOT, or production can be halted until results are delivered. Provide a copy of each truck ticket printout with the corresponding plant acceptance test results.

#### 4.1 Mixture

Evaluate the HMA mixture at the plant, with respect to asphalt binder content and to the air voids and VMA of laboratory-compacted samples, on a LOT-to-LOT basis. Test the material for acceptance in accordance with the provisions of these special provisions. Reject any load or loads of mixture, which, in the opinion of the Department's certified roadway technician, are obviously contaminated, segregated, or otherwise unacceptable for use in the work.

#### 4.1.1 Mainline production

Base the acceptance and pay factors for asphalt binder content and the volumetric properties of air voids and VMA on the percentage of the LOT that is within the specification limits based on the Quality Index calculated using the test results from the LOT. A LOT for asphalt binder content and volumetric properties is defined as a day's production with at least 3 SUBLOTS, where a SUBLOT consists of 500 tons of a particular mixture.

Therefore, in accordance to Table 3, if 4 tests are obtained from a given LOT, calculate the Quality Index on the results of four tests (n=4). However, when operational conditions are such that fewer than 4 tests are obtained from the production on a given day, follow the procedure in the next paragraph.

If the number of tests obtained from the day's production is three (n=3), compute the Quality Index from the results of the 3 tests and use the corresponding table for n=3. If insufficient tests (n=1 or n=2) are obtained from the day's production, combined these results with the next day's production SUBLOTS until at least 3 tests are obtained. If the next day's production is not within 30 days of the open SUBLOT, combine the open SUBLOT with enough tests from the previous completed LOT to yield 3 tests and calculate the Quality Index and close out the open LOT. If the last LOT on the project has only 1 or 2 tests, combine with enough tests from the previous LOT to yield 3 tests and calculate the Quality Index.

If the first SUBLOT is expected not to reach the random tonnage according to Table 1 of **SC-T-101**, then perform at least one series of Plant Quality Control and Acceptance tests for payment. Provide a random sampling tonnage for such low-production days to the **DAM** prior to production. In the event that production falls short of random tonnage for the first sample, contact the **DAM** and notify them that a new sampling tonnage needs to be determined. In the event that the **DAM** can not be contacted, obtain a sample from the last truck containing tonnage being sent to the roadway. If production continues, refer to Table 1 of **SC-T-101** for sampling tonnage for the second and following SUBLOTS of the mixture.

#### 4.1.2 In-Place Density

For mainline paving (including shoulders, ramps, and acceleration/deceleration lanes), apply inplace density pay factors as specified herein unless otherwise noted on the plans. The Department's Certified Roadway Technician is responsible for determining the random core locations and providing the information to the contractor for each SUBLOT in accordance to **SC-T-101** once compaction has been completed.

#### 4.1.2.1 Intermediate Courses and Surface Courses Type A, B, and CM Evaluate the in-place density for Intermediate courses and Surface courses Type A, B and CM,on a LOT-to-LOT basis, where a LOT is defined as a day's production with at least 3 plant

acceptance SUBLOTS. Therefore, if less than 3 plant SUBLOTS are performed for a given day, combine the roadway cores taken from the first day with the following day(s) until at least 3 plant acceptance SUBLOTS are completed.

In the event that less than 3 roadway cores are obtained, but 3 plant acceptance SUBLOTS are complete, use the entire length of the represented LOT to establish the remaining core(s) to close the LOT.

Express the in-place density as a percentage of the theoretical maximum mix density. Calculate the theoretical maximum density from the maximum specific gravity as determined by **SC-T-83**. Determine the maximum specific gravity by averaging the maximum specific gravity results of the entire LOT. Carry calculations for density to the hundredths (0.01) and round to the nearest tenth (0.1) in accordance with **ASTM E29** rules of rounding.

4.1.2.2 Base Courses and Surface Course Type C and D

Evaluate Base Courses and Surface Course Type C and D on a LOT-to-LOT basis. Compute the in-place density by comparing density values determined by the use of an approved density gauge to the target density established on control strips constructed in accordance with **SC-T-65**. Construct a control strip at the beginning of work. Construct additional control strips when a change is made in the type or source of materials or compaction equipment, or whenever a significant change occurs in the composition of the underlying pavement structure or the composition of the material being placed from the same source.

4.1.2.3 Shoulder Widening Course, Surface Course Type E and Open Graded Friction Course

Shoulder Widening Course, Surface Course Type E and OGFC will not have to have in place density performed. Place these mixtures at the proper rate and promptly roll as required by the standard specifications.

#### 4.2 Acceptance Plan

It is the intent of these specifications that each LOT meets specification requirements at the time of initial evaluation. No re-sampling or re-testing (other than referee testing described in Subsection 3.8, "Split Test Sample Program") will be allowed.

Adjust the payment for each LOT on the basis of acceptance test results in accordance with the requirements of these specifications. Keep accurate records of the tonnage of HMA in each LOT. Determine pay factors as indicated below.

#### 4.2.1 Determination of Pay Factor for Mainline Paving

For mainline LOTS, determine pay factors for asphalt binder content, air voids, VMA, and inplace density for Intermediate courses, and Surface courses Type A, B, CM and C, based on the estimated PWL determined from the Quality Index and Tables 12 through 20. The Quality Index uses both the average and standard deviation within each LOT to estimate the percentage of the LOT within the specification limits. Remove and replace all material in the LOT that has a TPWL of 20 or less for any one acceptance characteristic, or has a TPWL of 40 or less for any 2 acceptance characteristics, or has a TPWL of 60 or less for any 3 or more acceptance characteristics. For material with a TPWL greater than 60, compute the unit bid price in accordance with Subsection 4.2.1.3, "Pay Factors."

Base the pay factor for in-place density for Base Courses and Surface Course Type C and D on the percent of the established target density. Compute the pay factor for in-place density and the unit bid price in accordance with Subsection 4.2.1.3, "Pay Factors." Compute only binder content and gradation pay factors for Surface Course Type E and OGFC.

#### 4.2.1.1 **Specification Limits**

Calculate the specification limits for mixture properties from the allowable tolerances from the job mix formula (JMF) shown in Table 6.

| Characteristic            | Surface   | Intermediate | Base      |
|---------------------------|-----------|--------------|-----------|
| Characteristic            | Tolerance | Tolerance    | Tolerance |
| Asphalt Binder Content, % | 0.36      | 0.43         | 0.50      |
| Air Voids, %              | 1.15      |              |           |
| VMA, %                    | 1.15      |              |           |

#### Table 6. Allowable Tolerances from the Job Mix Formula for Mixture Properties

Compute the specification limits for mixture properties using the tolerances from Table 6 and the following equations:

LSL = JMF - Tolerance

Where:

| USL       | = Upper Specification Limit         |
|-----------|-------------------------------------|
| LSL       | = Lower Specification Limit         |
| JMF       | = Job Mix Formula Target Value      |
| Tolerance | = Allowable Tolerance from Table 6. |
|           |                                     |

The in-place mat density specification limits are shown in Table 7.

| Table 7. Specification | Limits for | In-Place Density |
|------------------------|------------|------------------|
|------------------------|------------|------------------|

|  | Intermediate Courses and<br>Surface Type A, B and C |      | Base Courses and<br>Surface Type D |     |        |     |
|--|---|------|------------------------------------|-----|--------|-----|
| % of Theoretical<br>Maximum Density    | LSL   |      | USL                                | LSL | Target | USL |
| Interstate and<br>US Primary<br>Routes | 92.2  | 94.0 | 96.0                               |     |        | _   |
| All Other Paving                       | 91.2  | 94.0 | 96.0                               | -   |        | _   |
| % of Control Strip<br>Target Density   | —   | —    | —                                  | 98  | 100    | 102 |

In the event that a LOT contains mixtures are placed on various roads that require different specification limits listed above, the Interstate-Primary route specification will be used to compute LPF.

#### 4.2.1.2 **Determining Percent Within Limits**

Determine the estimated PWL value for each acceptance characteristic, asphalt binder content, air voids, VMA, and in-place density as follows:

Step 1. Calculate the LOT average,  $X_a$ , and sample standard deviation, s, using the equations below:

Where:

*n* is the number of test results for the LOT.  $X_i$  represents the individual contractor acceptance test results

$$X_{a} = \frac{\sum_{i=1}^{n} X_{i}}{n} \qquad \qquad s = \sqrt{\frac{\sum_{i=1}^{n} (X_{i} - X_{a})^{2}}{n-1}}$$

Step 2.

Calculate the lower specification limit Quality Index,  $Q_L$ , using the equation below:

$$Q_L = \frac{X_a - LSL}{s}$$

<u>Step 3.</u> Calculate the upper specification limit Quality Index,  $Q_U$ , using the equation below:

$$Q_U = \frac{USL - X_a}{s}$$

<u>Step 4.</u> Depending upon the value of *n*, use  $Q_L$  to enter the appropriate table (from Tables 12 through 20), to determine the percentage of the LOT that is above the lower specification limit. This will be called the Lower Percent Within Limits (LPWL). If there is no lower specification limit for a material characteristic, then LPWL = 100.0%.

<u>Step 5.</u> Depending upon the value of *n*, use  $Q_U$  to enter the appropriate table (from Tables 12 through 20) to determine the percentage of the LOT that is below the upper specification limit. This will be called the Upper Percent Within Limits (UPWL). If there is no upper specification limit for a material characteristic, then UPWL = 100.0%.

<u>Step 6.</u> Calculate the total percentage of the LOT that is within the specification limits. This will be called the Total Percent Within Limits (TPWL) and is calculated using the equation below:

$$TPWL = (LPWL + UPWL) - 100$$

#### 4.2.1.3 Pay Factors

If the TPWL is 20 or less for any one acceptance characteristic, or 40 or less for any 2 acceptance characteristics, or 60 or less for any 3 or more acceptance characteristics remove and replace the mixture representing that LOT.

Determine, by using the equation below, an individual percent pay factor, *PF*, for each of the individual material characteristics if the TPWL for each of the individual material characteristics (asphalt content, air voids, VMA, and in-place density) is appropriate to leave in place, and if no one TPWL is less than 80. If any one individual material characteristics cannot be more than **100 percent.** LOTS with TPWL greater than 90 will receive pay factors greater than 100 percent. The maximum pay factor is 105 percent.

$$PF = 55 + 0.5(TPWL)$$

For Base Courses and Surface Course Type D, base the pay factor for in-place density on percent of the target density. The payment schedule is shown in Table 8.

| Average Percent of Target Control Strip<br>Density | Pay Factor                   |  |
|--|------------------------------|--|
| Greater than 102.0                                 | 97                           |  |
| 98.0-102.0   | 100                          |  |
| 96.0 - 97.9  | 5 × (Percent Density – 78.0) |  |
| Less than 96.0                                     | 80.0                         |  |

Determine the percent pay factor for the LOT, *LPF*, by multiplying the percent pay factors for asphalt binder content, air voids, VMA, and in-place density by weighted coefficients as shown in the equation below. Carry the percent pay factor for the LOT to the nearest hundredth (0.01) and round to the nearest tenth (0.1). Determine the *LPF* from the following equation:

LPF = 
$$0.30(PF_{AC}) + 0.25(PF_{AV}) + 0.10(PF_{VMA}) + 0.35(PF_{Den})$$

Where:

| LPF   | = Percent pay factor for the LOT                |  |  |
|---|---|--|--|
| PF <sub>AC</sub>                                      | = Percent pay factor for asphalt binder content |  |  |
| PFAV  | = Percent pay factor for air voids              |  |  |
| $PF_{VMA}$  | = Percent pay factor for VMA.                   |  |  |
| $PF_{Den}$ = Percent pay factor for in-place density. |   |  |  |

When Base Courses are produced, determine the pay factors by computing a pay factor for asphalt binder content, gradation, and density. Determine the pay for asphalt binder content in accordance to Subsection 4.2.1.2 and the pay factor for gradation by using Table 9.

 Table 9. Pay Factor for Gradations

 (Base Courses, Shoulder Widening Course, Surface Type E, and OGFC only)

| Number of out of tolerance<br>gradations per LOT | Pay Factor<br>(PF <sub>GRAD</sub> ) |
|--|-------------------------------------|
| 0  | 100                                 |
| 1  | 90                                  |
| 2  | 75                                  |
| 3 or more  | 50                                  |

LPF = 
$$0.30(PF_{AC}) + 0.35(PF_{GRAD}) + 0.35(PF_{Den})$$

Where:

 $PF_{GRAD}$  = Percent pay factor for Gradation (see Table 9)

When Shoulder Widening Course, Surface Course Type E, and Open Graded Friction Courses are produced, compute the pay factors by using a pay factor for asphalt binder content, and gradation. Determine the pay for asphalt binder content by Subsection 4.2.1.2 and the pay factor for gradation by using Table 9.

LPF =  $0.50(PF_{AC}) + 0.50(PF_{GRAD})$ 

Base any reductions or increases in payment that are necessary on the original contract unit bid price per ton of asphalt concrete mixture. The total amount of any reduction or increase in payment will be in the form of a lump sum deducted from or added to the monies due.

#### 5. Acceptance of Low Tonnage Paving

Use this acceptance procedure when there are 2500 tons or less of a specific HMA mixture on a project or when the specific HMA mixture is to be used for non-mainline work, such as patching, leveling, widening less than 8-foot, wedging and driveway paving. Evaluate all materials used for low tonnage paving for acceptance by the Department's Acceptance Procedures specified herein. The Department will utilize results from the Contractor's acceptance testing when determining the acceptability of the materials. In addition, the Department will conduct limited testing and monitor and observe the Contractor's sampling and testing procedures to verify the data used for acceptance purposes. The Department's data will be compared with data from the Contractor's acceptance testing program as described in Subsection 3.8, "Split Test Sample

Program" and Subsection 3.9, "Verification Program." Conduct acceptance test sampling and testing on a random basis according to frequencies indicated in Subsection 3.6, "Acceptance Program."

Base the acceptance and pay factors for low tonnage for asphalt binder content and the volumetric properties of air voids and VMA on the difference from the target value for each acceptance characteristic. Perform at least one series of required plant acceptance tests in accordance to Table 3 per LOT where a LOT is defined as a day's production. Notify the Department at least one day prior to any production in order to make necessary arrangements for verification. Failure to do so could result in no payment for that given day's production.

Record all inspections and test results on approved forms and charts and keep up to date records that are available at all times to the Department during the performance of the work. Utilize only those tests designated in advance as acceptance tests in the computation of pay factors. Record test results on forms provided by the Department. The Department will prepare and distribute uniform forms for reproduction for use as required. Deliver, either in person, email or fax all test results necessary to calculate payment factors to the **DAM** no later than 3 working days after the completion of the LOT, or production may be halted by the **DAM** until results are delivered. Provide a copy of each truck ticket printout with the corresponding plant acceptance test results.

#### 5.1 Mixture

Evaluate the HMA mixture at the plant, with respect to asphalt binder content and to the air voids, VMA and/or in-place density, on a LOT-to-LOT basis. Test the material for acceptance in accordance with the provisions of these special provisions. Reject any load or loads of mixture, which, in the opinion of the Department's certified roadway technician, are obviously contaminated, segregated, or otherwise unacceptable for use in the work.

#### 5.1.1 Low-tonnage production

Base the acceptance and pay factors for asphalt binder content and the volumetric properties of air voids and VMA on the percentage of the LOT that is within the specification limits based on the Quality Index calculated using the test results from the LOT when more than 3 SUBLOTS are produced in a day. If less than 3 SUBLOTS are produced in a day, base the acceptance and pay factors for asphalt binder content and the volumetric properties of air voids and VMA on the absolute average difference (AAD) from the target value for each acceptance characteristic.

Therefore, in accordance to Table 3, if 3 or more (n=3 or more) tests are obtained from a given LOT, calculate the Quality Index on the results of the tests in accordance with Subsection 4.2.1.2, "Determining Percent Within Limits" and use Subsection 4.2.1.3 "Pay Factors" to calculate payment. Payments computed with 3 or more tests are calculated using PWL, and will eligible for incentive payment. However, when operational conditions are such that fewer than 3 tests are obtained from the production on a given day, follow the procedure in the next paragraph.

If the number of tests obtained from the day's production is less than 3 (n=1 or n=2), determine pay factors for asphalt binder content, air voids, and VMA based on the average absolute difference (*AAD*) between the acceptance test results from the LOT and the acceptance target values in accordance to Subsection 5.2.1 "Determining Average Absolute Difference," and compute the pay factor in accordance with Subsection 5.2.2, "Pay Factors."

Perform at least one series of required plant acceptance tests per LOT no matter how many tons of a particular mixture is produced in a day and follow the requirements according to the sampling and test methods in Table 3.

#### 5.1.2 In-Place Density

5.1.2.1 Intermediate Courses and Surface Courses Type A, B, and CM

Evaluate the in-place density for Intermediate courses and for Surface courses Type A, B, and CM on a LOT-to-LOT basis. If the number of linear feet in the LOT is less than 1,500, no cores are required. Compute the LOT payment in accordance with Subsection 5.2.2.2. If the number of linear feet is greater than 1500, subdivide the LOT into 3 separate SUBLOTS and obtain cores in accordance to **SC-T-101**. Compute the payment in accordance with Subsection 5.2.2.1.

Express the in-place density as a percentage of the theoretical maximum mix density. Calculate the theoretical maximum density from the maximum specific gravity as determined by **SC-T-83**. The maximum specific gravity used shall be the average of the maximum specific gravity results of the LOT using Contractor data. Carry calculations for density to the hundredths (0.01) and round to the nearest tenth (0.1) in accordance with **ASTM E29** rules of rounding.

#### 5.1.2.2 Base Courses and Surface Courses Type C and D

Evaluate Base Courses and Surface Courses Type C and D on a LOT-to-LOT basis. The inplace density shall be based on density values determined by the use of an approved density gauge, and on a target density established on control strips constructed in accordance with **SC-T-65**. One control strip shall be constructed at the beginning of work on each roadway or shoulder course, and on each lift of each course. An additional control strip shall be constructed when a change is made in the type or source of materials or compaction equipment, or whenever a significant change occurs in the composition of the underlying pavement structure or the composition of the material being placed from the same source.

5.1.2.3 Surface Course Type E and Open Graded Friction Course

Surface Course Type E and OGFC will not have in-place density performed. Place these mixtures at the proper rate and promptly roll with at least 2 passes of a tandem steel wheel roller. Cease rolling as soon as the mixture is properly seated to the underlying surface.

5.1.2.4 Acceptance Plan

It is the intent of these specifications that each LOT meets specification requirements at the time of initial evaluation. No re-sampling or retesting (other than referee testing described in Subsection 3.6, "Verification Program") will be allowed.

Adjust the payment for each LOT on the basis of acceptance test results in accordance with the requirements of these specifications. Keep accurate records of the tonnage of HMA in each LOT. Determine pay factors as indicated below.

#### 5.2.1 Determining Average Absolute Difference

Determine the *AAD* from the target value for each acceptance characteristic, asphalt binder content, air voids, and VMA, as follows:

<u>Step 1.</u> For each acceptance property, calculate the absolute difference,  $D_i$ , between each Contractor acceptance test result,  $X_i$ , and the target value, T, from the equation below that gives a positive value for  $D_i$ :

$$D_i = X_i - T$$
 or  $D_i = T - X_i$ 

<u>Step 2.</u> For each acceptance property, calculate the average absolute difference,  $AAD_{j}$ , using the absolute differences,  $D_{i}$ , calculated in Step 1, from the following equation:

$$AAD_{j} = \frac{\sum_{i=1}^{n} D_{i}}{n}$$

Where: *n* is the number of test results for the LOT.

#### 5.2.2 Pay Factors

Determine an individual pay factor, *PF*, for each acceptance property, asphalt binder content, air voids, and VMA in accordance to Subsection 5.1 "Mixture." Remove and replace any mixture having a property pay factor below 80 percent.

| Property       |              | PF  | Average Absolute Difference<br>from Target<br>Number of Tests |           |
|----------------|--------------|-----|---|-----------|
|                | 1            | 400 | 1   | 2         |
|                |              | 100 | 0.00-0.36   | 0.00-0.28 |
|                | Surface      | 95  | 0.37-0.44   | 0.29-0.36 |
|                | Guilace      | 90  | 0.45-0.55   | 0.37-0.43 |
|                |              | 80  | 0.56-0.66   | 0.44-0.51 |
| Binder Content |              | 100 | 0.00-0.43   | 0.00-0.33 |
| Binder Content | Intermediate | 95  | 0.44-0.52   | 0.34-0.42 |
|                |              | 90  | 0.53-0.65   | 0.43-0.51 |
|                |              | 80  | 0.66-0.78   | 0.52-0.60 |
|                |              | 100 | 0.00-0.50   | 0.00-0.38 |
|                | Base         | 95  | 0.51-0.65   | 0.39-0.49 |
|                | ваѕе         | 90  | 0.66-0.75   | 0.50-0.59 |
|                |              | 80  | 0.76-0.90   | 0.60-0.69 |
|                |              | 100 | 0.00-1.15   | 0.00-0.89 |
| Air Voids &    | Surface and  | 95  | 1.16-1.40   | 0.90-1.14 |
| VMA            | Intermediate | 90  | 1.41-1.75   | 1.15-1.36 |
|                |              | 80  | 1.76-2.10   | 1.37-1.61 |

#### Table 10. Pay Factors for Non Mainline Paving LOTS

#### 5.2.2.1 Density LOTS

Determine the percent pay factor for the LOT, *LPF*, by multiplying the percent pay factors for asphalt binder content, air voids, VMA, and in-place density by weighted coefficients as shown in the equation below. Carry the percent pay factor for the LOT to the nearest hundredth (0.01) and round to the nearest tenth (0.1). Use the following equation to determine the *LPF*:

LPF = 
$$0.30(PF_{AC}) + 0.25(PF_{AV}) + 0.10(PF_{VMA}) + 0.35(PF_{Den})$$

Where:

| 0.         |   |
|------------|---|
| LPF        | = Percent pay factor for the LOT                |
| $PF_{AC}$  | = Percent pay factor for asphalt binder content |
| $PF_{AV}$  | = Percent pay factor for air voids              |
| $PF_{VMA}$ | = Percent pay factor for VMA.                   |
| $PF_{Den}$ | = Percent pay factor for Density.               |
|            |   |

When Base courses are produced, determine pay factors by computing a pay factor for asphalt binder content, gradation and density. Use Subsection 5.1 "Mixture" to determine the pay for asphalt binder content and Table 9 to determine the pay factor for gradation.

LPF = 
$$0.35(PF_{AC}) + 0.30(PF_{GRAD}) + 0.35(PF_{Den})$$

Where:

 $PF_{GRAD}$  = Percent pay factor for Gradation (see Table 9)

Base any reductions or increases in payment that are necessary on the original contract unit bid price per ton of asphalt concrete mixture. The total amount of any reduction or increase in payment will be in the form of a lump sum deducted from or added to the monies due.

#### 5.2.2.2 Non-Density LOTS

Determine the percent pay factor for the LOT, *LPF*, by multiplying the percent pay factors for asphalt binder content, air voids, and VMA by weighted coefficients as shown in the equation below. Carry the percent pay factor for the LOT to the nearest hundredth (0.01) and round to the nearest tenth (0.1). Use the following equation to determine the *LPF*:

LPF = 
$$0.45(PF_{AC}) + 0.45(PF_{AV}) + 0.10(PF_{VMA})$$

When Base Courses, Surface Course Type E, and/or Open Graded Friction Courses are produced, determine the LPF by computing a pay factor for asphalt binder content and gradation. Use Subsection 5.1 "Mixture" to determine the pay for asphalt binder content and Table 9 to determine the pay factor for gradation.

LPF = 
$$0.50(PF_{AC}) + 0.50(PF_{GRAD})$$

Base any reductions or increases in payment that are necessary on the original contract unit bid price per ton of asphalt concrete mixture. The total amount of any reduction or increase in payment will be in the form of a lump sum deducted from or added to the monies due.

| 1.152 or More100 $-0.039 \text{ to} 0.000$ 501.149 to 1.15199 $-0.069 \text{ to} -0.040$ 491.144 to 1.14497 $-0.139 \text{ to} -0.070$ 481.141 to 1.14497 $-0.139 \text{ to} -0.110$ 471.138 to 1.14096 $-0.179 \text{ to} -0.140$ 461.134 to 1.13795 $-0.219 \text{ to} -0.180$ 451.127 to 1.13394 $-0.249 \text{ to} -0.220$ 441.118 to 1.12693 $-0.289 \text{ to} -0.250$ 431.111 to 1.12693 $-0.289 \text{ to} -0.250$ 431.111 to 1.11091 $-0.359 \text{ to} -0.320$ 411.091 to 1.10090 $-0.389 \text{ to} -0.360$ 401.071 to 1.00088 $-0.459 \text{ to} -0.430$ 381.041 to 1.09087 $-0.489 \text{ to} -0.490$ 361.011 to 1.01084 $-0.519 \text{ to} -0.490$ 361.011 to 1.01084 $-0.569 \text{ to} -0.520$ 351.001 to 1.01084 $-0.619 \text{ to} -0.660$ 310.971 to 1.00083 $-0.649 \text{ to} -0.620$ 320.931 to 0.96081 $-0.679 \text{ to} -0.660$ 310.911 to 0.82075 $-0.839 \text{ to} -0.710$ 290.871 to 0.80077 $-0.789 \text{ to} -0.740$ 280.841 to 0.87077 $-0.789 \text{ to} -0.740$ 280.841 to 0.70073 $-0.689 \text{ to} -0.800$ 250.711 to 0.74072 $-0.990 \text{ to} -0.890$ 250.741 to 0.75073 $-0.889 \text{ to} -0.760$ 27 <th><math>Q_L \text{ or } Q_U</math></th> <th>2. Estimate of LPWL or<br/>LPWL or UPWL</th> <th><math>Q_L \text{ or } Q_U</math></th> <th>LPWL or UPWL</th> | $Q_L \text{ or } Q_U$ | 2. Estimate of LPWL or<br>LPWL or UPWL | $Q_L \text{ or } Q_U$ | LPWL or UPWL |
|--|-----------------------|--|-----------------------|--------------|
| $\begin{array}{c c c c c c c c c c c c c c c c c c c $   | -                     |  | -                     |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       |  |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       |  |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 1.145 to 1.148        |  | -0.109 to -0.070      |              |
| 1.134 to $1.137$ $95$ $-0.219$ to $-0.180$ $45$ $1.127$ to $1.133$ $94$ $-0.249$ to $-0.220$ $44$ $1.118$ to $1.126$ $93$ $-0.289$ to $-0.250$ $43$ $1.111$ to $1.117$ $92$ $-0.319$ to $-0.290$ $42$ $1.101$ to $1.110$ $91$ $-0.359$ to $-0.320$ $41$ $1.091$ to $1.000$ $90$ $-0.389$ to $-0.320$ $41$ $1.091$ to $1.000$ $89$ $-0.429$ to $-0.390$ $39$ $1.061$ to $1.070$ $88$ $-0.459$ to $-0.430$ $38$ $1.041$ to $1.060$ $87$ $-0.489$ to $-0.460$ $37$ $1.031$ to $1.040$ $86$ $-0.519$ to $-0.60$ $34$ $1.011$ to $1.000$ $85$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.000$ $83$ $-0.619$ to $-0.620$ $32$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.620$ $32$ $0.931$ to $0.900$ $78$ $-0.759$ to $-0.740$ $28$ $0.871$ to $0.890$ $78$ $-0.759$ to $-0.740$ $28$ $0.811$ to $0.800$ $76$ $-0.819$ to $0.740$ $24$ $0.771$ to $0.789$ to $0.740$ $23$ $-0.779$ $0.821$ to $0.800$ $75$ $-0.839$ to $0.820$ $25$ $0.761$ to <td></td> <td>97</td> <td>-0.139 to -0.110</td> <td>47</td>  |                       | 97                                     | -0.139 to -0.110      | 47           |
| 1.127 to $1.133$ $94$ $-0.249$ to $-0.220$ $44$ $1.118$ to $1.126$ $93$ $-0.289$ to $-0.250$ $43$ $1.111$ to $1.117$ $92$ $-0.319$ to $-0.290$ $42$ $1.101$ to $1.110$ $91$ $-0.359$ to $-0.320$ $41$ $1.091$ to $1.000$ $90$ $-0.389$ to $-0.360$ $40$ $1.071$ to $1.090$ $89$ $-0.429$ to $-0.390$ $39$ $1.061$ to $1.070$ $88$ $-0.459$ to $-0.430$ $38$ $1.041$ to $1.060$ $87$ $-0.489$ to $-0.460$ $37$ $1.031$ to $1.040$ $86$ $-0.519$ to $-0.430$ $38$ $1.041$ to $1.040$ $86$ $-0.559$ to $-0.520$ $35$ $1.011$ to $1.040$ $86$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.040$ $86$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.000$ $83$ $-0.619$ to $-0.620$ $32$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.680$ $30$ $0.971$ to $0.970$ $82$ $-0.649$ to $-0.70$ $22$ $0.941$ to $0.960$ $81$ $-0.790$ to $-0.790$ to $-0.790$ to $0.911$ to $0.930$ $80$ $-0.759$ to $-0.740$ $28$ $0.841$ to $0.870$ $77$ $-0.789$ to $-0.790$ $26$   | 1.138 to 1.140        | 96                                     | -0.179 to -0.140      | 46           |
| 1.118  to 1.126 $93$ $-0.289  to -0.250$ $43$ $1.111  to 1.117$ $92$ $-0.319  to -0.290$ $42$ $1.001  to 1.100$ $90$ $-0.389  to -0.320$ $41$ $1.091  to 1.100$ $90$ $-0.389  to -0.390$ $39$ $1.071  to 1.090$ $89$ $-0.429  to -0.430$ $38$ $1.041  to 1.070$ $88$ $-0.459  to -0.430$ $38$ $1.041  to 1.060$ $87$ $-0.489  to -0.460$ $37$ $1.031  to 1.040$ $86$ $-0.519  to -0.490$ $36$ $1.011  to 1.030$ $85$ $-0.559  to -0.520$ $35$ $1.001  to 1.010$ $84$ $-0.589  to -0.560$ $34$ $0.971  to 1.000$ $83$ $-0.619  to -0.590$ $33$ $0.961  to 0.970$ $82$ $-0.649  to -0.620$ $32$ $0.931  to 0.960$ $81$ $-0.679  to -0.680$ $30$ $0.991  to 0.930$ $80$ $-0.799  to -0.710$ $29$ $0.871  to 0.890$ $78$ $-0.759  to -0.740$ $28$ $0.841  to 0.870$ $77$ $-0.839  to -0.840$ $24$ $0.711  to 0.820$ $75$ $-0.839  to -0.840$ $24$ $0.741  to 0.760$ $73$ $-0.889  to -0.870$ $23$ $0.621  to 0.660$ $70$ $-0.999  to -0.930$ $20$ $0.621  to 0.650$ $69$ $-0.999  to -0.970$ $18$ $0.591  to 0.620$ $68$ $-0.999  to -0.970$ $18$ $0.561  to 0.590$ $67$ <   | 1.134 to 1.137        | 95                                     | -0.219 to -0.180      | 45           |
| 1.111 to 1.11792 $-0.319$ to $-0.290$ 421.101 to 1.11091 $-0.359$ to $-0.320$ 411.091 to 1.10090 $-0.389$ to $-0.320$ 401.071 to 1.09089 $-0.429$ to $-0.390$ 391.061 to 1.07088 $-0.459$ to $-0.430$ 381.041 to 1.06087 $-0.489$ to $-0.460$ 371.031 to 1.04086 $-0.519$ to $-0.490$ 361.011 to 1.03085 $-0.559$ to $-0.520$ 351.001 to 1.01084 $-0.589$ to $-0.500$ 34 $0.971$ to 1.00083 $-0.619$ to $-0.620$ 320.961 to 0.97082 $-0.649$ to $-0.620$ 320.931 to 0.96081 $-0.679$ to $-0.680$ 300.991 to 0.91079 $-0.739$ to $-0.710$ 290.871 to 0.89078 $-0.759$ to $-0.740$ 280.841 to 0.87077 $-0.789$ to $-0.790$ 260.791 to 0.82075 $-0.839$ to $-0.870$ 230.711 to 0.74072 $-0.990$ to $-0.890$ 220.741 to 0.76073 $-0.890$ to $-0.930$ 200.621 to 0.65069 $-0.999$ to $-0.930$ 200.621 to 0.65069 $-0.999$ to $-0.930$ 200.621 to 0.65069 $-0.999$ to $-0.970$ 180.591 to 0.62065 $-1.039$ to $-1.000$ 170.521 to 0.56066 $-1.029$ to $-1.040$ 140.431 to 0.46063 $-1.069$ to $-1.060$ 13  | 1.127 to 1.133        | 94                                     | -0.249 to -0.220      | 44           |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 1.118 to 1.126        | 93                                     | -0.289 to -0.250      | 43           |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 1.111 to 1.117        | 92                                     | -0.319 to -0.290      | 42           |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 1.101 to 1.110        | 91                                     | -0.359 to -0.320      | 41           |
| 1.061 to $1.070$ $88$ $-0.459$ to $-0.430$ $38$ $1.041$ to $1.060$ $87$ $-0.489$ to $-0.460$ $37$ $1.031$ to $1.040$ $86$ $-0.519$ to $-0.490$ $36$ $1.011$ to $1.030$ $85$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.010$ $84$ $-0.689$ to $-0.560$ $34$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.590$ $33$ $0.961$ to $0.970$ $82$ $-0.649$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.650$ $31$ $0.911$ to $0.930$ $80$ $-0.799$ to $-0.680$ $30$ $0.891$ to $0.910$ $79$ $-0.739$ to $-0.710$ $29$ $0.871$ to $0.890$ $78$ $-0.759$ to $-0.740$ $28$ $0.841$ to $0.870$ $77$ $-0.789$ to $-0.760$ $27$ $0.821$ to $0.840$ $76$ $-0.819$ to $-0.790$ $26$ $0.791$ to $0.820$ $75$ $-0.839$ to $-0.820$ $25$ $0.761$ to $0.790$ $74$ $-0.869$ to $-0.840$ $24$ $0.741$ to $0.760$ $73$ $-0.889$ to $-0.870$ $23$ $0.711$ to $0.740$ $72$ $-0.909$ to $-0.900$ $21$ $0.651$ to $0.650$ $69$ $-0.959$ to $-0.960$ $19$ $0.591$ to $0.650$ $66$ $-1.029$ to $-1.000$ $17$ $0.521$ to $0.560$ $66$ $-1.029$ to $-1.000$ $17$ $0.521$ to $0.560$ $66$ $-1.029$ to $-1.030$ $15$ $0.461$ to $0.490$ $64$ $-1.059$ to $-1.040$ $14$ $0.431$ to $0.460$   | 1.091 to 1.100        | 90                                     | -0.389 to -0.360      | 40           |
| 1.041 to 1.06087-0.489 to -0.460371.031 to 1.04086-0.519 to -0.490361.011 to 1.03085-0.559 to -0.520351.001 to 1.01084-0.589 to -0.560340.971 to 1.00083-0.619 to -0.590330.961 to 0.97082-0.649 to -0.620320.931 to 0.96081-0.679 to -0.650310.911 to 0.93080-0.709 to -0.680300.891 to 0.91079-0.739 to -0.710290.871 to 0.89078-0.759 to -0.740280.841 to 0.87077-0.789 to -0.760270.821 to 0.84076-0.819 to -0.790260.791 to 0.82075-0.839 to -0.840240.741 to 0.76073-0.869 to -0.840240.741 to 0.76073-0.899 to -0.910210.651 to 0.68070-0.999 to -0.930200.651 to 0.65069-0.909 to -0.900190.591 to 0.62068-0.999 to -0.970180.561 to 0.59067-1.009 to -1.000170.521 to 0.56066-1.029 to -1.010160.491 to 0.52065-1.039 to -1.030150.461 to 0.49064-1.059 to -1.040140.431 to 0.46063-1.069 to -1.06013   | 1.071 to 1.090        | 89                                     | -0.429 to -0.390      | 39           |
| 1.031 to $1.040$ $86$ $-0.519$ to $-0.490$ $36$ $1.011$ to $1.030$ $85$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.010$ $84$ $-0.589$ to $-0.560$ $34$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.590$ $33$ $0.961$ to $0.970$ $82$ $-0.649$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.650$ $31$ $0.911$ to $0.930$ $80$ $-0.709$ to $-0.680$ $30$ $0.891$ to $0.910$ $79$ $-0.739$ to $-0.710$ $29$ $0.871$ to $0.890$ $78$ $-0.759$ to $-0.740$ $28$ $0.841$ to $0.870$ $77$ $-0.789$ to $-0.760$ $27$ $0.821$ to $0.840$ $76$ $-0.819$ to $-0.790$ $26$ $0.791$ to $0.820$ $75$ $-0.839$ to $-0.820$ $25$ $0.761$ to $0.790$ $74$ $-0.869$ to $-0.840$ $24$ $0.741$ to $0.760$ $73$ $-0.890$ to $-0.900$ $23$ $0.681$ to $0.710$ $71$ $-0.929$ to $-0.910$ $21$ $0.651$ to $0.680$ $70$ $-0.959$ to $-0.930$ $20$ $0.621$ to $0.650$ $69$ $-0.999$ to $-0.900$ $19$ $0.591$ to $0.620$ $68$ $-0.999$ to $-0.970$ $18$ $0.561$ to $0.590$ $67$ $-1.009$ to $-1.000$ $17$ $0.521$ to $0.560$ $66$ $-1.029$ to $-1.010$ $16$ $0.491$ to $0.520$ $65$ $-1.039$ to $-1.040$ $14$ $0.431$ to $0.460$ $63$ $-1.069$ to $-1.060$ $13$  | 1.061 to 1.070        | 88                                     | -0.459 to -0.430      | 38           |
| 1.031 to $1.040$ $86$ $-0.519$ to $-0.490$ $36$ $1.011$ to $1.030$ $85$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.010$ $84$ $-0.589$ to $-0.560$ $34$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.590$ $33$ $0.961$ to $0.970$ $82$ $-0.649$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.680$ $31$ $0.911$ to $0.930$ $80$ $-0.709$ to $-0.680$ $30$ $0.891$ to $0.910$ $79$ $-0.739$ to $-0.710$ $29$ $0.871$ to $0.890$ $78$ $-0.759$ to $-0.740$ $28$ $0.841$ to $0.870$ $77$ $-0.789$ to $-0.760$ $27$ $0.821$ to $0.840$ $76$ $-0.819$ to $-0.790$ $26$ $0.791$ to $0.820$ $75$ $-0.839$ to $-0.820$ $25$ $0.761$ to $0.790$ $74$ $-0.869$ to $-0.840$ $24$ $0.741$ to $0.760$ $73$ $-0.890$ to $-0.900$ $23$ $0.681$ to $0.710$ $71$ $-0.929$ to $-0.910$ $21$ $0.651$ to $0.680$ $70$ $-0.959$ to $-0.930$ $20$ $0.621$ to $0.650$ $69$ $-0.999$ to $-0.900$ $19$ $0.591$ to $0.620$ $68$ $-0.999$ to $-0.970$ $18$ $0.561$ to $0.590$ $67$ $-1.009$ to $-1.000$ $17$ $0.521$ to $0.560$ $66$ $-1.029$ to $-1.010$ $16$ $0.491$ to $0.520$ $65$ $-1.039$ to $-1.040$ $14$ $0.431$ to $0.460$ $63$ $-1.069$ to $-1.060$ $13$  |                       | 87                                     |                       | 37           |
| 1.011 to $1.030$ $85$ $-0.559$ to $-0.520$ $35$ $1.001$ to $1.010$ $84$ $-0.589$ to $-0.560$ $34$ $0.971$ to $1.000$ $83$ $-0.619$ to $-0.590$ $33$ $0.961$ to $0.970$ $82$ $-0.649$ to $-0.620$ $32$ $0.931$ to $0.960$ $81$ $-0.679$ to $-0.650$ $31$ $0.911$ to $0.930$ $80$ $-0.709$ to $-0.680$ $30$ $0.891$ to $0.910$ $79$ $-0.739$ to $-0.710$ $29$ $0.871$ to $0.890$ $78$ $-0.759$ to $-0.740$ $28$ $0.841$ to $0.870$ $77$ $-0.789$ to $-0.760$ $27$ $0.821$ to $0.840$ $76$ $-0.819$ to $-0.790$ $26$ $0.791$ to $0.820$ $75$ $-0.839$ to $-0.820$ $25$ $0.761$ to $0.790$ $74$ $-0.869$ to $-0.840$ $24$ $0.741$ to $0.760$ $73$ $-0.899$ to $-0.930$ $22$ $0.681$ to $0.710$ $71$ $-0.929$ to $-0.910$ $21$ $0.651$ to $0.680$ $70$ $-0.929$ to $-0.930$ $20$ $0.621$ to $0.650$ $69$ $-0.999$ to $-0.970$ $18$ $0.561$ to $0.590$ $67$ $-1.009$ to $-1.000$ $17$ $0.521$ to $0.560$ $66$ $-1.029$ to $-1.010$ $16$ $0.461$ to $0.490$ $64$ $-1.059$ to $-1.040$ $14$  |                       | 86                                     |                       | 36           |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       |  |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       | -                                      |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       | -                                      |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       |  |                       |              |
| 0.741 to 0.760         73         -0.889 to -0.870         23           0.711 to 0.740         72         -0.909 to -0.890         22           0.681 to 0.710         71         -0.929 to -0.910         21           0.651 to 0.680         70         -0.959 to -0.930         20           0.621 to 0.650         69         -0.969 to -0.960         19           0.591 to 0.620         68         -0.999 to -0.970         18           0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |                       |  |                       |              |
| 0.681 to 0.710         71         -0.929 to -0.910         21           0.651 to 0.680         70         -0.959 to -0.930         20           0.621 to 0.650         69         -0.969 to -0.960         19           0.591 to 0.620         68         -0.999 to -0.970         18           0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.651 to 0.680         70         -0.959 to -0.930         20           0.621 to 0.650         69         -0.969 to -0.960         19           0.591 to 0.620         68         -0.999 to -0.970         18           0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.621 to 0.650         69         -0.969 to -0.960         19           0.591 to 0.620         68         -0.999 to -0.970         18           0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.591 to 0.620         68         -0.999 to -0.970         18           0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.561 to 0.590         67         -1.009 to -1.000         17           0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.521 to 0.560         66         -1.029 to -1.010         16           0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.491 to 0.520         65         -1.039 to -1.030         15           0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.461 to 0.490         64         -1.059 to -1.040         14           0.431 to 0.460         63         -1.069 to -1.060         13  |                       |  |                       |              |
| 0.431 to 0.460 63 -1.069 to -1.060 13  |                       |  |                       |              |
|  |                       |  |                       |              |
|  |                       |  |                       |              |
| 0.391 to 0.430 62 -1.089 to -1.070 12  |                       |  |                       |              |
| 0.361 to 0.390 61 -1.099 to -1.090 11  |                       |  |                       |              |
| 0.321 to 0.360 60 -1.109 to -1.100 10  |                       |  |                       |              |
| 0.291 to 0.320 59 -1.116 to -1.110 9   |                       |  |                       |              |
| 0.251 to 0.290 58 -1.125 to -1.117 8   |                       |  |                       |              |
| 0.221 to 0.250 57 -1.132 to -1.126 7   |                       | -                                      |                       |              |
| 0.181 to 0.220 56 -1.136 to -1.133 6   |                       |  |                       |              |
| 0.141 to 0.180 55 -1.139 to -1.137 5   |                       |  |                       |              |
| 0.111 to 0.140 54 -1.143 to -1.140 4   |                       |  |                       |              |
| 0.071 to 0.110 53 -1.147 to -1.144 3   |                       |  | -1.147 to -1.144      |              |
| 0.041 to 0.070 52 -1.150 to -1.148 2   | 0.041 to 0.070        | 52                                     | -1.150 to -1.148      | 2            |
| 0.001 to 0.040 51 -1.159 to -1.151 1   | 0.001 to 0.040        |  | -1.159 to -1.151      | 1            |
| -0.039 to 0.000 50 -1.160 or Less 0  | -0.039 to 0.000       | 50                                     | -1.160 or Less        | 0            |

Table 12. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 3.

|                       | 3. Estimate of LPWL or |                  |    |
|-----------------------|------------------------|------------------|----|
| $Q_L \text{ or } Q_U$ | LPWL or UPWL           | $Q_L$ or $Q_U$   |    |
| 1.471 or More         | 100                    | -0.029 to 0.000  | 50 |
| 1.441 to 1.470        | 99                     | -0.059 to -0.030 | 49 |
| 1.411 to 1.440        | 98                     | -0.089 to -0.060 | 48 |
| 1.381 to 1.410        | 97                     | -0.119 to -0.090 | 47 |
| 1.351 to 1.380        | 96                     | -0.149 to -0.120 | 46 |
| 1.321 to 1.350        | 95                     | -0.179 to -0.150 | 45 |
| 1.291 to 1.320        | 94                     | -0.209 to -0.180 | 44 |
| 1.261 to 1.290        | 93                     | -0.239 to -0.210 | 43 |
| 1.231 to 1.260        | 92                     | -0.269 to -0.240 | 42 |
| 1.201 to 1.230        | 91                     | -0.299 to -0.270 | 41 |
| 1.171 to 1.200        | 90                     | -0.329 to -0.300 | 40 |
| 1.141 to 1.170        | 89                     | -0.359 to -0.330 | 39 |
| 1.111 to 1.140        | 88                     | -0.389 to -0.360 | 38 |
| 1.081 to 1.110        | 87                     | -0.419 to -0.390 | 37 |
| 1.051 to 1.080        | 86                     | -0.449 to -0.420 | 36 |
| 1.021 to 1.050        | 85                     | -0.479 to -0.450 | 35 |
| 0.991 to 1.020        | 84                     | -0.509 to -0.480 | 34 |
| 0.961 to 0.990        | 83                     | -0.539 to -0.510 | 33 |
| 0.931 to 0.960        | 82                     | -0.569 to -0.540 | 32 |
| 0.901 to 0.930        | 81                     | -0.599 to -0.570 | 31 |
| 0.871 to 0.900        | 80                     | -0.629 to -0.600 | 30 |
| 0.841 to 0.870        | 79                     | -0.659 to -0.630 | 29 |
| 0.811 to 0.840        | 78                     | -0.689 to -0.660 | 28 |
| 0.781 to 0.810        | 77                     | -0.719 to -0.690 | 27 |
| 0.751 to 0.780        | 76                     | -0.749 to -0.720 | 26 |
| 0.721 to 0.750        | 75                     | -0.779 to -0.750 | 25 |
| 0.691 to 0.720        | 74                     | -0.809 to -0.780 | 24 |
| 0.661 to 0.690        | 73                     | -0.839 to -0.810 | 23 |
| 0.631 to 0.660        | 72                     | -0.869 to -0.840 | 22 |
| 0.601 to 0.630        | 71                     | -0.899 to -0.870 | 21 |
| 0.571 to 0.600        | 70                     | -0.929 to -0.900 | 20 |
| 0.541 to 0.570        | 69                     | -0.959 to -0.930 | 19 |
| 0.511 to 0.540        | 68                     | -0.989 to -0.960 | 18 |
| 0.481 to 0.510        | 67                     | -1.019 to -0.990 | 17 |
| 0.451 to 0.480        | 66                     | -1.049 to -1.020 | 16 |
| 0.421 to 0.450        | 65                     | -1.079 to -1.050 | 15 |
| 0.391 to 0.420        | 64                     | -1.109 to -1.080 | 14 |
| 0.361 to 0.390        | 63                     | -1.139 to -1.110 | 13 |
| 0.331 to 0.360        | 62                     | -1.169 to -1.140 | 12 |
| 0.301 to 0.330        | 61                     | -1.199 to -1.170 | 11 |
| 0.271 to 0.300        | 60                     | -1.229 to -1.200 | 10 |
| 0.241 to 0.270        | 59                     | -1.259 to -1.230 | 9  |
| 0.211 to 0.240        | 58                     | -1.289 to -1.260 | 8  |
| 0.181 to 0.210        | 57                     | -1.319 to -1.290 | 7  |
| 0.151 to 0.180        | 56                     | -1.349 to -1.320 | 6  |
| 0.121 to 0.150        | 55                     | -1.379 to -1.350 | 5  |
| 0.091 to 0.120        | 54                     | -1.409 to -1.380 | 4  |
| 0.061 to 0.090        | 53                     | -1.439 to -1.410 | 3  |
| 0.031 to 0.060        | 52                     | -1.469 to -1.440 | 2  |
| 0.001 to 0.030        | 51                     | -1.499 to -1.470 | 1  |
| -0.029 to 0.000       | 50                     | -1.500 or Less   | 0  |
|                       | 1                      |                  | 1  |

Table 13. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 4.

|                                  | <ol> <li>Estimate of LPWL or</li> </ol> |                                  |              |
|----------------------------------|---|----------------------------------|--------------|
| Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL                            | Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL |
| 1.671 or More                    | 100                                     | -0.029 to 0.000                  | 50           |
| 1.601 to 1.670                   | 99                                      | -0.059 to -0.030                 | 49           |
| 1.541 to 1.600                   | 98                                      | -0.079 to -0.060                 | 48           |
| 1.491 to 1.540                   | 97                                      | -0.109 to -0.080                 | 47           |
| 1.441 to 1.490                   | 96                                      | -0.139 to -0.110                 | 46           |
| 1.391 to 1.440                   | 95                                      | -0.159 to -0.140                 | 45           |
| 1.351 to 1.390                   | 94                                      | -0.199 to -0.160                 | 44           |
| 1.311 to 1.350                   | 93                                      | -0.229 to -0.200                 | 43           |
| 1.271 to 1.310                   | 92                                      | -0.249 to -0.230                 | 42           |
| 1.231 to 1.270                   | 91                                      | -0.279 to -0.250                 | 41           |
| 1.191 to 1.230                   | 90                                      | -0.309 to -0.280                 | 40           |
| 1.151 to 1.190                   | 89                                      | -0.339 to -0.310                 | 39           |
| 1.121 to 1.150                   | 88                                      | -0.369 to -0.340                 | 38           |
| 1.081 to 1.120                   | 87                                      | -0.399 to -0.370                 | 37           |
| 1.051 to 1.080                   | 86                                      | -0.429 to -0.400                 | 36           |
| 1.011 to 1.050                   | 85                                      | -0.449 to -0.430                 | 35           |
| 0.981 to 1.010                   | 84                                      | -0.449 to -0.430                 | 34           |
|                                  | 83                                      |                                  | 33           |
| 0.951 to 0.980                   |   | -0.509 to -0.470                 |              |
| 0.911 to 0.950                   | 82                                      | -0.539 to -0.510                 | 32           |
| 0.881 to 0.910                   | 81                                      | -0.569 to -0.540                 | 31           |
| 0.851 to 0.880                   | 80                                      | -0.599 to -0.570                 | 30           |
| 0.821 to 0.850                   | 79                                      | -0.629 to -0.600                 | 29           |
| 0.781 to 0.820                   | 78                                      | -0.659 to -0.630                 | 28           |
| 0.751 to 0.780                   | 77                                      | -0.689 to -0.660                 | 27           |
| 0.721 to 0.750                   | 76                                      | -0.719 to -0.690                 | 26           |
| 0.691 to 0.720                   | 75                                      | -0.749 to -0.720                 | 25           |
| 0.661 to 0.690                   | 74                                      | -0.779 to -0.750                 | 24           |
| 0.631 to 0.660                   | 73                                      | -0.819 to -0.780                 | 23           |
| 0.601 to 0.630                   | 72                                      | -0.849 to -0.820                 | 22           |
| 0.571 to 0.600                   | 71                                      | -0.879 to -0.850                 | 21           |
| 0.541 to 0.570                   | 70                                      | -0.909 to -0.880                 | 20           |
| 0.511 to 0.540                   | 69                                      | -0.949 to -0.910                 | 19           |
| 0.471 to 0.510                   | 68                                      | -0.979 to -0.950                 | 18           |
| 0.451 to 0.470                   | 67                                      | -1.009 to -0.980                 | 17           |
| 0.431 to 0.450                   | 66                                      | -1.049 to -1.010                 | 16           |
| 0.401 to 0.430                   | 65                                      | -1.079 to -1.050                 | 15           |
| 0.371 to 0.400                   | 64                                      | -1.119 to -1.080                 | 14           |
| 0.341 to 0.370                   | 63                                      | -1.149 to -1.120                 | 13           |
| 0.311 to 0.340                   | 62                                      | -1.189 to -1.150                 | 12           |
| 0.281 to 0.310                   | 61                                      | -1.229 to -1.190                 | 11           |
| 0.251 to 0.280                   | 60                                      | -1.269 to -1.230                 | 10           |
| 0.231 to 0.250                   | 59                                      | -1.309 to -1.270                 | 9            |
| 0.201 to 0.230                   | 58                                      | -1.349 to -1.310                 | 8            |
| 0.161 to 0.200                   | 57                                      | -1.389 to -1.350                 | 7            |
| 0.141 to 0.160                   | 56                                      | -1.439 to -1.390                 | 6            |
| 0.111 to 0.140                   | 55                                      | -1.489 to -1.440                 | 5            |
| 0.081 to 0.110                   | 55                                      | -1.539 to -1.490                 | 4            |
|                                  | 53                                      |                                  | 3            |
| 0.061 to 0.080                   |   | -1.599 to -1.540                 | 2            |
| 0.031 to 0.060                   | 52                                      | -1.669 to -1.600                 |              |
| 0.001 to 0.030                   | 51                                      | -1.789 to -1.670                 | 1            |
| -0.029 to 0.000                  | 50                                      | -1.790 or Less                   | 0            |

Table 14. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 5.

|                       | 5. Estimate of LPWL or |                  |    |
|-----------------------|------------------------|------------------|----|
| $Q_L \text{ or } Q_U$ | LPWL or UPWL           | $Q_L$ or $Q_U$   |    |
| 1.801 or More         | 100                    | -0.029 to 0.000  | 50 |
| 1.701 to 1.800        | 99                     | -0.049 to -0.030 | 49 |
| 1.621 to 1.700        | 98                     | -0.079 to -0.050 | 48 |
| 1.551 to 1.620        | 97                     | -0.109 to -0.080 | 47 |
| 1.491 to 1.550        | 96                     | -0.129 to -0.110 | 46 |
| 1.431 to 1.490        | 95                     | -0.159 to -0.130 | 45 |
| 1.381 to 1.430        | 94                     | -0.189 to -0.160 | 44 |
| 1.331 to 1.380        | 93                     | -0.219 to -0.190 | 43 |
| 1.291 to 1.330        | 92                     | -0.249 to -0.220 | 42 |
| 1.241 to 1.290        | 91                     | -0.269 to -0.250 | 41 |
| 1.201 to 1.240        | 90                     | -0.299 to -0.270 | 40 |
| 1.161 to 1.200        | 89                     | -0.329 to -0.300 | 39 |
| 1.121 to 1.160        | 88                     | -0.359 to -0.330 | 38 |
| 1.081 to 1.120        | 87                     | -0.389 to -0.360 | 37 |
| 1.041 to 1.080        | 86                     | -0.409 to -0.390 | 36 |
| 1.011 to 1.040        | 85                     | -0.439 to -0.410 | 35 |
| 0.971 to 1.010        | 84                     | -0.469 to -0.440 | 34 |
| 0.941 to 0.970        | 83                     | -0.499 to -0.470 | 33 |
| 0.901 to 0.940        | 82                     | -0.529 to -0.500 | 32 |
| 0.871 to 0.900        | 81                     | -0.559 to -0.530 | 31 |
| 0.841 to 0.870        | 80                     | -0.589 to -0.560 | 30 |
| 0.801 to 0.840        | 79                     | -0.619 to -0.590 | 29 |
| 0.771 to 0.800        | 78                     | -0.649 to -0.620 | 28 |
| 0.741 to 0.770        | 77                     | -0.679 to -0.650 | 27 |
| 0.711 to 0.740        | 76                     | -0.709 to -0.680 | 26 |
| 0.681 to 0.710        | 75                     | -0.739 to -0.710 | 25 |
| 0.651 to 0.680        | 74                     | -0.769 to -0.740 | 24 |
| 0.621 to 0.650        | 73                     | -0.799 to -0.770 | 23 |
| 0.591 to 0.620        | 72                     | -0.839 to -0.800 | 22 |
| 0.561 to 0.590        | 71                     | -0.869 to -0.840 | 21 |
| 0.531 to 0.560        | 70                     | -0.899 to -0.870 | 20 |
| 0.501 to 0.530        | 69                     | -0.939 to -0.900 | 19 |
| 0.471 to 0.500        | 68                     | -0.969 to -0.940 | 18 |
| 0.441 to 0.470        | 67                     | -1.009 to -0.970 | 17 |
| 0.411 to 0.440        | 66                     | -1.039 to -1.010 | 16 |
| 0.391 to 0.410        | 65                     | -1.079 to -1.040 | 15 |
| 0.361 to 0.390        | 64                     | -1.119 to -1.080 | 14 |
| 0.331 to 0.360        | 63                     | -1.159 to -1.120 | 13 |
| 0.301 to 0.330        | 62                     | -1.199 to -1.160 | 12 |
| 0.271 to 0.300        | 61                     | -1.239 to -1.200 | 11 |
| 0.251 to 0.270        | 60                     | -1.289 to -1.240 | 10 |
| 0.221 to 0.250        | 59                     | -1.329 to -1.290 | 9  |
| 0.191 to 0.220        | 58                     | -1.379 to -1.330 | 8  |
| 0.161 to 0.190        | 57                     | -1.429 to -1.380 | 7  |
| 0.131 to 0.160        | 56                     | -1.489 to -1.430 | 6  |
| 0.111 to 0.130        | 55                     | -1.549 to -1.490 | 5  |
| 0.081 to 0.110        | 54                     | -1.619 to -1.550 | 4  |
| 0.051 to 0.080        | 53                     | -1.699 to -1.620 | 3  |
| 0.031 to 0.050        | 52                     | -1.799 to -1.700 | 2  |
| 0.001 to 0.030        | 51                     | -2.029 to -1.800 | 1  |
| -0.029 to 0.000       | 50                     | -2.030 or Less   | 0  |
|                       | 1                      |                  | 1  |

Table 15. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 6.

| 1                                | 16. Estimate of LPWL or |                                  |              |
|----------------------------------|-------------------------|----------------------------------|--------------|
| Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL            | Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL |
| 1.891 or More                    | 100                     | -0.029 to 0.000                  | 50           |
| 1.761 to 1.890                   | 99                      | -0.049 to -0.030                 | 49           |
| 1.671 to 1.760                   | 98                      | -0.079 to -0.050                 | 48           |
| 1.591 to 1.670                   | 97                      | -0.109 to -0.080                 | 47           |
| 1.521 to 1.590                   | 96                      | -0.129 to -0.110                 | 46           |
| 1.461 to 1.520                   | 95                      | -0.159 to -0.130                 | 45           |
| 1.401 to 1.460                   | 94                      | -0.189 to -0.160                 | 44           |
| 1.351 to 1.400                   | 93                      | -0.209 to -0.190                 | 43           |
| 1.301 to 1.350                   | 92                      | -0.239 to -0.210                 | 42           |
| 1.251 to 1.300                   | 91                      | -0.269 to -0.240                 | 41           |
| 1.201 to 1.250                   | 90                      | -0.299 to -0.270                 | 40           |
| 1.161 to 1.200                   | 89                      | -0.319 to -0.300                 | 39           |
| 1.121 to 1.160                   | 88                      | -0.349 to -0.320                 | 38           |
| 1.081 to 1.120                   | 87                      | -0.379 to -0.350                 | 37           |
| 1.041 to 1.080                   | 86                      | -0.409 to -0.380                 | 36           |
| 1.001 to 1.040                   | 85                      | -0.439 to -0.410                 | 35           |
| 0.961 to 1.000                   | 84                      | -0.459 to -0.440                 | 34           |
| 0.931 to 0.960                   | 83                      | -0.489 to -0.460                 | 33           |
| 0.901 to 0.930                   | 82                      | -0.489 to -0.480                 | 32           |
|                                  |                         |                                  |              |
| 0.861 to 0.900                   | 81                      | -0.549 to -0.520                 | 31           |
| 0.831 to 0.860                   | 80                      | -0.579 to -0.550                 | 30           |
| 0.801 to 0.830                   | 79                      | -0.609 to -0.580                 | 29           |
| 0.761 to 0.800                   | 78                      | -0.639 to -0.610                 | 28           |
| 0.731 to 0.760                   | 77                      | -0.669 to -0.640                 | 27           |
| 0.701 to 0.730                   | 76                      | -0.699 to -0.670                 | 26           |
| 0.671 to 0.700                   | 75                      | -0.729 to -0.700                 | 25           |
| 0.641 to 0.670                   | 74                      | -0.759 to -0.730                 | 24           |
| 0.611 to 0.640                   | 73                      | -0.799 to -0.760                 | 23           |
| 0.581 to 0.610                   | 72                      | -0.829 to -0.800                 | 22           |
| 0.551 to 0.580                   | 71                      | -0.859 to -0.830                 | 21           |
| 0.521 to 0.550                   | 70                      | -0.899 to -0.860                 | 20           |
| 0.491 to 0.520                   | 69                      | -0.929 to -0.900                 | 19           |
| 0.461 to 0.490                   | 68                      | -0.959 to -0.930                 | 18           |
| 0.441 to 0.460                   | 67                      | -0.999 to -0.960                 | 17           |
| 0.411 to 0.440                   | 66                      | -1.039 to -1.000                 | 16           |
| 0.381 to 0.410                   | 65                      | -1.079 to -1.040                 | 15           |
| 0.351 to 0.380                   | 64                      | -1.119 to -1.080                 | 14           |
| 0.321 to 0.350                   | 63                      | -1.159 to -1.120                 | 13           |
| 0.301 to 0.320                   | 62                      | -1.199 to -1.160                 | 12           |
| 0.271 to 0.300                   | 61                      | -1.249 to -1.200                 | 11           |
| 0.241 to 0.270                   | 60                      | -1.299 to -1.250                 | 10           |
| 0.211 to 0.240                   | 59                      | -1.349 to -1.300                 | 9            |
| 0.191 to 0.210                   | 58                      | -1.399 to -1.350                 | 8            |
| 0.161 to 0.190                   | 57                      | -1.459 to -1.400                 | 7            |
| 0.131 to 0.160                   | 56                      | -1.519 to -1.460                 | 6            |
| 0.111 to 0.130                   | 55                      | -1.589 to -1.520                 | 5            |
| 0.081 to 0.110                   | 54                      | -1.669 to -1.590                 | 4            |
| 0.051 to 0.080                   | 53                      | -1.759 to -1.670                 | 3            |
| 0.031 to 0.050                   | 52                      | -1.889 to -1.760                 | 2            |
|                                  | 51                      |                                  | 1            |
| 0.001 to 0.030                   |                         | -2.229 to -1.890                 |              |
| -0.029 to 0.000                  | 50                      | -2.230 or Less                   | 0            |

Table 16. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 7.

|                 | 7. Estimate of LPWL or |                       |    |
|-----------------|------------------------|-----------------------|----|
| $Q_L$ or $Q_U$  | LPWL or UPWL           | $Q_L \text{ or } Q_U$ |    |
| I.951 or More   | 100                    | -0.029 to 0.000       | 50 |
| 1.811 to 1.950  | 99                     | -0.049 to -0.030      | 49 |
| 1.701 to 1.810  | 98                     | -0.079 to -0.050      | 48 |
| 1.611 to 1.700  | 97                     | -0.099 to -0.080      | 47 |
| 1.541 to 1.610  | 96                     | -0.129 to -0.100      | 46 |
| 1.471 to 1.540  | 95                     | -0.159 to -0.130      | 45 |
| 1.411 to 1.470  | 94                     | -0.189 to -0.160      | 44 |
| 1.361 to 1.410  | 93                     | -0.209 to -0.190      | 43 |
| 1.301 to 1.360  | 92                     | -0.239 to -0.210      | 42 |
| 1.251 to 1.300  | 91                     | -0.269 to -0.240      | 41 |
| 1.211 to 1.250  | 90                     | -0.289 to -0.270      | 40 |
| 1.161 to 1.210  | 89                     | -0.319 to -0.290      | 39 |
| 1.121 to 1.160  | 88                     | -0.349 to -0.320      | 38 |
| 1.081 to 1.120  | 87                     | -0.379 to -0.350      | 37 |
| 1.041 to 1.080  | 86                     | -0.399 to -0.380      | 36 |
| 1.001 to 1.040  | 85                     | -0.429 to -0.400      | 35 |
| 0.961 to 1.000  | 84                     | -0.459 to -0.430      | 34 |
| 0.931 to 0.960  | 83                     | -0.489 to -0.460      | 33 |
| 0.891 to 0.930  | 82                     | -0.519 to -0.490      | 32 |
| 0.861 to 0.890  | 81                     | -0.549 to -0.520      | 31 |
| 0.821 to 0.860  | 80                     | -0.569 to -0.550      | 30 |
| 0.791 to 0.820  | 79                     | -0.599 to -0.570      | 29 |
| 0.761 to 0.790  | 78                     | -0.629 to -0.600      | 28 |
| 0.731 to 0.760  | 77                     | -0.659 to -0.630      | 27 |
| 0.701 to 0.730  | 76                     | -0.699 to -0.660      | 26 |
| 0.661 to 0.700  | 75                     | -0.729 to -0.700      | 25 |
| 0.631 to 0.660  | 74                     | -0.759 to -0.730      | 24 |
| 0.601 to 0.630  | 73                     | -0.789 to -0.760      | 23 |
| 0.571 to 0.600  | 72                     | -0.819 to -0.790      | 22 |
| 0.551 to 0.570  | 71                     | -0.859 to -0.820      | 21 |
| 0.521 to 0.550  | 70                     | -0.889 to -0.860      | 20 |
| 0.491 to 0.520  | 69                     | -0.929 to -0.890      | 19 |
| 0.461 to 0.490  | 68                     | -0.959 to -0.930      | 18 |
| 0.431 to 0.460  | 67                     | -0.999 to -0.960      | 17 |
| 0.401 to 0.430  | 66                     | -1.039 to -1.000      | 16 |
| 0.381 to 0.400  | 65                     | -1.079 to -1.040      | 15 |
| 0.351 to 0.380  | 64                     | -1.119 to -1.080      | 14 |
| 0.321 to 0.350  | 63                     | -1.159 to -1.120      | 13 |
| 0.291 to 0.320  | 62                     | -1.209 to -1.160      | 12 |
| 0.271 to 0.290  | 61                     | -1.249 to -1.210      | 11 |
| 0.241 to 0.270  | 60                     | -1.299 to -1.250      | 10 |
| 0.211 to 0.240  | 59                     | -1.359 to -1.300      | 9  |
| 0.191 to 0.210  | 58                     | -1.409 to -1.360      | 8  |
| 0.161 to 0.190  | 57                     | -1.469 to -1.410      | 7  |
| 0.131 to 0.160  | 56                     | -1.539 to -1.470      | 6  |
| 0.101 to 0.130  | 55                     | -1.609 to -1.540      | 5  |
| 0.081 to 0.100  | 54                     | -1.699 to -1.610      | 4  |
| 0.051 to 0.080  | 53                     | -1.809 to -1.700      | 3  |
| 0.031 to 0.050  | 52                     | -1.949 to -1.810      | 2  |
| 0.001 to 0.030  | 51                     | -2.389 to -1.950      | 1  |
| -0.029 to 0.000 | 50                     | -2.390 or Less        | 0  |
|                 | L                      | u                     | L  |

Table 17. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 8.

|                                  | 3. Estimate of LPWL or |                                  |              |
|----------------------------------|------------------------|----------------------------------|--------------|
| Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL           | Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL |
| 2.001 or More                    | 100                    | -0.029 to 0.000                  | 50           |
| 1.841 to 2.000                   | 99                     | -0.049 to -0.030                 | 49           |
| 1.721 to 1.840                   | 98                     | -0.079 to -0.050                 | 48           |
| 1.631 to 1.720                   | 97                     | -0.099 to -0.080                 | 47           |
| 1.551 to 1.630                   | 96                     | -0.129 to -0.100                 | 46           |
| 1.481 to 1.550                   | 95                     | -0.159 to -0.130                 | 45           |
| 1.421 to 1.480                   | 94                     | -0.179 to -0.160                 | 44           |
| 1.361 to 1.420                   | 93                     | -0.209 to -0.180                 | 43           |
| 1.311 to 1.360                   | 92                     | -0.239 to -0.210                 | 42           |
| 1.261 to 1.310                   | 91                     | -0.259 to -0.240                 | 41           |
| 1.211 to 1.260                   | 90                     | -0.289 to -0.260                 | 40           |
| 1.171 to 1.210                   | 89                     | -0.319 to -0.290                 | 39           |
| 1.121 to 1.170                   | 88                     | -0.349 to -0.320                 | 38           |
| 1.081 to 1.120                   | 87                     | -0.369 to -0.350                 | 37           |
| 1.041 to 1.080                   | 86                     | -0.399 to -0.370                 | 36           |
| 1.001 to 1.040                   | 85                     | -0.429 to -0.400                 | 35           |
| 0.961 to 1.000                   | 84                     | -0.459 to -0.430                 | 34           |
| 0.931 to 0.960                   | 83                     | -0.479 to -0.460                 | 33           |
| 0.891 to 0.930                   | 82                     | -0.509 to -0.480                 | 32           |
| 0.861 to 0.890                   | 81                     | -0.539 to -0.510                 | 31           |
| 0.821 to 0.860                   | 80                     | -0.569 to -0.540                 | 30           |
| 0.791 to 0.820                   | 79                     | -0.599 to -0.570                 | 29           |
| 0.761 to 0.790                   | 78                     | -0.629 to -0.600                 | 28           |
| 0.721 to 0.760                   | 77                     | -0.659 to -0.630                 | 27           |
| 0.691 to 0.720                   | 76                     | -0.689 to -0.660                 | 26           |
| 0.661 to 0.690                   | 75                     | -0.719 to -0.690                 | 25           |
| 0.631 to 0.660                   | 74                     | -0.759 to -0.720                 | 24           |
| 0.601 to 0.630                   | 73                     | -0.789 to -0.760                 | 23           |
| 0.571 to 0.600                   | 72                     | -0.819 to -0.790                 | 22           |
| 0.541 to 0.570                   | 71                     | -0.859 to -0.820                 | 21           |
| 0.511 to 0.540                   | 70                     | -0.889 to -0.860                 | 20           |
| 0.481 to 0.510                   | 69                     | -0.929 to -0.890                 | 19           |
| 0.461 to 0.480                   | 68                     | -0.959 to -0.930                 | 18           |
| 0.431 to 0.460                   | 67                     | -0.999 to -0.960                 | 17           |
| 0.401 to 0.430                   | 66                     | -1.039 to -1.000                 | 16           |
| 0.371 to 0.400                   | 65                     | -1.079 to -1.040                 | 15           |
| 0.351 to 0.370                   | 64                     | -1.119 to -1.080                 | 14           |
| 0.321 to 0.350                   | 63                     | -1.169 to -1.120                 | 13           |
| 0.291 to 0.320                   | 62                     | -1.209 to -1.170                 | 12           |
| 0.261 to 0.290                   | 61                     | -1.259 to -1.210                 | 11           |
| 0.241 to 0.260                   | 60                     | -1.309 to -1.260                 | 10           |
| 0.211 to 0.240                   | 59                     | -1.359 to -1.310                 | 9            |
| 0.181 to 0.210                   | 58                     | -1.419 to -1.360                 | 8            |
| 0.161 to 0.180                   | 57                     | -1.479 to -1.420                 | 7            |
| 0.131 to 0.160                   | 56                     | -1.549 to -1.480                 | 6            |
| 0.101 to 0.130                   | 55                     | -1.629 to -1.550                 | 5            |
| 0.081 to 0.100                   | 54                     | -1.719 to -1.630                 | 4            |
| 0.051 to 0.080                   | 53                     | -1.839 to -1.720                 | 3            |
| 0.031 to 0.050                   | 52                     | -1.999 to -1.840                 | 2            |
| 0.001 to 0.030                   | 51                     | -2.529 to -2.000                 | 1            |
| -0.029 to 0.000                  | 50                     | -2.530 or Less                   | 0            |
|                                  |                        |                                  | L            |

Table 18. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 9.

|  | LPWL or UPWL | WL Using $Q_L$ or $Q_U$ for r                                   | LPWL or UPWL |
|--|--------------|---|--------------|
| <b><i>Q<sub>L</sub></i> or <i>Q<sub>U</sub></i></b><br>2.041 or More | 100          | <i>Q<sub>L</sub></i> or <i>Q<sub>U</sub></i><br>-0.029 to 0.000 | 50           |
|  |              | -0.049 to -0.030  | 49           |
| 1.861 to 2.040   | 99<br>98     |   | 49 48        |
| 1.741 to 1.860   |              | -0.079 to -0.050  | 40           |
| 1.651 to 1.740   | 97           | -0.099 to -0.080  |              |
| 1.561 to 1.650   | 96           | -0.129 to -0.100  | 46           |
| 1.491 to 1.560   | 95           | -0.159 to -0.130  | 45           |
| 1.431 to 1.490   | 94           | -0.179 to -0.160  | 44           |
| 1.361 to 1.430   | 93           | -0.209 to -0.180  | 43           |
| 1.311 to 1.360   | 92           | -0.239 to -0.210  | 42           |
| 1.261 to 1.310   | 91           | -0.259 to -0.240  | 41           |
| 1.211 to 1.260   | 90           | -0.289 to -0.260  | 40           |
| 1.171 to 1.210   | 89           | -0.319 to -0.290  | 39           |
| 1.121 to 1.170   | 88           | -0.339 to -0.320  | 38           |
| 1.081 to 1.120   | 87           | -0.369 to -0.340  | 37           |
| 1.041 to 1.080   | 86           | -0.399 to -0.370  | 36           |
| 1.001 to 1.040   | 85           | -0.429 to -0.400  | 35           |
| 0.961 to 1.000   | 84           | -0.449 to -0.430  | 34           |
| 0.921 to 0.960   | 83           | -0.479 to -0.450  | 33           |
| 0.891 to 0.920   | 82           | -0.509 to -0.480  | 32           |
| 0.851 to 0.890   | 81           | -0.539 to -0.510  | 31           |
| 0.821 to 0.850   | 80           | -0.569 to -0.540  | 30           |
| 0.791 to 0.820   | 79           | -0.599 to -0.570  | 29           |
| 0.751 to 0.790   | 78           | -0.629 to -0.600  | 28           |
| 0.721 to 0.750   | 77           | -0.659 to -0.630  | 27           |
| 0.691 to 0.720   | 76           | -0.689 to -0.660  | 26           |
| 0.661 to 0.690   | 75           | -0.719 to -0.690  | 25           |
| 0.631 to 0.660   | 74           | -0.749 to -0.720  | 24           |
| 0.601 to 0.630   | 73           | -0.789 to -0.750  | 23           |
| 0.571 to 0.600   | 72           | -0.819 to -0.790  | 22           |
| 0.541 to 0.570   | 71           | -0.849 to -0.820  | 21           |
| 0.511 to 0.540   | 70           | -0.889 to -0.850  | 20           |
| 0.481 to 0.510   | 69           | -0.919 to -0.890  | 19           |
| 0.451 to 0.480   | 68           | -0.959 to -0.920  | 18           |
| 0.431 to 0.450   | 67           | -0.999 to -0.960  | 17           |
| 0.401 to 0.430   | 66           | -1.039 to -1.000  | 16           |
| 0.371 to 0.400   | 65           | -1.079 to -1.040  | 15           |
| 0.341 to 0.370   | 64           | -1.119 to -1.080  | 14           |
| 0.321 to 0.340   | 63           | -1.169 to -1.120  | 13           |
| 0.291 to 0.320   | 62           | -1.209 to -1.170  | 12           |
| 0.261 to 0.290   | 61           | -1.259 to -1.210  | 11           |
| 0.241 to 0.260   | 60           | -1.309 to -1.260  | 10           |
| 0.211 to 0.240   | 59           | -1.359 to -1.310  | 9            |
| 0.181 to 0.210   | 58           | -1.429 to -1.360  | 8            |
| 0.161 to 0.180   | 57           | -1.489 to -1.430  | 7            |
| 0.131 to 0.160   | 56           | -1.559 to -1.490  | 6            |
| 0.101 to 0.130   | 55           | -1.649 to -1.560  | 5            |
| 0.081 to 0.100   | 54           | -1.739 to -1.650  | 4            |
| 0.051 to 0.080   | 53           | -1.859 to -1.740  | 3            |
| 0.031 to 0.050   | 52           | -2.039 to -1.860  | 2            |
| 0.001 to 0.030   | 51           | -2.649 to -2.040  | 1            |
| -0.029 to 0.000  | 50           | -2.650 or Less  | 0            |

Table 19. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 10 to 11.

|                 | timate of LPWL or UPW |                                  |              |
|-----------------|-----------------------|----------------------------------|--------------|
| $Q_L$ or $Q_U$  | LPWL or UPWL          | Q <sub>L</sub> or Q <sub>U</sub> | LPWL or UPWL |
| 2.091 or More   | 100                   | -0.029 to 0.000                  | 50           |
| 1.911 to 2.090  | 99                    | -0.049 to -0.030                 | 49           |
| 1.771 to 1.910  | 98                    | -0.079 to -0.050                 | 48           |
| 1.671 to 1.770  | 97                    | -0.099 to -0.080                 | 47           |
| 1.581 to 1.670  | 96                    | -0.129 to -0.100                 | 46           |
| 1.501 to 1.580  | 95                    | -0.159 to -0.130                 | 45           |
| 1.441 to 1.500  | 94                    | -0.179 to -0.160                 | 44           |
| 1.371 to 1.440  | 93                    | -0.209 to -0.180                 | 43           |
| 1.321 to 1.370  | 92                    | -0.229 to -0.210                 | 42           |
| 1.261 to 1.320  | 91                    | -0.259 to -0.230                 | 41           |
| 1.211 to 1.260  | 90                    | -0.289 to -0.260                 | 40           |
| 1.171 to 1.210  | 89                    | -0.309 to -0.290                 | 39           |
| 1.121 to 1.170  | 88                    | -0.339 to -0.310                 | 38           |
| 1.081 to 1.120  | 87                    | -0.369 to -0.340                 | 37           |
| 1.041 to 1.080  | 86                    | -0.399 to -0.370                 | 36           |
| 1.001 to 1.040  | 85                    | -0.419 to -0.400                 | 35           |
| 0.961 to 1.000  | 84                    | -0.449 to -0.420                 | 34           |
| 0.921 to 0.960  | 83                    | -0.479 to -0.450                 | 33           |
| 0.891 to 0.920  | 82                    | -0.509 to -0.480                 | 32           |
| 0.851 to 0.890  | 81                    | -0.539 to -0.510                 | 31           |
| 0.821 to 0.850  | 80                    | -0.569 to -0.540                 | 30           |
| 0.781 to 0.820  | 79                    | -0.589 to -0.570                 | 29           |
| 0.751 to 0.780  | 78                    | -0.619 to -0.590                 | 28           |
| 0.721 to 0.750  | 77                    | -0.659 to -0.620                 | 27           |
| 0.691 to 0.720  | 76                    | -0.689 to -0.660                 | 26           |
| 0.661 to 0.690  | 75                    | -0.719 to -0.690                 | 25           |
| 0.621 to 0.660  | 74                    | -0.749 to -0.720                 | 24           |
| 0.591 to 0.620  | 73                    | -0.779 to -0.750                 | 23           |
| 0.571 to 0.590  | 72                    | -0.819 to -0.780                 | 22           |
| 0.541 to 0.570  | 71                    | -0.849 to -0.820                 | 21           |
| 0.511 to 0.540  | 70                    | -0.889 to -0.850                 | 20           |
| 0.481 to 0.510  | 69                    | -0.919 to -0.890                 | 19           |
| 0.451 to 0.480  | 68                    | -0.959 to -0.920                 | 18           |
| 0.421 to 0.450  | 67                    | -0.999 to -0.960                 | 17           |
| 0.401 to 0.420  | 66                    | -1.039 to -1.000                 | 16           |
| 0.371 to 0.400  | 65                    | -1.079 to -1.040                 | 15           |
| 0.341 to 0.370  | 64                    | -1.119 to -1.080                 | 14           |
| 0.311 to 0.340  | 63                    | -1.169 to -1.120                 | 13           |
| 0.291 to 0.310  | 62                    | -1.209 to -1.170                 | 12           |
| 0.261 to 0.290  | 61                    | -1.259 to -1.210                 | 11           |
| 0.231 to 0.260  | 60                    | -1.319 to -1.260                 | 10           |
| 0.211 to 0.230  | 59                    | -1.369 to -1.320                 | 9            |
| 0.181 to 0.210  | 58                    | -1.439 to -1.370                 | 8            |
| 0.161 to 0.180  | 57                    | -1.499 to -1.440                 | 7            |
| 0.131 to 0.160  | 56                    | -1.579 to -1.500                 | 6            |
| 0.101 to 0.130  | 55                    | -1.669 to -1.580                 | 5            |
| 0.081 to 0.100  | 54                    | -1.769 to -1.670                 | 4            |
| 0.051 to 0.080  | 53                    | -1.909 to -1.770                 | 3            |
| 0.031 to 0.050  | 52                    | -2.089 to -1.910                 | 2            |
| 0.001 to 0.030  | 52                    | -2.829 to -2.090                 | 1            |
| -0.029 to 0.000 | 50                    | -2.830 or Less                   | 0            |
| 0.023 10 0.000  | 50                    | 2.000 01 2000                    | v            |

Table 20. Estimate of LPWL or UPWL Using  $Q_L$  or  $Q_U$  for n = 12 or more